

# Thermal Differential EXAFS

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- An introduction to Differential EXAFS
- Thermal modulation of sample materials
- Proof of concept – Thermal expansion measurements
- Data analysis procedure
- Future work – Probing phase transitions with single Kelvin resolution

# What is Differential EXAFS?



A Differential EXAFS spectrum is the difference between two conventional EXAFS spectra, taken with all environmental parameters kept constant except for *unit modulation* of some parameter of interest, such as temperature.

As a result, the signal contains information relating to structural *strain* that occurred due the change in chosen parameter.

First used to measure magnetostriction in FeCo (R.F. Pettifer et al., *Nature* 435, 78)

## Potential problems:

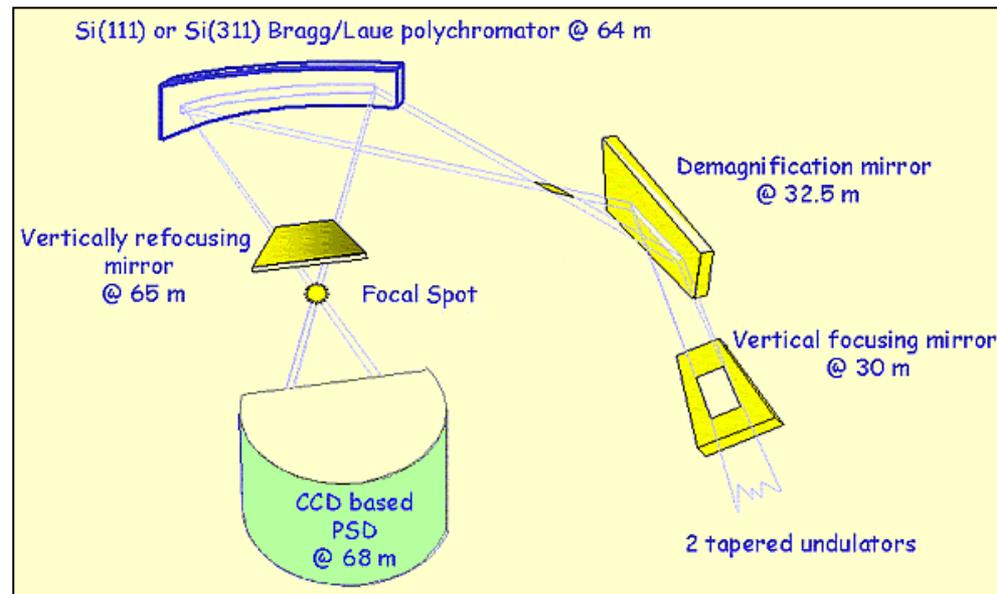
- Energy drift of the beam generating spurious signals
- Spatial drift of the beam causing measurement of different parts of sample
- Statistical noise preventing resolution of structural changes, typically  $\sim 10^{-5}\text{\AA}$

## Solutions:

- Acquire both spectra in minimal time; of the order of a few seconds or less
- Use a high intensity 3<sup>rd</sup> generation source in conjunction with a sensitive detector
- Average signal over many pairs of measurements  
(O. Mathon et al., *J. Synchrotron Rad.* 11, 423)

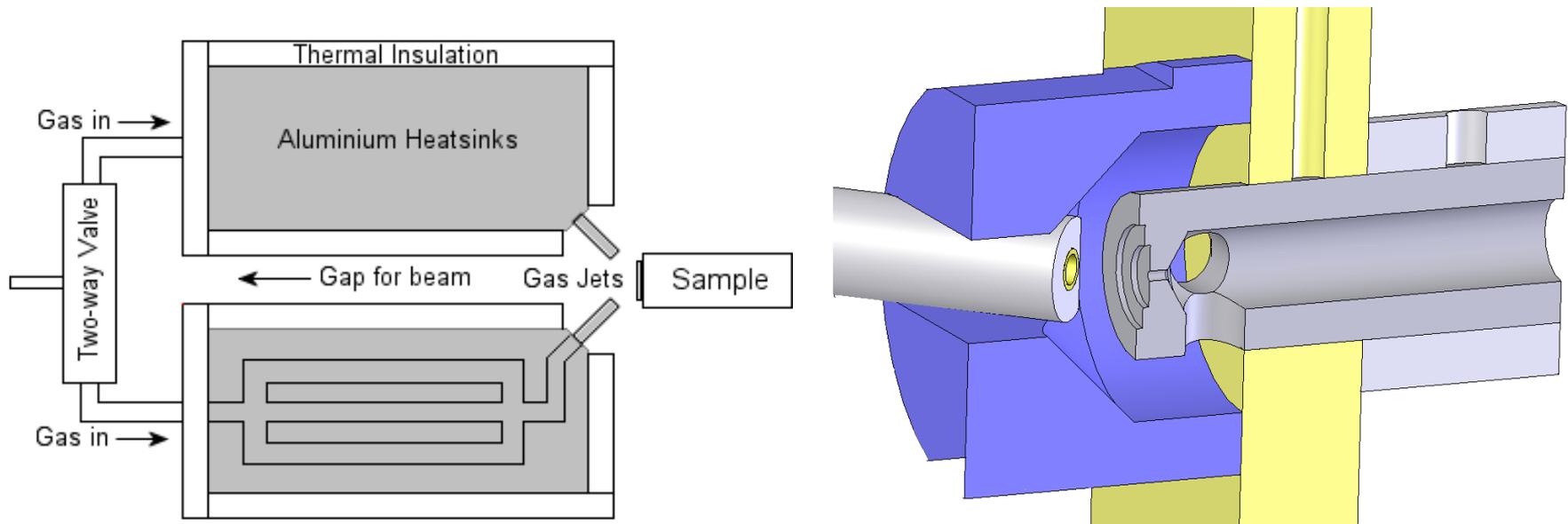
# ID24 for Differential EXAFS

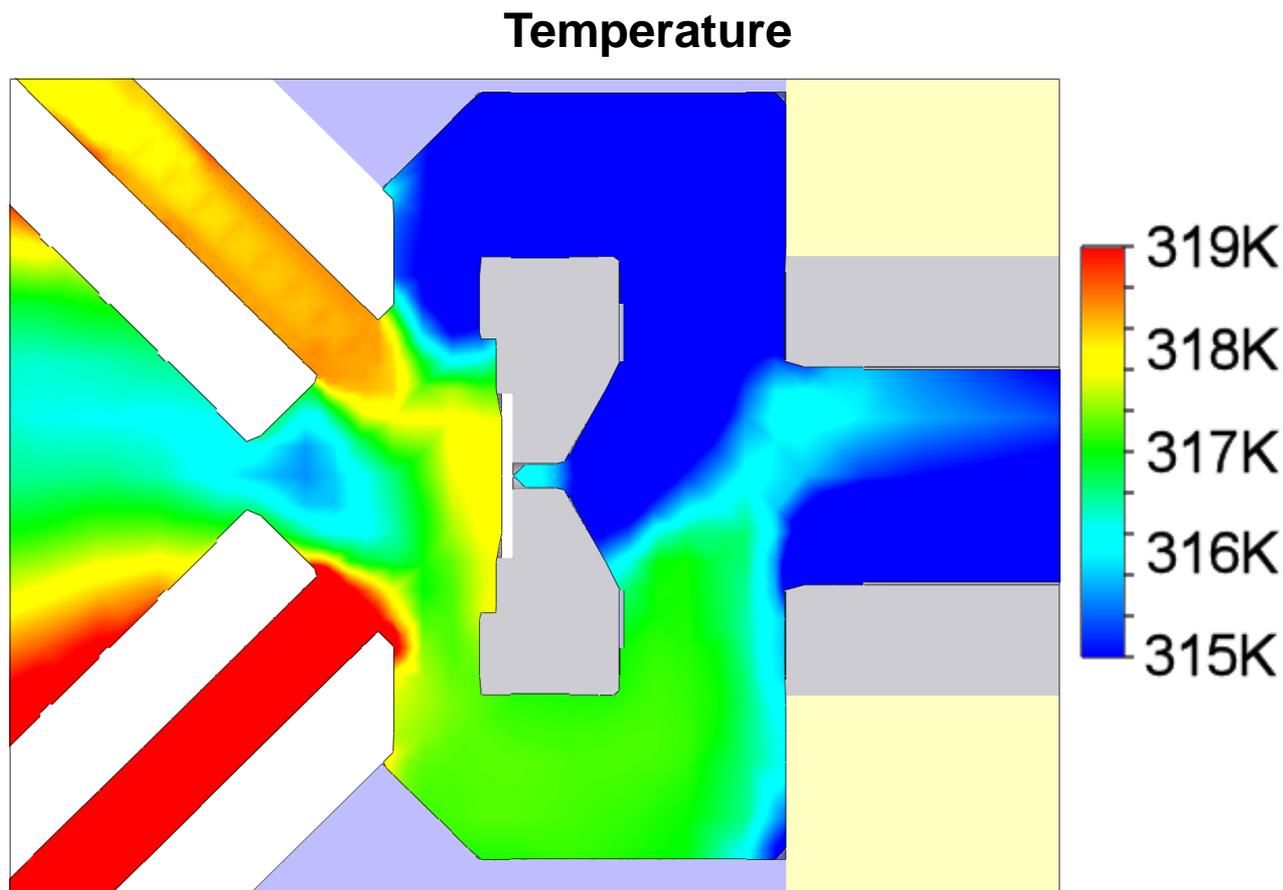
- All Differential EXAFS experiments performed to date have been conducted on ID24, the Dispersive XAS beamline of the ESRF.
- Mounted on a high-intensity 3<sup>rd</sup> generation undulator source.
- Entire spectrum is obtained simultaneously in around 200ms, minimising drift.
- Has no moving parts, which improves beam stability.
- Tight focal spot size allows use of samples with tiny thermal mass.



# Thermal modulation apparatus

- Thermal modulation apparatus must alternately heat and cool the sample material between XAS measurements at  $T+$  and  $T-$ .
- The heating/cooling must be quick. Ideally less than 1 second.
- Temperature at  $T+$  and  $T-$  must be both stable and reproducible.
- Solution is to use two jets of heated gas, switched by a fluidic valve.





- Gas is heated as it traverses the heatsink
- Heated jet of gas strikes sample
- Gas passing around the rear of the sample provides secondary heating

$$\chi(k, T) = \sum_j A_j(k) e^{-2\sigma_j^2(T)k^2} \sin(s_j(T)k + \phi_j(k))$$

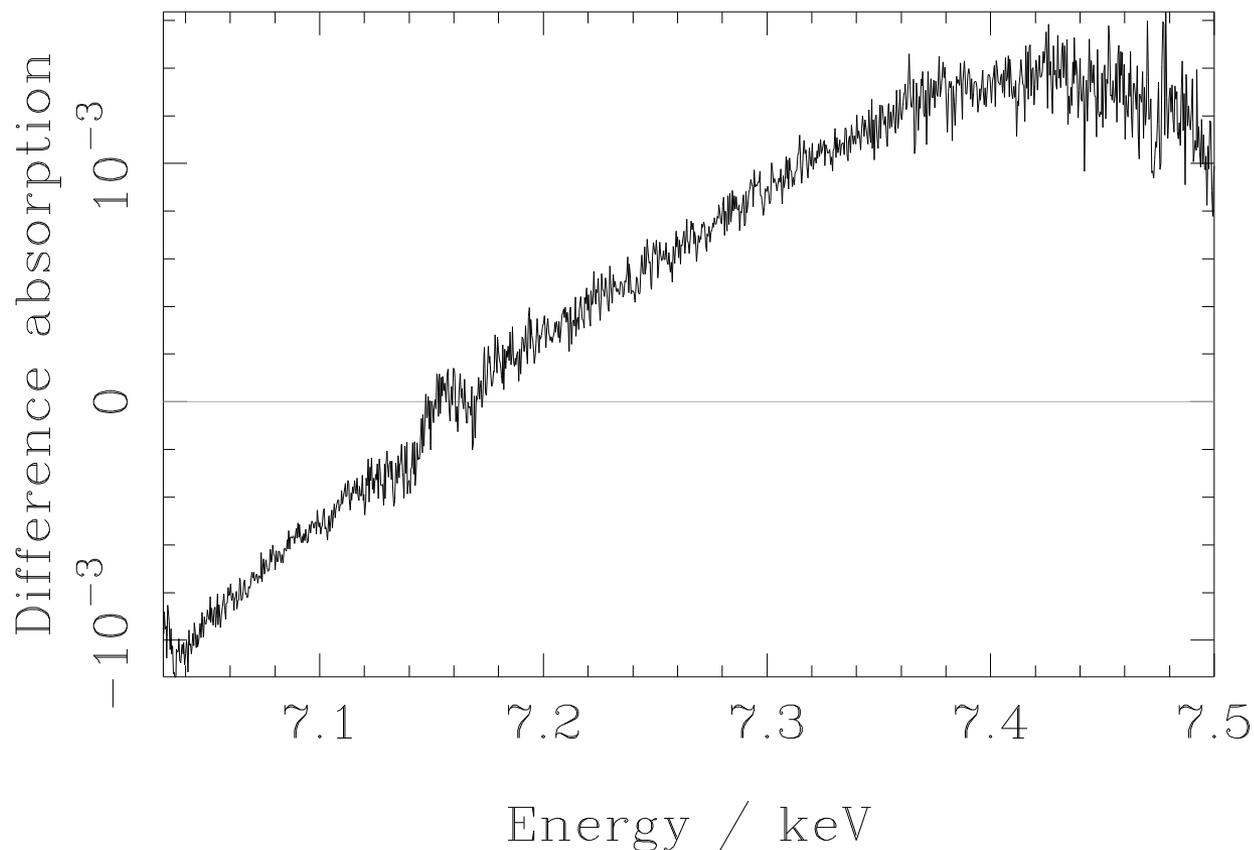
Neglect weak path length dependence of A and  $\phi$ , making them T independent.

Take a first order Taylor expansion with respect to temperature

$$\frac{\partial \chi(k, T)}{\partial T} = \sum_j \left( \alpha s_j k A_j(k) e^{-2\sigma_j^2(T)k^2} \cos(s_j(T)k + \phi_j(k)) - 2k^2 \frac{\partial \sigma_j^2}{\partial T} A_j(k) e^{-2\sigma_j^2(T)k^2} \sin(s_j(T)k + \phi_j(k)) \right)$$

## Key Features

- The Differential signal contains both a Thermal Expansion and Disorder term.
- Thermal Disorder contributions are in phase with the original EXAFS signal.
- Thermal Expansion contributions are in quadrature with the original EXAFS signal.
- Given  $\alpha \ll \partial \sigma_j^2 / \partial T$ , signal will be largely in phase with  $\chi$ , but slightly phase shifted.

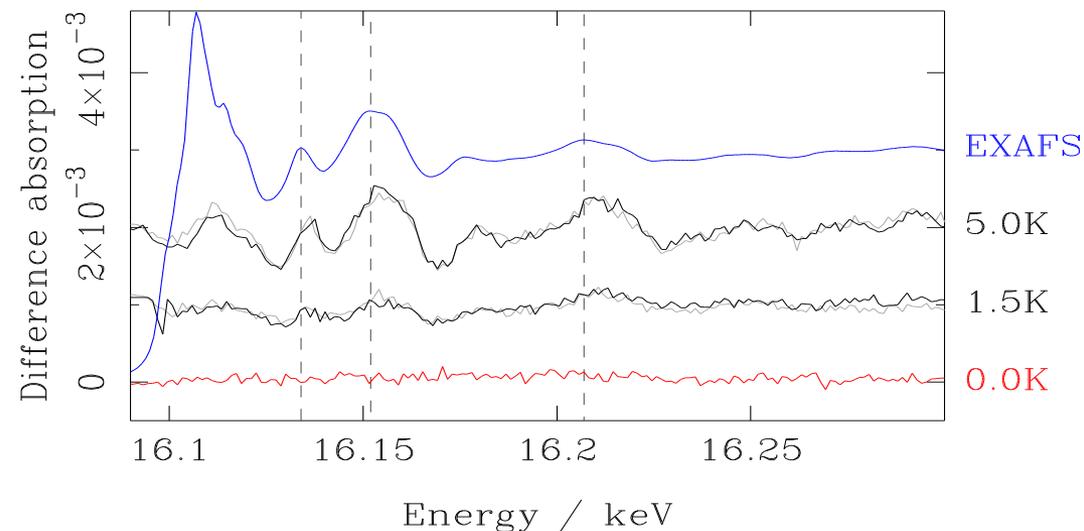
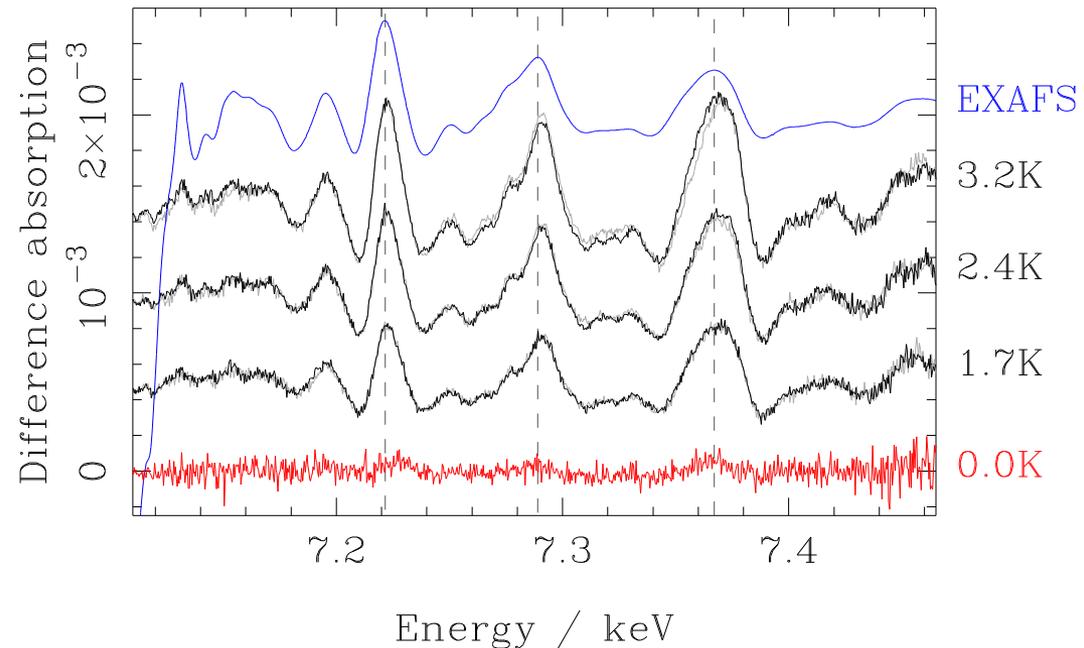


- Must obtain a flat DiffEXAFS baseline, passing through  $\Delta\chi = 0$ , for  $\Delta T = 0\text{K}$ .
- Pressure gradients within sample mount generated grey signal.
- 4 days of beamtime were needed to produce a flat baseline!

# Thermal Expansion measurements

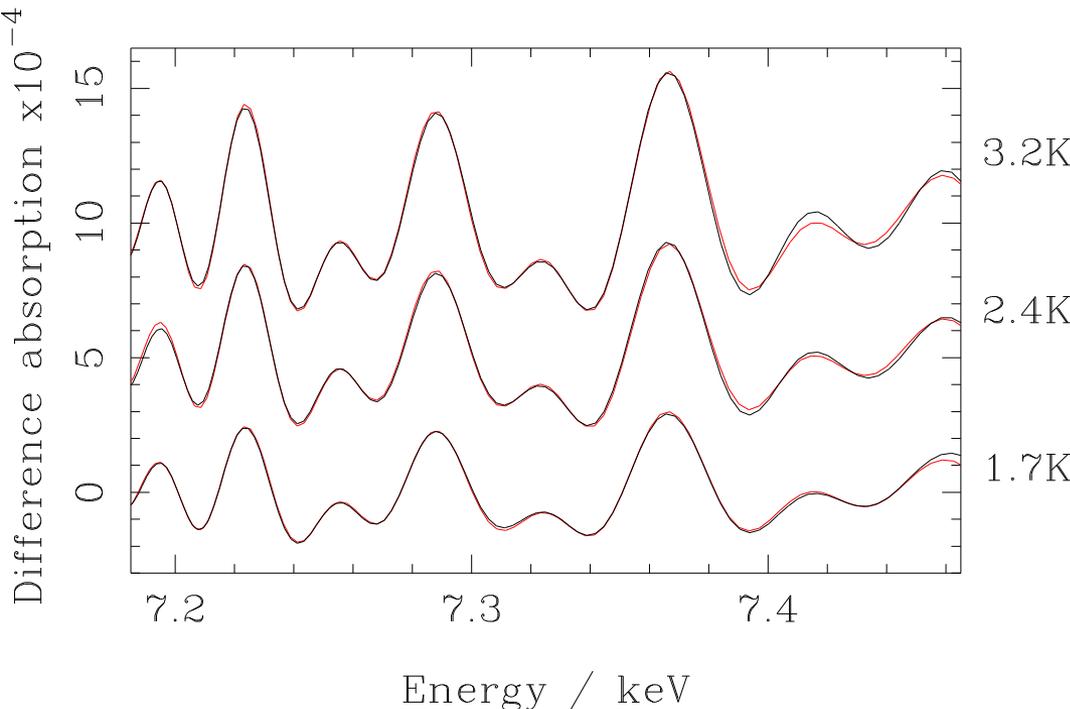


- To prove Thermal Differential EXAFS works in practice, thermal expansion measurements were made on samples of  $\alpha$ -Fe and  $\text{SrF}_2$
- Signals are averaged over 600 pairs of acquisitions for a range of temperature differences.
- Disorder term dominates given signals are largely in phase with EXAFS.
- DiffEXAFS peaks are phase shifted, indicating detection of the thermal expansion component.



## To obtain the thermal expansion coefficient:

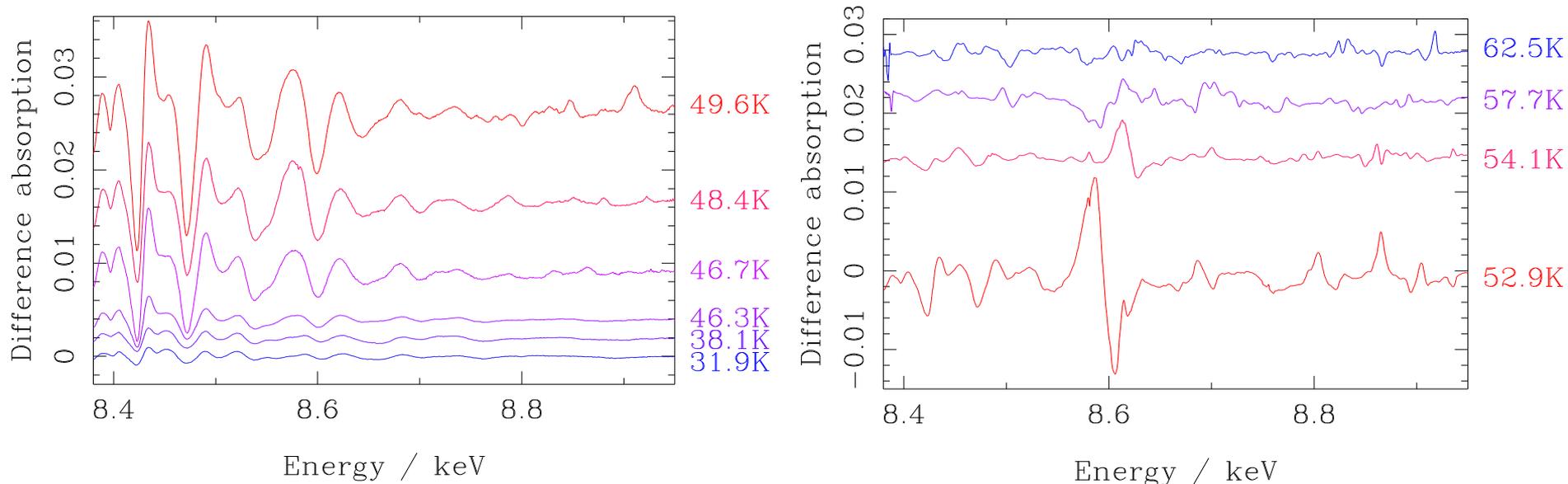
1. Define a reference from which to measure thermally induced displacements
2. Fit the differential fine-structure function to each differential signal to establish  $\alpha$  and the  $\partial\sigma_j^2/\partial T$
3.  $\alpha$  for Fe is  $11.8 \times 10^{-6} \text{K}^{-1}$



$\partial\sigma_j^2/\partial T$	$\Delta T = 1.7\text{K}$	$\Delta T = 2.4\text{K}$	$\Delta T = 3.2\text{K}$
SS1	$1.13 \pm 0.04$	$1.08 \pm 0.02$	$1.08 \pm 0.01$
SS2	$0.88 \pm 0.08$	$0.91 \pm 0.05$	$0.91 \pm 0.04$
SS3	$0 \pm 300$	$2.1 \pm 0.1$	$1.72 \pm 0.08$
SS4	$2.6 \pm 0.4$	$3.4 \pm 0.3$	$2.7 \pm 0.2$
Units of $\partial\sigma_j^2/\partial T$ are $\times 10^{-4} \text{\AA}^2$ and $\alpha$ is $\times 10^{-6} \text{K}^{-1}$	$12.1 \pm 0.8$	$12.1 \pm 0.8$	$11.8 \pm 0.6$

Thermal expansion measurements have shown Thermal Differential EXAFS works in practice.

But the true power of the technique lies in studies of disordered or amorphous systems or of non-linear phenomena such as *phase transitions*.



With temperature steps of  $\sim 1\text{K}$ , it is possible to measure structural changes over many points through the transition region itself rather than just above and below it.