

# Inorganic Nanotube Mesophases Enable Strong Self-Healing Fibers

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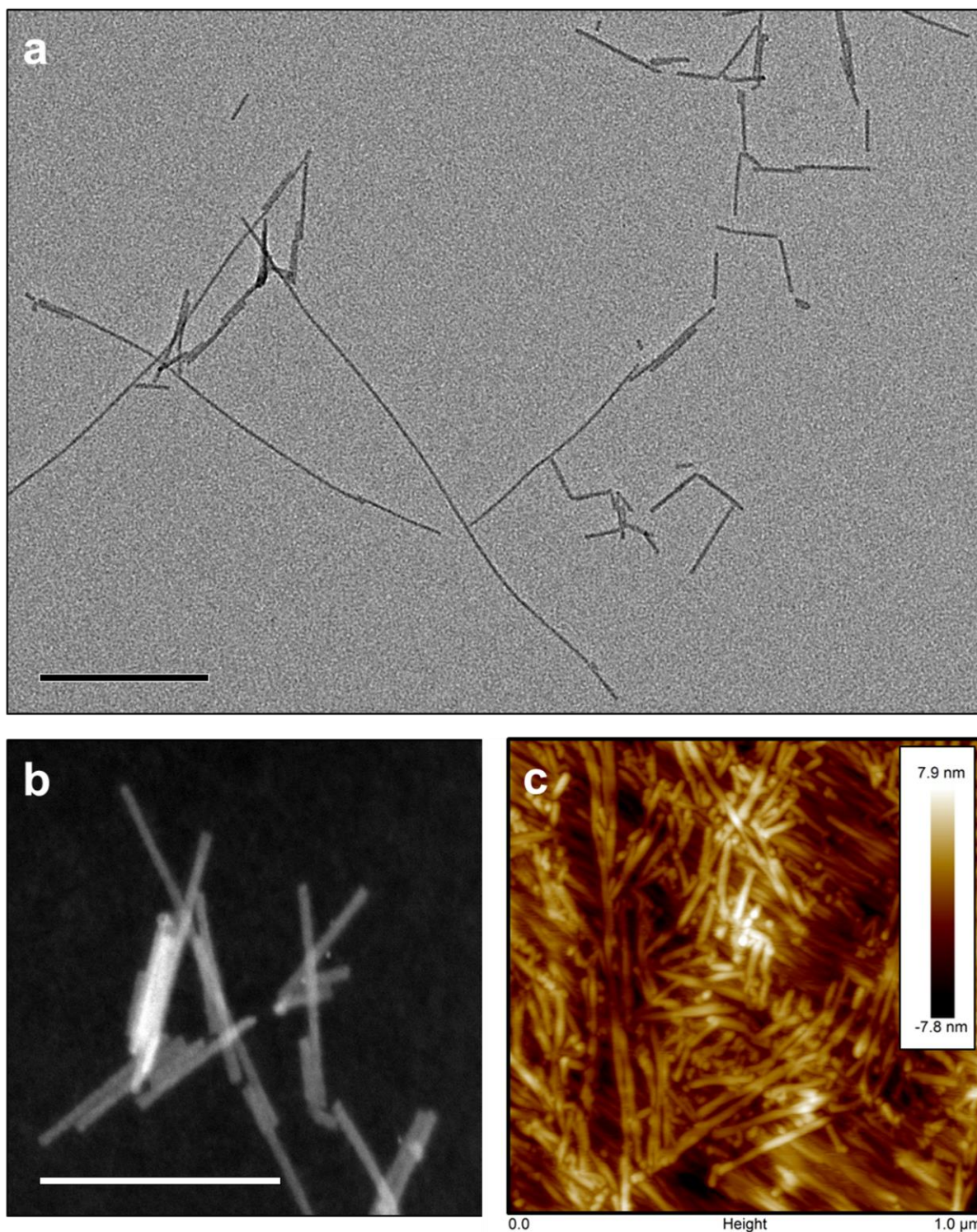
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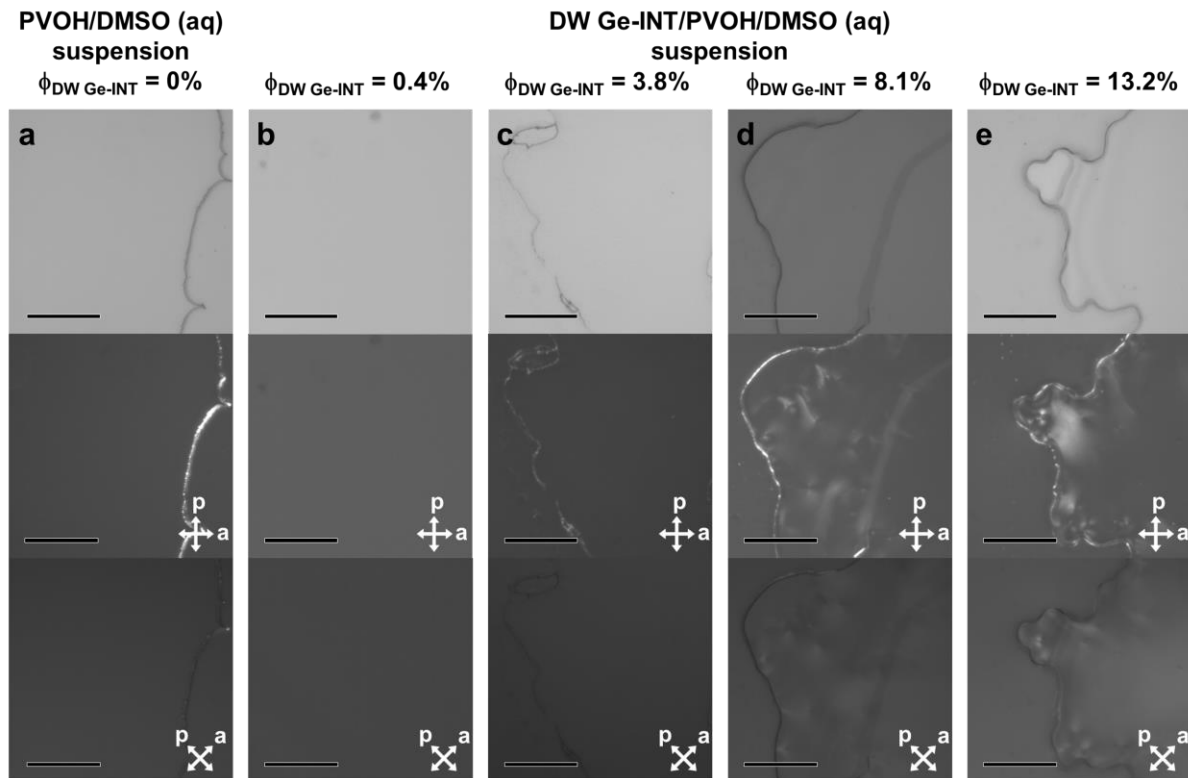
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## Morphology of double-walled aluminogermanate imogolite nanotubes



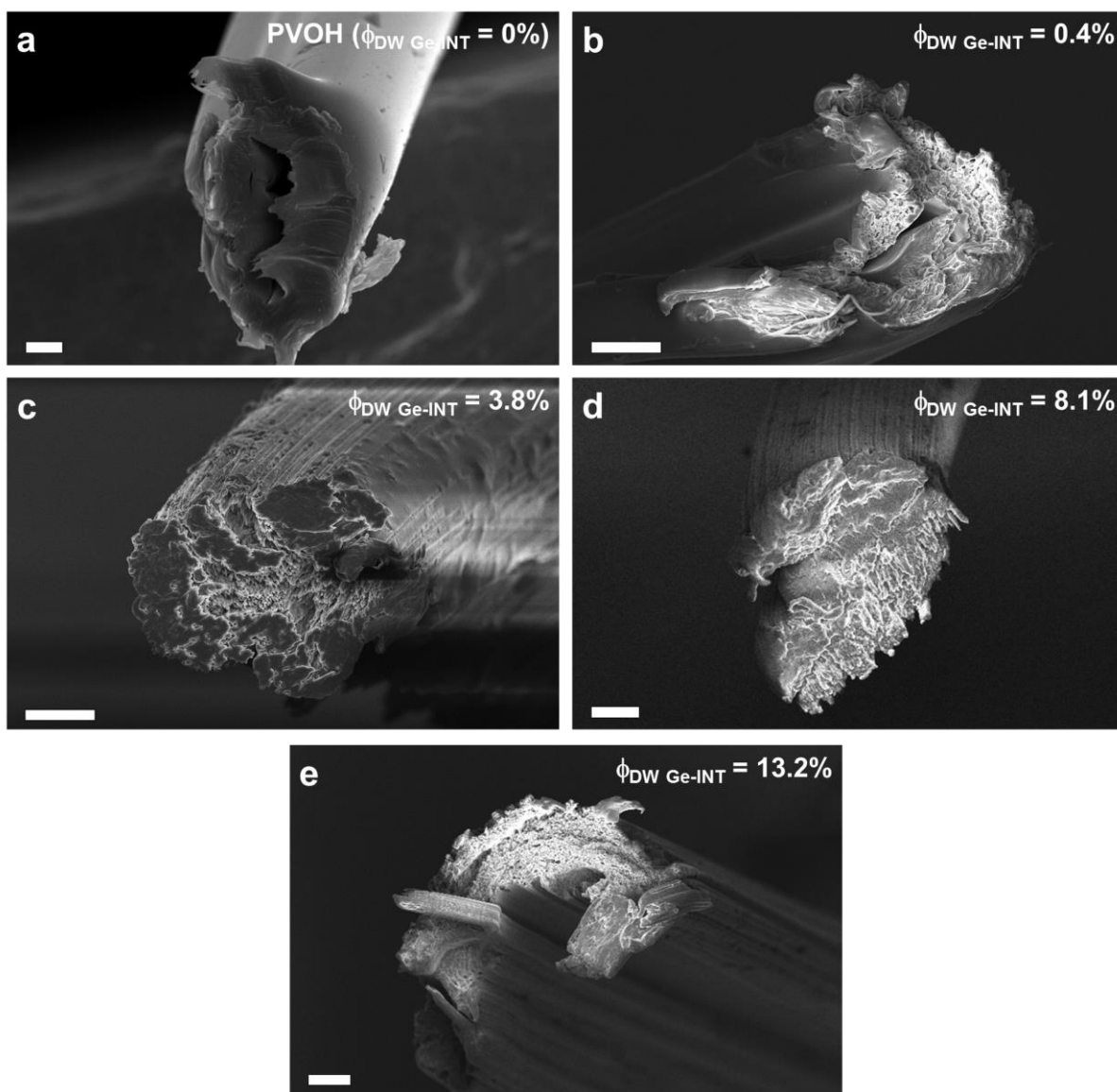
**Figure S1** Characterization of synthesized double-walled aluminogermanate imogolite nanotubes, (a) transmission electron micrograph (TEM) image with 200 nm scale bar, (b) higher magnification scanning TEM high-angle annular dark-field image with 100 nm scale bar, (c) atomic force microscopy box size 1 μm x 1 μm.

## Optical microscopy of double-walled aluminogermanate imogolite nanotube spinning dopes

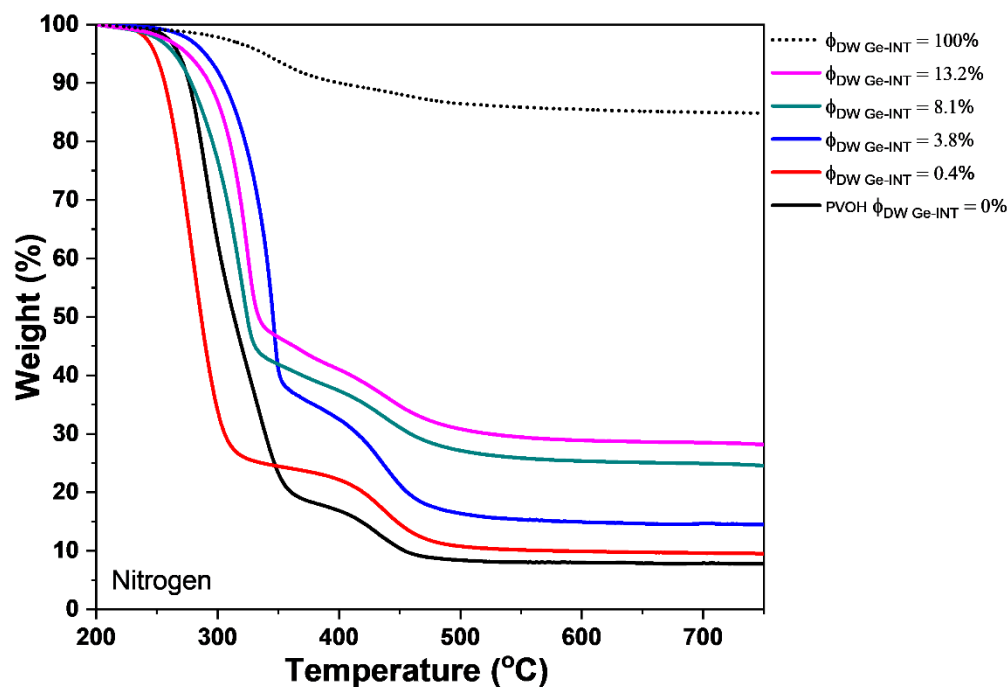


**Figure S2** Grayscale transmission optical micrographs of a range of spinning dopes, without polarizers (top) and with cross-polarizers (middle  $0^\circ/90^\circ$ , bottom  $45^\circ/-45^\circ$ ). The spinning dopes contain polyvinyl alcohol (PVOH) with varying double-walled aluminogermanate imogolite nanotubes (DW Ge-INTs) volume fraction ( $\phi_{\text{DW Ge-INT}}$ ), in water/dimethyl sulfoxide (DMSO). (a) PVOH solution ( $\phi_{\text{DW Ge-INT}} = 0\%$ ), DW Ge-INT/PVOH suspensions (b)  $\phi_{\text{DW Ge-INT}} = 0.4\%$ , (c)  $\phi_{\text{DW Ge-INT}} = 3.8\%$ , (d)  $\phi_{\text{DW Ge-INT}} = 8.1\%$ , (e)  $\phi_{\text{DW Ge-INT}} = 13.2\%$ ,  $50 \mu\text{m}$  scale bar for all frames.

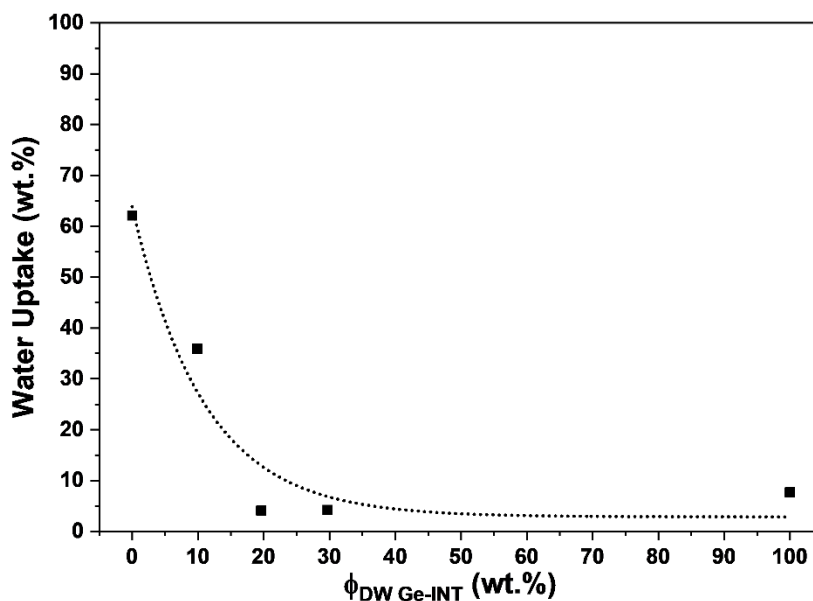
## Characterization of wet-spun fibers



**Figure S3** Scanning electron micrographs of cryo-fractured polyvinyl alcohol (PVOH) fiber cross-sections, containing varying fractions of double-walled aluminogermanate imogolite nanotubes (DW Ge-INTs): (a) PVOH fiber ( $\phi_{\text{DW Ge-INT}} = 0\%$ ), DW Ge-INT/PVOH composite fiber (b)  $\phi_{\text{DW Ge-INT}} = 0.4\%$ , (c)  $\phi_{\text{DW Ge-INT}} = 3.8\%$ , (d)  $\phi_{\text{DW Ge-INT}} = 8.1\%$ , (e)  $\phi_{\text{DW Ge-INT}} = 13.2\%$ , 10  $\mu\text{m}$  scale bar for all frames, nominal diameters are provided in Table S2.

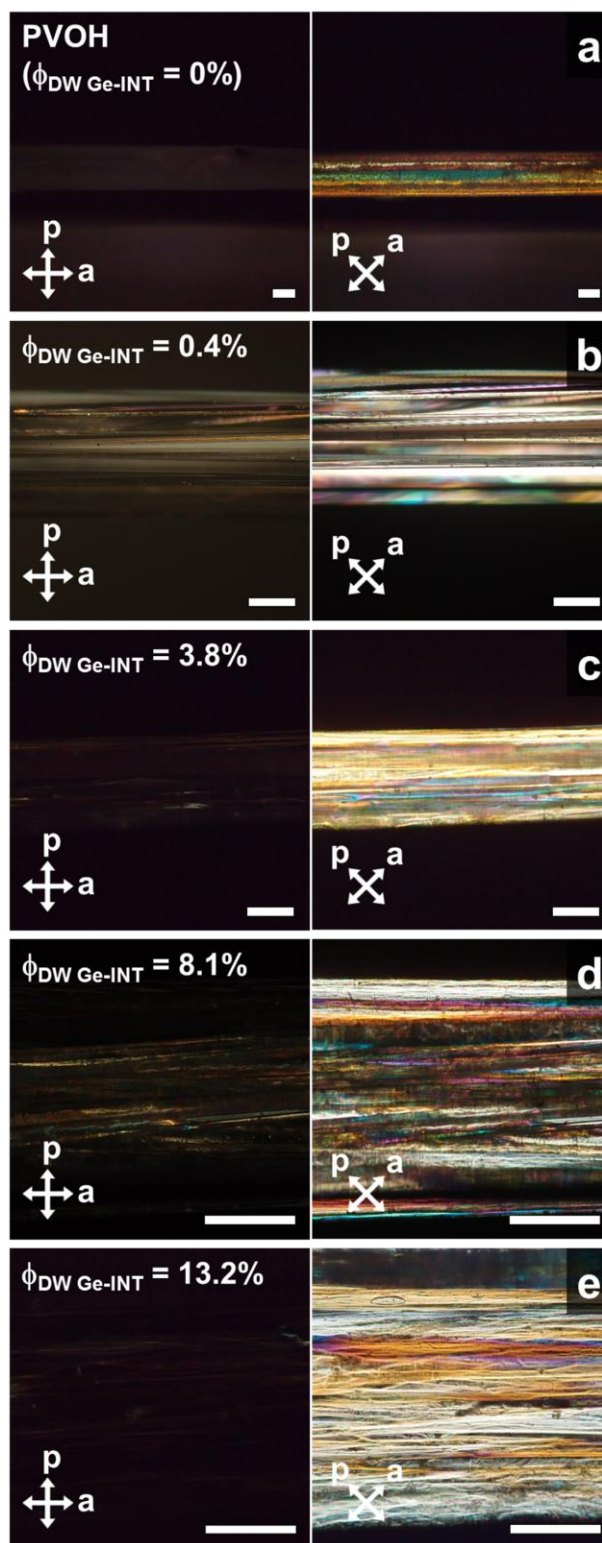


**Figure S4** Thermogravimetric analysis of double-walled aluminogermanate imogolite nanotube (DW Ge-INT)/polyvinyl alcohol (PVOH) composite fibers, pure PVOH fiber (control) and the as-synthesized DW Ge-INTs (black). PVOH fiber ( $\phi_{\text{DW Ge-INT}} = 0\%$ ), DW Ge INT/PVOH composite fibers: (red)  $\phi_{\text{DW Ge-INT}} = 0.4\%$ , (blue)  $\phi_{\text{DW Ge-INT}} = 3.8\%$ , (turquoise-green)  $\phi_{\text{DW Ge-INT}} = 8.1\%$ , (pink)  $\phi_{\text{DW Ge-INT}} = 13.2\%$ , and (black dotted) DW Ge-INTs ( $\phi_{\text{DW Ge-INT}} = 100\%$ , powder), carried out in nitrogen.



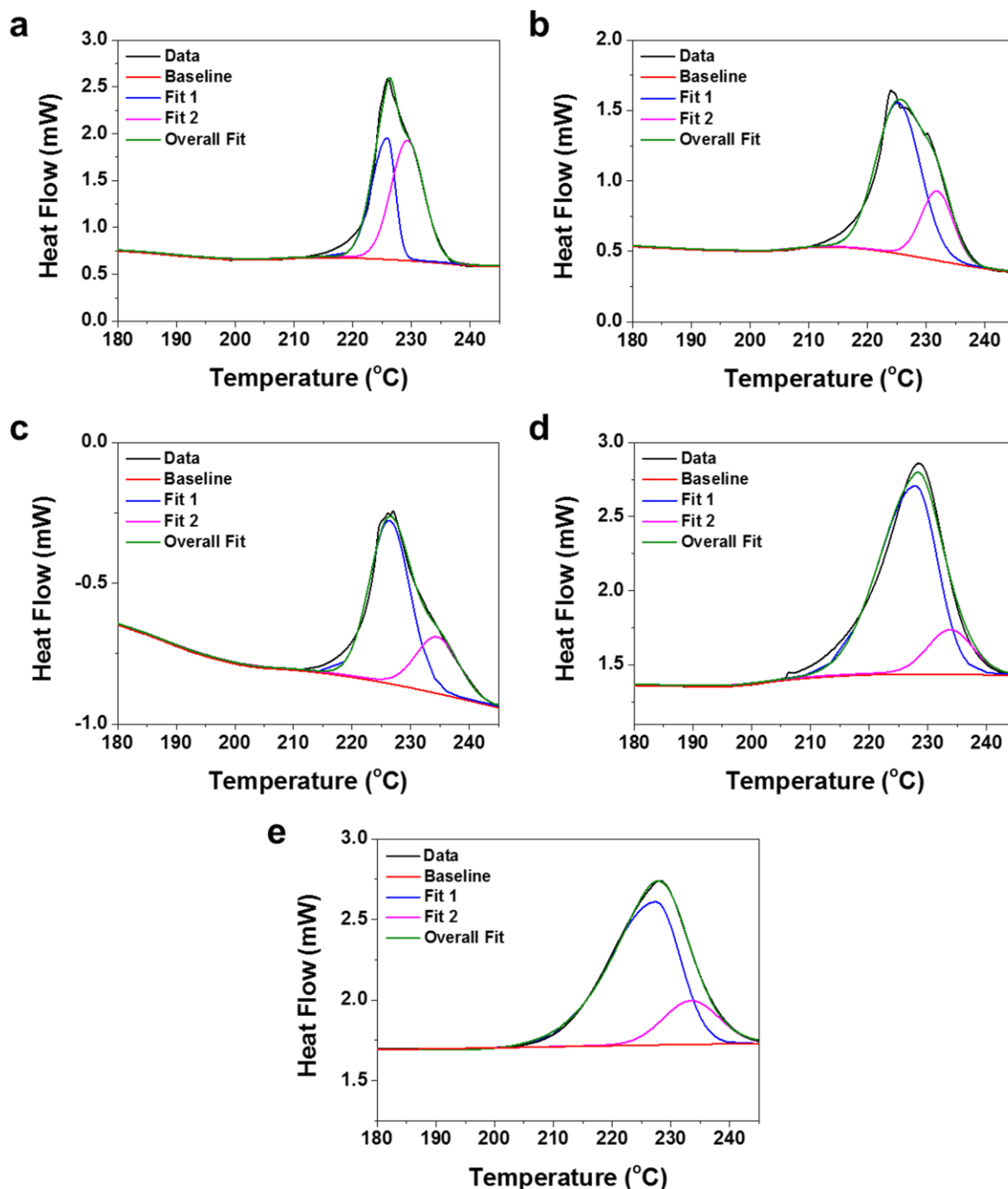
**Figure S5** Saturated water content of double-walled aluminogermanate imogolite nanotube (DW Ge-INT)/polyvinyl alcohol (PVOH) composite fibers, pure PVOH fiber (control, 0%) and as-synthesized DW Ge-INTs (control 100%), as determined by thermogravimetric analysis. The data indicate a lower uptake with increasing INT loading. (Dotted line is a guide for the eye).





**Figure S6** Cross-polarized optical microscopy (left  $0^\circ/90^\circ$ , right  $+45^\circ/-45^\circ$ ) images of double-walled aluminogermanate imogolite nanotube (DW Ge-INT)/polyvinyl alcohol (PVOH) composite fibers and pure PVOH fiber (control). (a) PVOH fiber ( $\phi_{\text{DW Ge-INT}} = 0\%$ ), DW Ge-INT/PVOH composite fiber (b)  $\phi_{\text{DW Ge-INT}} = 0.4\%$ , (c)  $\phi_{\text{DW Ge-INT}} = 3.8\%$ , (d)  $\phi_{\text{DW Ge-INT}} = 8.1\%$ , (e)  $\phi_{\text{DW Ge-INT}} = 13.2\%$ . 50  $\mu\text{m}$  scale bar for all frames.

## Crystallinity and composition of polyvinyl alcohol in wet-spun fibers



**Figure S7** Differential scanning calorimetry (DSC) thermographs of double-walled aluminogermanate imogolite nanotube (DW Ge-INT)/polyvinyl alcohol (PVOH) composite fibers and pure PVOH fiber (control). (a) PVOH fiber ( $\phi_{\text{DW Ge-INT}} = 0\%$ ), DW Ge-INT/PVOH composite fiber (b)  $\phi_{\text{DW Ge-INT}} = 0.4\%$ , (c)  $\phi_{\text{DW Ge-INT}} = 3.8\%$ , (d)  $\phi_{\text{DW Ge-INT}} = 8.1\%$ , (e)  $\phi_{\text{DW Ge-INT}} = 13.2\%$ . Fit 1 (blue), Fit 2 (pink) correspond to the melting and the decomposition peaks of PVOH, respectively. The DSC overall fit (green) includes the contribution of Fit 1 and Fit 2 in relation to the baseline fit (red) and can be compared to the experimental thermograph (black).

The degree of crystallinity of polyvinyl alcohol (PVOH) content in composite fiber was calculated using the following equation;

$$\chi_c = \frac{\Delta H_m}{\Delta H_0} \times 100, \quad (\text{S1})$$

where  $\chi_c$ ,  $\Delta H_m$  and  $\Delta H_0$  are the degree of crystallinity in weight percentage of the whole fiber, the measured melting endothermic enthalpy, and the theoretical melting enthalpy<sup>1</sup> of 100% crystalline PVOH (156 J g<sup>-1</sup>), respectively. As the addition of double-walled aluminogermanate imogolite nanotubes did not alter the melting temperature, it was considered not to provide a contribution to the measured melting endothermic enthalpy of the crystalline PVOH.

**Table S1** Composition and thermal data for double-walled aluminogermanate imogolite nanotube (DW Ge-INT)/polyvinyl alcohol (PVOH) composite fibers and pure PVOH fiber (control). Degree of crystallinity ( $\chi_c$ ), in weight fraction, determined through differential scanning calorimetry as described above. Linear density of the fibers, by direct measurement, as described elsewhere in the methods.

DW Ge-INT/PVOH fiber composition [vol.%]	Melting temperature [°C]	$\Delta H_m$ [J g <sup>-1</sup> ]	DW Ge-INT content [wt.%]	PVOH degree of crystallinity ( $\chi_c$ ) [wt.%]	PVOH amorphous content [wt.%]	Linear density ( $\delta_L$ ) [tex]
$\phi_{\text{DW Ge-INT}} = 0\%$	225.9	33.65	0.00	21.57	78.43	1.9
$\phi_{\text{DW Ge-INT}} = 0.4\%$	225.2	35.19	1.00	22.56	76.44	1.9
$\phi_{\text{DW Ge-INT}} = 3.8\%$	226.3	46.29	9.91	29.67	60.42	1.2
$\phi_{\text{DW Ge-INT}} = 8.1\%$	227.6	50.56	19.64	32.41	47.95	2.1
$\phi_{\text{DW Ge-INT}} = 13.2\%$	227.4	42.47	29.68	27.23	43.10	4.5



**Table S2** Composition, in volume fractions, of double-walled aluminogermanate imogolite nanotube (DW Ge-INT)/polyvinyl alcohol (PVOH) composite fibers and pure PVOH fiber (control) determined from the weight fractions in Table S1, and the material densities: 1.269 g cm<sup>-3</sup> and 1.345 g cm<sup>-3</sup> for amorphous PVOH and crystalline PVOH,<sup>2</sup> respectively; the DW Ge-INTs density, 3.6 g cm<sup>-3</sup> was calculated as the ratio between the mass of a nanotube over its period divided by the corresponding volume of the two walls of the nanotubes. Atomic positions were determined *via* wide angle X-ray scattering analysis,<sup>3</sup> and adjusted to account for H atoms<sup>4</sup> to which X-rays are rather insensitive. The composite fiber bulk density was calculated from the rule-of-mixtures (RoM) addition of the constituent densities. The linear fiber density (in tex, Table S1), was used to calculate the mechanical properties in N/tex directly (Table S5), which were then converted to mechanical properties in GPa, using the estimated composite fiber bulk density. For reference, the measured linear density in tex, and estimated bulk density, can be converted to an implied calculated mean fiber radius, shown in the Table below. Independent measurements of the nominal (circular) composite fiber radii determined by scanning electron microscopy are also tabulated and show reasonable agreement with the density derived values; however, the linear density approach is considered to be more accurate as it averages over the whole fiber sample, and underestimates rather than overestimates the mechanical properties when diameter varies.

DW Ge-INT/PVOH fiber composition [vol.%]	DW Ge-INT content [vol.%]	PVOH degree of crystallinity [vol.%]	PVOH amorphous content [vol.%]	Composite fiber bulk density ( $\delta_B$ ) [g cm <sup>-3</sup> ]	Calculated fiber radius [ $\mu$ m]	Nominal fiber radius from SEM [ $\mu$ m]
$\phi_{DW\ Ge-INT} = 0\%$	0.0	20.6	79.4	1.28	22	29
$\phi_{DW\ Ge-INT} = 0.4\%$	0.4	21.7	77.9	1.29	22	15
$\phi_{DW\ Ge-INT} = 3.8\%$	3.8	30.5	65.7	1.38	17	17
$\phi_{DW\ Ge-INT} = 8.1\%$	8.1	35.8	56.1	1.49	21	23
$\phi_{DW\ Ge-INT} = 13.2\%$	13.2	32.4	54.4	1.60	30	25

The volume fraction of DW Ge-INTs in the composite fibers is given by;

$$\phi_{DW\ Ge-INT} = \frac{\frac{wt.\% [DW\ Ge-INT]}{\delta [DW\ Ge-INT]}}{\frac{wt.\% [DW\ Ge-INT]}{\delta [DW\ Ge-INT]} + \frac{wt.\% [crystalline\ PVOH]}{\delta_B [crystalline\ PVOH]} + \frac{wt.\% [amorphous\ PVOH]}{\delta_B [amorphous\ PVOH]}} \quad (S2)$$

where wt.% is weight percentage,  $\delta$  is density, and  $\delta_B$  is bulk density.

## Orientalional order parameter determination for double-walled aluminogermanate imogolite nanotube and polyvinyl alcohol fibers

As detailed in the manuscript, for the wide-angle X-ray scattering experiments, the angular scattered intensity  $Q$  values at 0.6 and 1.4  $\text{\AA}^{-1}$  correspond to scattering features located in the equatorial plane perpendicular to the double-walled aluminogermanate imogolite nanotubes (DW Ge-INTs) and polyvinyl alcohol (PVOH) long axes, respectively. Azimuthal scans,  $I_Q(\tau)$ , in Figure S8 of the composite fibers, are fitted by Lorentzian functions, characterized by their half-width-at-half-maximum (HWHM,  $w_d$ ), plus two Gaussian functions at  $\pm 28^\circ$  from the Lorentzian for DW Ge-INT/PVOH  $\phi_{\text{DW Ge-INT}} = 13.2\%$  composite fiber. Note that due to the overlap of the diffuse peak of amorphous PVOH and  $10\bar{1}$  and  $101$  peaks of crystalline PVOH, amorphous and crystalline contributions cannot be clearly assigned. Angular intensity distribution measured in reciprocal space can be directly calculated from the orientation distribution function  $p(\theta)$  in direct space, with  $\theta$  being the angle between the wet-spun fiber axis and the nanotube (or PVOH) long axis<sup>5</sup>;

$$I_Q(\tau) \propto \int_0^{90} p[\cos^{-1}\{\cos(\xi) \sin(\cos^{-1}[\cos(\theta_B) \cos(\tau)])\}] d\xi, \quad (\text{S3})$$

where  $\tau$ ,  $\theta_B$  and  $\xi$  are the azimuthal angle, Bragg angle and a variable, respectively. Lorentzian curves in Figure S8 are well reproduced for Lorentzian functions to the power 1.5 in direct space ( $L_{w_d}^{3/2}$ ), so that;

$$p(\theta) = \frac{L_{w_d}^{3/2}(\theta)}{4\pi \int_0^{90} L_{w_d}^{3/2}(\theta) \sin(\theta) d\theta}, \quad (\text{S4})$$

with,

$$L_{w_d}^{3/2}(\theta) = \frac{1}{\left[1 + \left(\frac{0.7664\theta}{w_d}\right)^2\right]^{1.5}} \quad (0 \leq \theta \leq 90^\circ). \quad (\text{S5})$$

Finally, one calculates the orientational order parameter;

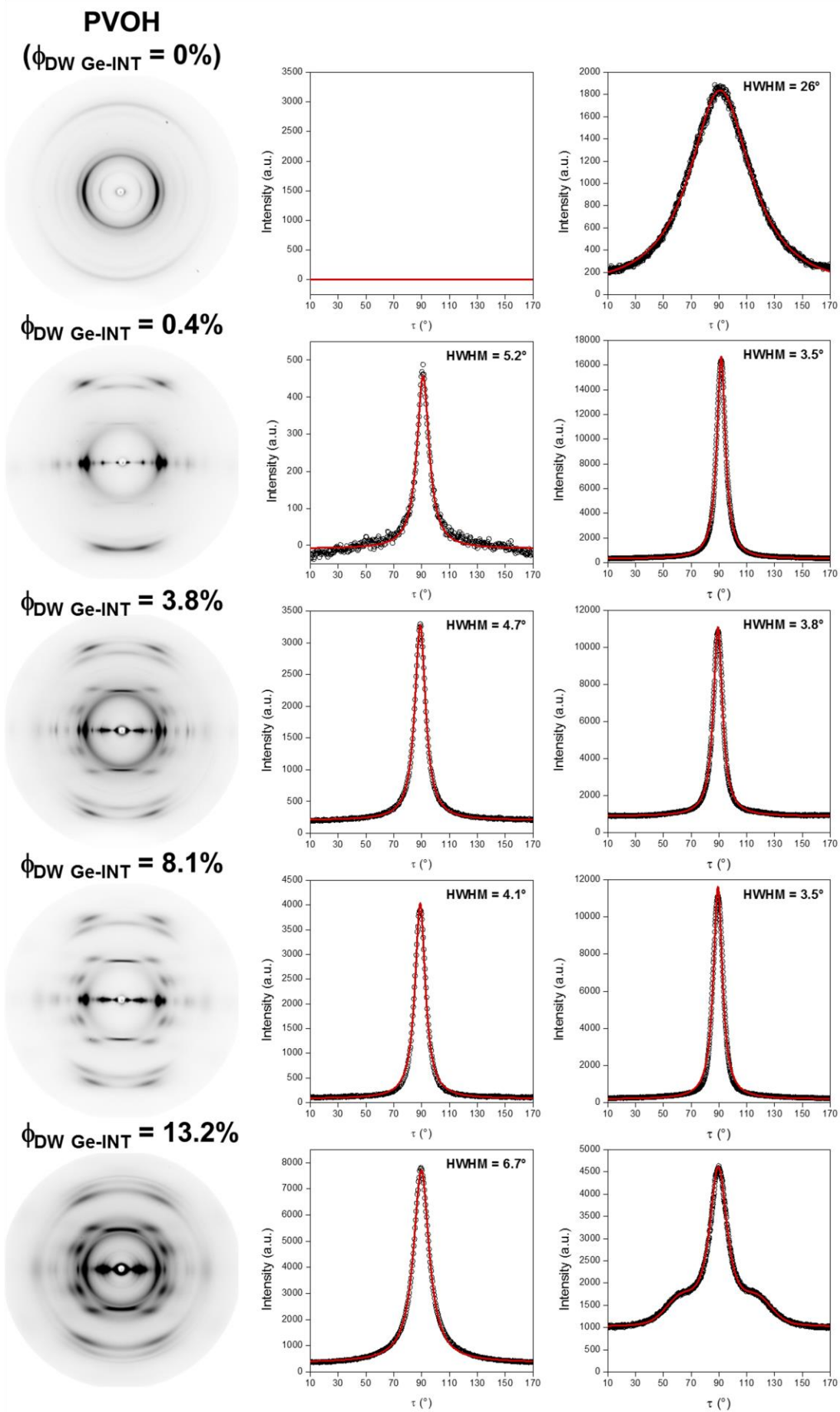
$$S = \left\langle \frac{3\cos^2(\theta) - 1}{2} \right\rangle = \frac{12\pi \int_0^{90} p(\theta) \cos^2(\theta) \sin(\theta) d\theta - 1}{2}. \quad (\text{S6})$$

Table S3 provides the values of the HWHM of the Lorentzian orientational distribution of DW Ge-INTs and PVOH, as well as the calculated values of  $S$ . In the case of the  $\phi_{\text{DW Ge-INT}} = 13.2\%$  fiber, for  $Q = 1.4 \text{\AA}^{-1}$ , the distribution of intensity in reciprocal space is notably different from the one at  $Q = 0.6 \text{\AA}^{-1}$ . It is found to be fitted by the following sum of a Lorentzian function and of two Gaussian functions:

$$I_Q(\tau) \propto \frac{1}{1 + \left(\frac{\tau - 90.}{8}\right)^2} + 0.13e^{-\ln 2 \left(\frac{\tau - 62.}{12}\right)^2} + 0.13e^{-\ln 2 \left(\frac{\tau - 108.}{12}\right)^2}, \quad (\text{S7})$$

with the corresponding orientational distribution function described as

$$p(\theta) \propto \frac{1}{\left[1 + \left(\frac{0.7664\theta}{6}\right)^2\right]^{1.5}} + 0.04e^{-\ln 2 \left(\frac{\theta - 34.}{9}\right)^2} \quad (0 \leq \theta \leq 90^\circ). \quad (\text{S8})$$

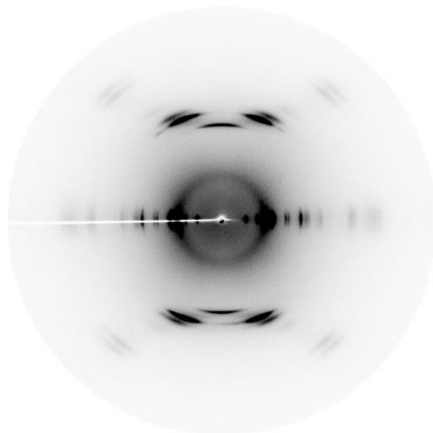


**Figure S8** Characterization of the orientation parameters of the constituents in double-walled aluminogermanate imogolite nanotube (DW Ge-INT)/polyvinyl alcohol (PVOH) composite fibers and pure PVOH fiber (control,  $\phi_{\text{DW Ge-INT}} = 0\%$ ). Left column: Two dimensional wide-angle X-ray scattering pattern, center column: angular scattered intensity at  $Q = 0.6 \text{ \AA}^{-1}$  corresponding to a maximum of the form factor of DW Ge-INT and angular scattered intensity at  $Q = 1.4 \text{ \AA}^{-1}$ , corresponding to the diffraction from crystalline and amorphous PVOH. Experimental values (open black circles) and Lorentzian fitting (red line), with corresponding HWHM, provided. In the case of the DW Ge-INT/PVOH composite fiber  $\phi_{\text{DW Ge-INT}} = 13.2\%$ , the fit was performed with a Lorentzian function (HWHM =  $8^\circ$ ) and two Gaussian functions (HWHM =  $12^\circ$ ) at  $62^\circ$  and  $118^\circ$ , following Equation S8.

**Table S3** Determination of the orientation order parameters,  $S$ , for double-walled aluminogermanate imogolite nanotube (DW Ge-INT)/polyvinyl alcohol (PVOH) composite fibers and pure PVOH fiber ( $\phi_{\text{DW Ge-INT}} = 0\%$ ) from angular scattered intensity plots shown in Figure S8. Half-width-at-half-maximum (HWHM,  $w_d$ ) are reported for fitting Lorentzian functions to the power 1.5, which describe the orientation distribution functions in direct space, and allow the fitting of the azimuthal curves at  $Q = 0.6$  and  $1.4 \text{ \AA}^{-1}$ , which correspond to DW Ge-INTs and PVOH scattering, respectively. In the specific case of DW Ge-INT/PVOH  $\phi_{\text{Ge-INT}} = 13.2\%$  composite fibers, the orientation distribution function is found to be given by the sum of two functions, a Lorentzian function to the power 1.5 (HWHM =  $6^\circ$ ) and a Gaussian function centered at  $\theta \approx 34^\circ$ , with HWHM =  $9^\circ$ , Equation S8. Moreover, in this case only, one cannot rule out the possibility that a fraction of the PVOH molecules is fully disoriented (see reference Pichot *et al.*<sup>5</sup> for more details on the related two-phases), so that the calculated orientation parameter value reported in the table is only an upper limit. Accuracy on the values of the orientation order parameter  $S_{\text{INT}}$  ( $S_{\text{PVOH}}$ ) is mainly limited by uncertainties in the values of HWHM, determined by performing azimuthal scans at other  $Q$ -values where INT and PVOH contributions are dominant. A value of unity would signify full alignment of the species with respect to the fiber axis.

DW Ge-INT/PVOH fiber composition [vol.%]	$w_d$ ( $^\circ$ ) DW Ge-INT	$w_d$ ( $^\circ$ ) PVOH	$S_{\text{DW Ge-INT}}$	$S_{\text{PVOH}}$
$\phi_{\text{DW Ge-INT}} = 0\%$	NA	20.0	NA	$0.50 \pm 0.05$
$\phi_{\text{DW Ge-INT}} = 0.4\%$	4.0	2.6	$0.86 \pm 0.05$	$0.91 \pm 0.05$
$\phi_{\text{DW Ge-INT}} = 3.8\%$	3.6	2.9	$0.87 \pm 0.05$	$0.90 \pm 0.05$
$\phi_{\text{DW Ge-INT}} = 8.1\%$	3.1	2.6	$0.89 \pm 0.05$	$0.91 \pm 0.05$
$\phi_{\text{DW Ge-INT}} = 13.2\%$	5.1	-	$0.83 \pm 0.05$	$\leq 0.7$

The crystallite size in the DW Ge-INTs/PVOH composite fiber ( $\phi_{\text{DW Ge-INT}} = 3.8\%$ ) reported in Figure 1 was compared that obtained from a diffraction experiment on a conventional, commercial PVOH fiber reference (Figure S9).



**Figure S9** Two dimensional wide angle X-ray scattering pattern of a commercial PVOH fiber Kuralon 1239, manufactured by Kuraray Co. Ltd.

**Table S4** Full-width-at-half-maximum (FWHM) and the average crystallite size (L) estimated using the Scherrer equation for crystal axes 001 or 200, for a commercial PVOH fiber (Kuralon 1239) and a wet-spun DW Ge INTs/PVOH composite fiber ( $\phi_{\text{DW Ge-INT}} = 3.8\%$ ).

	<b>FWHM_001</b> <b><math>Q_{001} = 1.145</math></b> <b><math>[\text{\AA}^{-1}]</math></b>	<b>FWHM_200</b> <b><math>Q_{200} = 1.6</math></b> <b><math>[\text{\AA}^{-1}]</math></b>	<b>L<sub>001</sub></b> <b>[nm]</b>	<b>L<sub>200</sub></b> <b>[nm]</b>
Kuralon 1239	0.057	0.065	22	20
$\phi_{\text{DW Ge-INT}} = 3.8\%$	0.038	0.05	33	26

## Mechanical modelling equations, tabulated data and healed composite fiber stress-strain curves

The tensile stiffness of double-walled aluminogermanate imogolite nanotube (DW Ge-INT)/polyvinyl alcohol (PVOH) composite fibers can be predicted using the well-known rule-of-mixtures (RoM). However, when the reinforcing components are anisotropic, additional efficiency factors are required to take into account orientation and stress transfer variations. Krenchel's modified RoM equation is given below:

$$E = \eta_0 \eta_{l_{\text{DW Ge-INT}}} \phi_{\text{DW Ge-INT}} E_{\text{DW Ge-INT}} + \phi_m E_m, \quad (\text{S9})$$

where  $\eta_0$ ,  $\eta_{l_{\text{DW Ge-INT}}}$  are efficiency factors relating to DW Ge-INT orientation and length,  $\phi_{\text{DW Ge-INT}}$ ,  $\phi_m$  are volume fraction of DW Ge-INT and matrix, and  $E$ ,  $E_{\text{DW Ge-INT}}$ ,  $E_m$  are the moduli (in GPa) of composite fiber, DW Ge-INT and matrix, respectively. The DW Ge-INT orientation efficiency factor ( $\eta_0$ )<sup>6</sup> and the DW Ge-INT efficiency length factor ( $\eta_{l_{\text{DW Ge-INT}}}$ )<sup>7</sup> are given by;

$$\eta_0 = \langle \cos^4 \theta \rangle \quad (\text{S10})$$

$$\eta_{l_{\text{DW Ge-INT}}} = 1 - \frac{\tanh \beta}{\beta} \quad (\text{S11})$$

where,

$$\beta = 2 \frac{l_{\text{DW Ge-INT}}}{D} \sqrt{\frac{G_m}{E_{\text{DW Ge-INT}} \ln\left(\frac{K_R}{\phi_{\text{DW Ge-INT}}}\right)}} \quad (\text{R01})$$

where  $\theta$  is taken from the azimuthal curves at  $Q = 0.6$ , and  $l_{\text{DW Ge-INT}}$  and  $D$  are DW Ge-INT length (c.a. 85 nm) and diameter (c.a. 4.3 nm).<sup>8</sup>  $G_m$  is the shear modulus of the matrix in GPa (ca. 1.7 GPa for PVOH),<sup>9</sup> and  $K_R$  is a constant equal to 1 for cylinders in shear lag models.<sup>10</sup>

However, when Equation S9 was used, fitting a single semi-crystalline PVOH modulus (10-30 GPa)<sup>11</sup>, there was a poor fit to the data. Additional consideration of the varying crystalline/amorphous proportions was required to gain a good fit. The crystalline to amorphous content in composite fibers was determined *via* differential scanning calorimetry, Figure S7.

Krenchel's model was then adapted as follows:

$$E = \eta_0 \eta_{l_{\text{DW Ge-INT}}} \phi_{\text{DW Ge-INT}} E_{\text{DW Ge-INT}} + \phi_{\text{m.a}} E_{\text{m.a}} + \phi_{\text{m.c}} E_{\text{m.c}}, \quad (\text{S13})$$

where  $\phi_{\text{m.a}}$ ,  $\phi_{\text{m.c}}$  are volume fractions of amorphous and crystalline PVOH matrix, and  $E_{\text{m.a}}$ ,  $E_{\text{m.c}}$  are the moduli of amorphous and crystalline PVOH, respectively.

Assuming,

$$V_f + V_{\text{m.a}} + V_{\text{m.c}} = 1, \quad (\text{S14})$$

where  $V_f$ ,  $V_{\text{m.a}}$  and  $V_{\text{m.c}}$  are volume fractions of imogolite reinforcement, amorphous matrix and crystalline matrix, respectively.



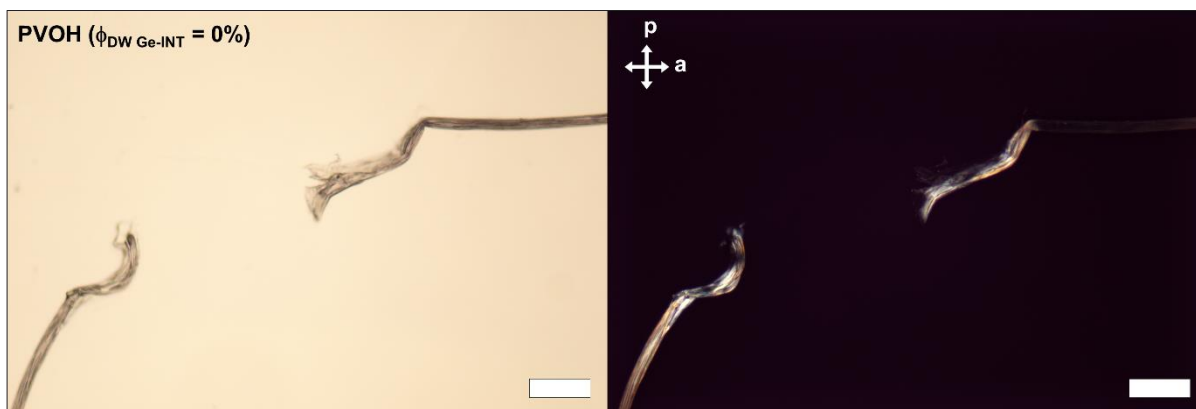
The moduli substituted into Equation S13 were 328 GPa,<sup>12</sup> 3.75 GPa,<sup>13</sup> 37 GPa<sup>14</sup> for DW Ge-INT ((12,0)@(21,0)), amorphous and crystalline PVOH, respectively. The volume fractions of PVOH and DW Ge-INT were determined from weight fractions added to the spinning dope and the material densities, 3.6 g cm<sup>-3</sup>, 1.269 g cm<sup>-3</sup> and 1.345 g cm<sup>-3</sup> for DW Ge-INTs (details on page 9, Supporting Information), amorphous PVOH and crystalline PVOH,<sup>2</sup> respectively.

**Table S5** Tabulated tensile properties of double-walled aluminogermanate imogolite nanotube (DW Ge-INT)/polyvinyl alcohol (PVOH) composite fibers and pure PVOH fiber (control,  $\phi_{\text{DW Ge-INT}} = 0\%$ ), with Krenchel's micromechanical reinforcing efficiency factors, and the resulting tensile modulus determined from the modified rule-of-mixtures (RoM).

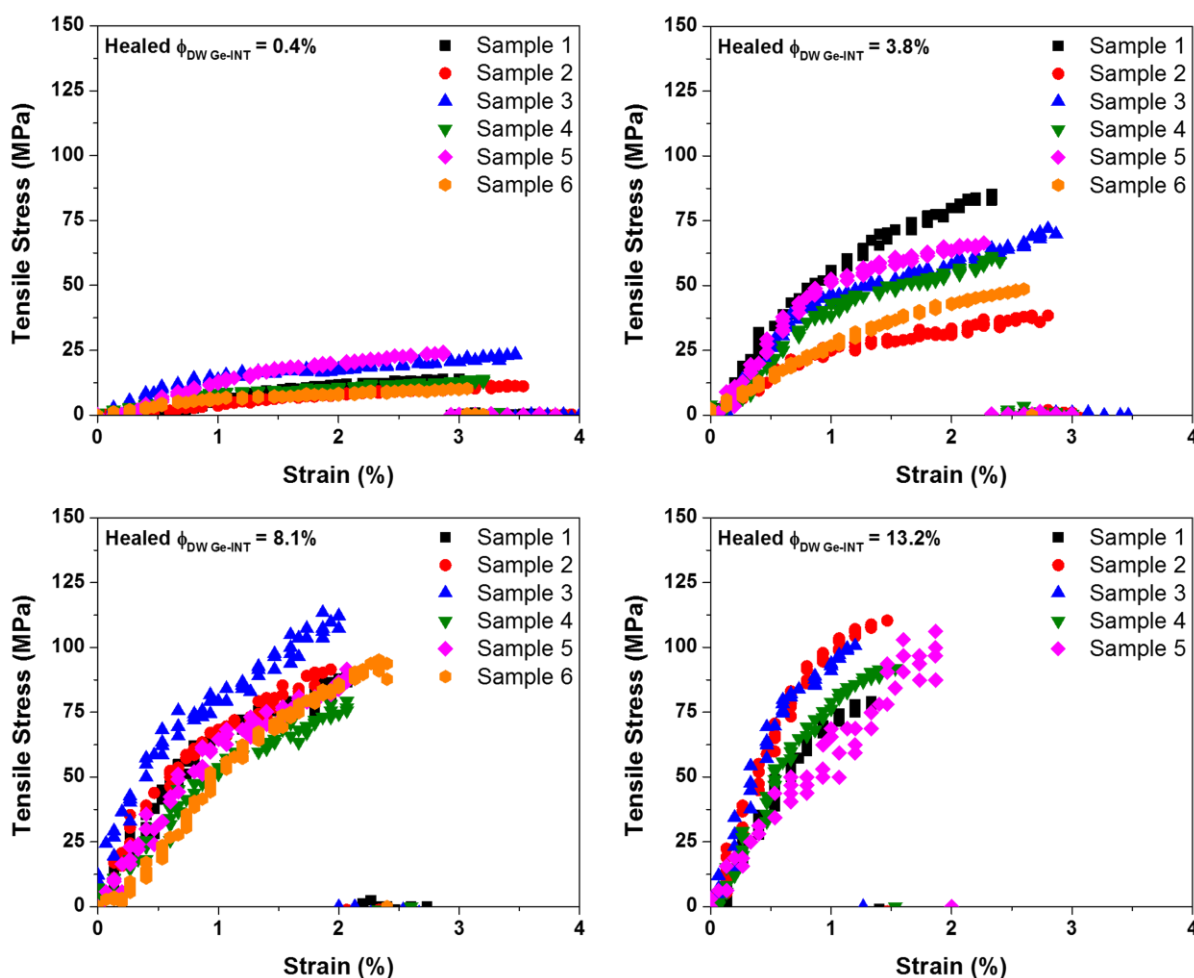
DW Ge-INT/PVOH composite fibers [vol.%]	Tensile modulus ( $E$ ) [N tex <sup>-1</sup> ]	Tensile strength ( $\sigma$ ) [N tex <sup>-1</sup> ]	Tensile modulus ( $E$ ) [GPa]	Tensile strength ( $\sigma$ ) [MPa]	Strain -to- failure ( $\epsilon$ ) [%]	RoM tensile modulus [GPa]
$\phi_{\text{DW Ge-INT}} = 0\%$	$7.49 \pm 1.49$	$0.45 \pm 0.08$	$9.87 \pm 2.61$	$603 \pm 71$	$9.0 \pm 1.5$	10.6
$\phi_{\text{DW Ge-INT}} = 0.4\%$	$10.10 \pm 0.83$	$0.43 \pm 0.05$	$13.27 \pm 0.83$	$559 \pm 64$	$6.9 \pm 0.5$	11.2
$\phi_{\text{DW Ge-INT}} = 3.8\%$	$12.32 \pm 1.24$	$0.47 \pm 0.04$	$18.79 \pm 1.24$	$712 \pm 68$	$5.9 \pm 0.4$	18.1
$\phi_{\text{DW Ge-INT}} = 8.1\%$	$14.09 \pm 1.81$	$0.45 \pm 0.03$	$24.11 \pm 1.81$	$794 \pm 56$	$5.4 \pm 0.5$	26.1
$\phi_{\text{DW Ge-INT}} = 13.2\%$	$9.31 \pm 2.65$	$0.25 \pm 0.05$	$18.58 \pm 2.65$	$506 \pm 99$	$5.8 \pm 1.4$	31.7

**Table S6** Tabulated tensile properties of healed composite fibers. The polyvinyl alcohol control could not be healed using the same procedure.

DW Ge-INT/PVOH composite fibers [vol.%]	Tensile modulus ( $E$ ) [GPa]	Tensile strength ( $\sigma$ ) [MPa]	Strain -to- failure ( $\epsilon$ ) [%]	Stiffness healing efficiency ( $\alpha_E$ ) [%]	Strength healing efficiency ( $\alpha_\sigma$ ) [%]
$\phi_{\text{DW Ge-INT}} = 0\%$	NA	NA	NA	NA	NA
$\phi_{\text{DW Ge-INT}} = 0.4\%$	$1.19 \pm 0.52$	$16.10 \pm 5.50$	$3.19 \pm 0.24$	8.94	2.88
$\phi_{\text{DW Ge-INT}} = 3.8\%$	$4.84 \pm 1.47$	$61.72 \pm 15.30$	$2.53 \pm 0.21$	25.75	8.67
$\phi_{\text{DW Ge-INT}} = 8.1\%$	$6.76 \pm 0.95$	$93.10 \pm 9.85$	$2.10 \pm 0.15$	28.05	11.72
$\phi_{\text{DW Ge-INT}} = 13.2\%$	$8.10 \pm 1.78$	$97.65 \pm 11.08$	$1.48 \pm 0.22$	43.57	19.30



**Figure S10** Transmission optical micrographs under normal illumination (left) and with crossed polarizers (right), showing the response of PVOH fiber ( $\phi_{\text{DW Ge-INT}} = 0\%$ ) under ‘healing conditions’, including contraction and distortion, 100  $\mu\text{m}$  scale bar for both micrographs.



**Figure S11** Tensile stress-strain curves for healed composite fibers double-walled aluminogermanate imogolite nanotube (DW Ge-INT)/polyvinyl alcohol (PVOH) composite fibers.

**Table S7** Tensile mechanical properties of healed materials found in literature. Tensile modulus ( $E$ ), ultimate tensile stress (UTS), strain-to-failure ( $\epsilon$ ), healing time ( $\alpha_{\text{time}}$ ), healing temperature ( $\alpha_{\text{Temp.}}$ ), stiffness healing efficiency ( $\alpha_E$ ), UTS healing efficiency ( $\alpha_{\sigma\text{UTS}}$ ), strain-to-failure healing efficiency ( $\alpha_\epsilon$ ). Dimensions when provided, length x width x thickness (l x w x t), with yarn and dog bone (DG) sample geometries indicated and gauge region detailed if specified. Cross sectional area (CSA) provided in lieu of overall/gauge dimensions where available.

Initial $E$	Initial $\sigma_{\text{UTS}}$	Initial $\epsilon$	$\alpha_{\text{time}}$	$\alpha_{\text{Temp.}}$	Healed $E$	Healed $\sigma_{\text{UTS}}$	Healed $\epsilon$	$\alpha_E$	$\alpha_{\sigma\text{UTS}}$	$\alpha_\epsilon$	Dimensions (Standard)	Ref.
[GPa]	[MPa]	[%]	[h]	[°C]	[GPa]	[MPa]	[%]	[%]	[%]	[%]	[mm]	[#]
0.269	10.6	84	14	21		11.8	7.4		111.3	8.8	3 x 10 x 0.25	15
0.261	3.25	22.5	0.333	85	0.150			57.5			30.0 x 3.3 x 0.150	16
0.239	25.0	138	0.5/24	130/50	0.228	17.0	50.0	95.4	68.0	36.2		17
0.209	7.09	54	4/24	150/65	0.111	5.21	30.0	53.3	73.5	55.6	35 x 6 x 0.1-0.5 (DG)	18
0.141	11.20	610	14	21		8.40	430.0		75.0	70.5	3 x 10 x 0.25	15
0.075	0.41	750	0.083	25	0.070	0.40	750.0	93.3	97.6	100.0	Yarn	19
0.066	5.0	583	14	21		3.5	346.0		70.0	59.3	3 x 10 x 0.25	15
0.036	3.77	3.1	24	25		2.50	240.0		66.3	7741.9		20
0.022	8.01	449	4/24	150/65	0.016	5.70	275.0	71.0	71.2	61.2	35 x 6 x 0.1-0.5 (DG)	18
0.017	1.92	780	24	25		1.75	720.0		91.1	92.3		20
0.012	0.27	897	24	30		0.29	817.0		107.4	91.1	20 x 6 x 2 (Gauge 12 x 2 [l x w], D)	21
0.011	4.23	310	24	20	0.011	2.08	44.0	99.1	49.2	14.2	12 x 2 x 1 (D)	22
0.004	9.5	1450	3	25		9.0	1450.0		94.7	100.0	5 x 0.5 [w x l]	23
0.004	15.2	1053	5	25		7.0	700.0		46.1	66.5	5 x 0.5 [w x l]	23
0.0010			0.083	80	0.001			100.0			40 x 3.5 x 0.10	24
0.0009	3.7	115	24	22		2.1	75.0		56.8	65.2	ASTM D638-10 (type IV)	25
0.0008	0.35	250	16	25		0.35	230.0		100.0	92.0		26

**Table S8** Tensile mechanical properties of self-healing materials (continued).

<b>Initial</b> <i>E</i>	<b>Initial</b> $\sigma_{UTS}$	<b>Initial</b> $\epsilon$	$\alpha_{time}$	$\alpha_{Temp.}$	<b>Healed</b> <i>E</i>	<b>Healed</b> $\sigma_{UTS}$	<b>Healed</b> $\epsilon$	$\alpha_E$	$\alpha_{\sigma_{UTS}}$	$\alpha_{\epsilon}$	<b>Dimensions</b> <b>(Standard)</b>	<b>Ref.</b>
[GPa]	[MPa]	[%]	[h]	[°C]	[GPa]	[MPa]	[%]	[%]	[%]	[%]	[mm]	[#]
0.0005	0.23	1860	48	25		0.23	1750.0		97.8	94.1	75 x 14 x 1.0 (Gauge 2 [I])	27
0.0005	6.4	+200	0.05			0.005	+200	94.1	97.8			28
0.0003	1.6	327	24	22		1.8			112.5		ASTM D638-10 (type IV)	25
0.0002	0.13	827	28								10 mm diameter	29
	4.5		0.15	150		10.0			222.2		25.4 x 10 x 5	30
	4.4	58	72	20		4.0	55.0		90.9	94.8		31
	3.5	650	3	20		2.8	525.0		80.0	80.8	ISO 527-3	32
	2.1	700	24	25		1.65	625.0		78.6	89.3	1 [t] (Gauge 30 [I], DG)	33
	0.9	165	120	20		0.30	48.0		33.3	29.1	JIS K 7113 (No. 2 (1/5))	34
	0.81	3100	24	25		0.77	3015.0		95.1	97.3	2 [t] (D)	35
	0.75	850	0.001	25		0.55	800.0		73.3	94.1		36
	0.75	830	72	50		0.80	850.0		106.7	102.4	12 x 2 x 0.5-0.7 (ISO 37-4)	37
	0.75	830	12	50		0.72	840.0		96.0	101.2	12 x 2 x 0.5-0.7 (ISO 37-4)	37
	~ 0.7	32.5	0.083	50		~ 0.8	32.5		<100	100.0	ASTM D638	38
	~0.5	17	0.017	~200		~0.5	17.0		~100	100.0	0.325-0.400 [t]	39
	0.45	425	24	25		0.40	260.0		88.9	61.2	ISO 527-3	40
	0.17	8	24	20		~0.2	13.0		<100	162.5	CSA $\approx$ 12 mm <sup>2</sup> (D)	41
	0.06		24			0.04			63.6			42

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