Abstract—Six degree-of-freedom (DoF) pose feedback is essential for the development of closed-loop control techniques for microrobotics. This paper presents two methods for depth estimation of transparent microrobots inside an Optical Tweezers (OT) setup using image sharpness measurements and model-based tracking. The $x$-$y$ position and the 3D orientation of the object are estimated using online model-based template matching. The proposed depth estimation methodologies are validated experimentally by comparing the results with the ground truth.

I. INTRODUCTION

Examining cells on an individual basis provides insights into their mechanical behaviour since properties such as Young’s modulus are useful in determining cell pathology [1]. Precise cell manipulation could also improve procedures, such as in-vitro fertilization. OT are capable of highly precise and multi-point actuation. However, direct cell manipulation with the laser can cause photodamage. To avoid this problem, microrobots can be fabricated to handle the cell indirectly.

Three-dimensional visual feedback of microrobots is necessary in order to develop microrobotic systems with manipulation capabilities comparable to that of large-scale robotic systems. Depth estimation techniques proposed for the macro-scale cannot be directly applied to the micro-scale due to the difference in the projection model that describes the microscope-camera system. In addition, in most microscope set-ups only one camera view is available.

Model-based approaches, using the microrobot’s geometrical design as reference, estimate the microstructure’s pose for assistance in microassembly [2], [3]. Shape estimation for haptic feedback has also been considered in [4]. A CAD-based optimization solution is proposed in [5] for intraocular microrobot localization. In [6], the velocity of helical micro-swimmers along the microscope z-axis is estimated for surface reconstruction using prior calibration of the microrobot’s velocity along the z-axis. Depth recovery has been investigated for set-ups inside a Scanning Electron Microscope (SEM) [7]. Cui et al. [8] have proposed a method for estimating the 3D position and the rotation on the x-y plane. In [9], estimation of multiple depths for objects in different heights within the scene is performed using the sharpness measurements locally in the image. Other applications include depth recovery of microgrippers and Carbon Nanotubes (CNT) for automation purposes using variance-based sharpness calculations [10].

One difference between the SEM and the optical microscope set-up is that object transparency is visible in the latter. The transparency issue cannot be overcome by 3D-printing opaque objects since modifying the fabrication properties with respect to transparency has an impact on the relative refractive index between the object and the medium. As a result, features from within the micro-object are observable and therefore the sharpness measurement is a combination of overlapping depths. Hence, in optical micromanipulation the relative refractive index is directly connected to the amplitude of the grasping force by the laser beam. A transparent object complicates the pose estimation, nonetheless and crucially, less transparent or opaque objects hinder trapping force due to the refractive index.

In this paper, two methods for depth estimation of 3D-printed transparent microstructures within an OT set-up is proposed, which incorporates position tracking and model-based 3D orientation estimation. Two methods are presented; I) using the overall sharpness of the image frame which corresponds to features in multiples depths from within the object and II) utilizing the local sharpness around distinct features for single depth recovery at specific regions of the object. The first method aims to provide an overall measurement for the $z$-displacement of the object, while the second takes into account local changes of sharpness which might be attributed to object 3D rotation rather than displacement along the microscope $z$-axis. The second method takes into account the estimated orientation of the microstructure as proposed in [11]. The motivation for the global and the local approach stems from the fact that the overall sharpness measure can not infer directly the depth of a 3D microstructure in case of simultaneous 3D translation and rotation. The proposed methodology is validated through experimental results which are compared with ground truth data.

II. DEPTH ESTIMATION

A. Framework Overview

This section presents an overview of the proposed methodology for recovering the 3D pose of optically transparent laser-driven microrobots in an OT set-up. The main issues that are addressed are the unobservable motion along the $z$-axis and object transparency.

The first method presented in Section II-C describes a strategy for recovering the $z$-translation of a co-ordinate frame attached to the microstructure with respect to the focus plane. This strategy requires calibration for estimating the global sharpness model as a function of a single depth value that describes the object displacement along the microscope $z$-axis (Section II-C.1). By the term global sharpness model, we refer to the function that maps a sharpness value to
the corresponding object z position relative to the focus plane approximated by a sum of Gaussian curves. The object depth is reconstructed by the set of functions derived from the calibration routine as explained in Section II-C.2. This method gives a depth estimation that describes the overall object displacement.

The second method attempts to estimate a local sharpness model for single features. By the term local sharpness, we denote the approximation of the mapping function that relates a single sharpness value to the corresponding depth of an individual object feature by one Gaussian curve. A calibration routine is also performed in this case for a number of object features (Section II-D.1). The corresponding local depths are estimated by solving an optimization problem as described in Section II-D.2.

The motivation for developing these two methods is that the first method does not tackle the problem of interfering object features at different depths that are visible due to transparency. In addition, a holistic focus measurement cannot distinguish whether changes in the sharpness are cause by displacement along the z-axis or by 3D object rotation, as this motion also results to parts of the object being focused or defocused.

B. Projection Model

The projection of a 3D point on the image plane by the microscope-camera system is described by the parallel projection model. We assume a known CAD model for the object. Let $\mathbf{P}_{\text{M}_i} \in \mathbb{R}^3$, $i = 1, \ldots, N$ be the $i_{th}$ vertex of the registered geometrical model expressed with respect to a fixed global co-ordinate frame and $\mathbf{P}_{\text{c}_i} \in \mathbb{R}^2$, $i = 1, \ldots, N$ be the corresponding projection of the $i_{th}$ point on the image plane. Hence, the projection $\mathbf{P}_{\text{c}_i}$ is equal to

$$
\mathbf{P}_{\text{c}_i} = KP(R\mathbf{P}_{\text{M}_i} + t)
$$

$$
K = \begin{bmatrix} p_x & 0 & 0 \\ 0 & p_y & 0 \\ 0 & 0 & 1 \end{bmatrix}, P = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \end{bmatrix}
$$

with $K$ the intrinsic parameters of the microscope-camera system, $P$ the projection matrix, $R \in \mathbb{R}^{3 \times 3}$ the rotation matrix that describes the object’s orientation and $t \in \mathbb{R}^3$ the object’s translation with respect to the global frame. As seen from the third column of matrix $P$ in (2), the translation along the z-axis is not observable.

In the Sections II-C and II-D, the depth information is estimated using image sharpness measurements and the information derived from the model-based orientation estimation. It is worth noting that the transparency of the object must be taken into consideration when using sharpness measurements to recover the three-dimensional position of the microrobot in an OT environment.

C. Depth estimation using global sharpness model approximation

The first method aims to reconstruct the overall z-displacement of the object by using a global representation of the sharpness model. The full image feed is used for the sharpness calculation.

In order to estimate the translation along the z-axis of the object, the mapping between the sharpness measurement for each image frame and the corresponding z-position of the object must be established. The focus measure $\phi$ that is used in this case is the Gaussian Derivative [12]:

$$
\phi = \sum (I * G_x)^2 + (I * G_y)^2 \quad, \quad G(x,y) = \frac{1}{2\pi\sigma^2}e^{-\frac{x^2+y^2}{2\sigma^2}}
$$

$$
G_x = \frac{\partial G(x,y)}{\partial x}, G_y = \frac{\partial G(x,y)}{\partial y}
$$

1) Global sharpness model approximation and calibration: A calibration routine is performed to approximate the mapping function between the sharpness and the displacement along z given a set of image frames and the corresponding ground truth z-translations of the piezo stage for each image frame. The calibration data is used to approximate the sharpness model as a function $\phi(z)$ of the overall object displacement $z$ by fitting a sum of $N$ Gaussian curves (Fig. 2 - top)

$$
\phi(z) = \sum_{i=1}^{N} \alpha_i e^{-\frac{(z-b_i)^2}{c_i^2}}
$$

where $\alpha_i$ the maximum amplitude of the $i_{th}$ Gaussian term, $b_i$ the depth at which the sharpness is maximum and $c_i$ the standard deviation of the $i_{th}$ Gaussian curve. An indicative set of calibration data is shown in Fig. 1, which include the depth measurements (orange), the image sequence and the corresponding sharpness values for each frame (blue). The calibration trajectory corresponds to scanning the microstructure along its height on an upwards and a downwards trajectory.

2) Global depth reconstruction: The global sharpness approximation as a function of the depth cannot be used directly to reconstruct the z-displacement as the Gaussian
functions are not invertible. In particular, it can be seen that two different depths can correspond to the same sharpness value (Fig. 2 - top). For this reason, the sinusoidal calibration trajectory can be divided in two sections to which a sum of one-sided Gaussian curves can be fitted (Fig 2 - Data sets 1 and 2 (top)). The corresponding inverted functions \( z_i = f^{-1}(\phi) \) are depicted in Fig. 2 (bottom) (here \( i = 1, 2 \)). The depth at which the data is divided corresponds to the depth \( z_a \) at which the approximated sharpness function is changing slope. The switching between the curves \( z_1 \) and \( z_2 \) (Fig. 2 - Fitted lines 1 and 2) is determined by a number of conditions. In particular, these switching conditions are defined by the sign of the rate of change of the estimated depth \( \Delta z \) and the range at which the estimated depth belongs to (Data Set 1 or 2). Continuous switching can be ensured since a continuous \( z \)-trajectory is assumed and high alterations of the depth cannot be performed. Therefore, the switching conditions are given as follows

\[
\begin{align*}
  z_{est\_curr} &= \begin{cases} 
    z_1, & \text{if } z_{est\_prev} \leq z_a \text{ or } \Delta z < 0 \\
    z_2, & \text{if } z_{est\_prev} > z_a \text{ or } \Delta \phi_m < 0 \text{ and } \Delta z < 0
  \end{cases} \\
  \Delta \phi_m = \phi_{m\_curr} - \phi_{m\_prev}, \quad \Delta z = z_{est\_curr} - z_{est\_prev}
\end{align*}
\]

where \( z_{est\_curr}, z_{est\_prev} \) the current and previous estimated depth and \( \phi_{m\_curr}, \phi_{m\_prev} \) the current and previous sharpness value respectively.

**D. Depth estimation using local sharpness model approximation**

The previous approach is sufficient for depth reconstruction when the sharpness function has a dominant peak that can describe the object displacement along the \( z \)-axis. Due to object transparency, the features below or above the focus plane contribute to the total sharpness measurement when using as input to the calculations the whole image frame. This is also indicated by the fact that the sharpness measure for the whole image is approximated by a sum of Gaussian terms. In the propose methodologies, it is assumed that each Gaussian curve corresponds to a dominant depth (or object feature). This implies that the contribution of the dominant features of the microstructure to the single sharpness measurement can correspond to different depths. In addition, during 3D rotation, different parts of the object become defocused, resulting to changes in the overall sharpness measurement. Hence, the overall sharpness measurement cannot identify whether defocusing occurs only locally at the object due to rotation or if it is uniform due to translation along the \( z \)-axis.

In order to get the corresponding depth of single features, smaller windows around single features of the object are obtained. The centres of the local windows are obtained by the projection of the registered 3D points of the CAD model on the image frame. The 3D orientation of the object is estimated as presented in [11]. Estimating the orientation and the 2D position of the object is necessary to obtain a window that contains only the feature of interest.

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![Fig. 2. Global sharpness model approximation from calibration (top). Inverse sharpness models (bottom)](image-url)
of the equation can be expressed as a sum of Gaussians, using the functions defined for the known features in the calibration procedure.

E. 2D position derivation and 3D model-based orientation estimation

As mentioned, the object position on the x-y plane and the 3D orientation are derived as presented in [11]. A brief overview of the methodology is described in this section.

1) Contour based 2D position derivation: The 2D position of the object is calculated using the extracted contour of the object. The centroid of the contour is used as the object 2D position for convex objects. Alternatively, for non-convex objects, the 2D position can be calculated with respect to another point within the extracted 2D contour.

2) Optimization based 2D to 3D registration: The microstructure 3D model is registered with its 2D projection on the image frame by manual selection of visible feature points. Since the initial point correspondences are known, the initial orientation $R_0$ and translation $t_0$ of the object are derived by solving the following optimization problem:

$$ R_0, t_0 = \arg\min_{R,t} \| P_{ci} - K P (RP_{Mi} + t) \| $$

s.t. $R^T R = I_{3 \times 3}$

3) 3D model-based orientation estimation: The 3D orientation of the microstructure is estimated using online generated model-based templates. Model-based template matching is preferred because the initial point correspondences do not need to be tracked in every subsequent image frame. The templates are generated from a number of possible relative rotations by an angle step $\Delta \theta$ with respect to the current orientation of the microstructure. The generated templates are matched with the filled extracted object contour on the current image frame. Kalman filtering is also performed in addition to the method presented at [11].

III. EXPERIMENTAL RESULTS

The proposed methodologies are evaluated and compared to the ground truth data. The object motion is generated by translating the piezo stage along the z-axis and keeping the camera position fixed. The piezo stage trajectory is used as the ground truth data for the experimental validation.

A. Experimental Setup

The components of the hardware experimental setup include an Acoustic-Opto Deflector (AOD) Optical Tweezers (Elliot Scientific, UK) and an integrated 3D micromanipulation piezo stage which is used to simulate the object trajectories. The laser source is a 1070 nm fiber laser (Ytterbium Fiber Laser, IPG Photonics, USA) with 10 W maximum output power. A CCD camera (Basler AG, Germany) and an immersion oil lens optical microscope (Nikon Ti) with 100x magnification are used to capture the live feed during the experiment. The experimental set-up is shown in Fig. 4.

B. Microstructure fabrication

The structures used in the experiments are 3D-printed micro-gears. The height of the structure is 11.2 $\mu$m. The microstructures were printed using the Nanoscribe 3D-printer (Nanoscribe, Germany) and the IP-L photoresist. The printing power was set to 25%. The structures were printed on a glass substrate, placed in deionized water and kept fixed on the glass substrate.

C. Depth estimation using global sharpness approximation model

1) Results and discussion: The depth of the 3D-printed microstructure in a different object trajectory is estimated by using the sharpness approximation model obtained from the calibration. In this case, a triangular trajectory was chosen but alternative motions could also be performed. The focus measurement of the new sequence is calculated and the resulting sharpness for each frame is shown in Fig. 5. The calculated sharpness values are used to estimate the depth using the inverse switching model as described in Section II-C. As shown in Fig. 6, the estimated depth trajectory follows the ground truth stage trajectory. It is worth noting that the reconstruction error is similar for all three phases as the object trajectory is periodic.
D. Depth estimation using local sharpness approximation model

1) Results and discussion: To confirm that the proposed method can estimate the relative depth of the local features on the microstructure, the translational stage is moved by following a sine wave trajectory. For each local feature, a depth relative to the initial position is estimated by using the calibrated parameters of the 1D Gaussian model. As shown in Fig. 7 (top), a set of local windows are cropped around the corner features in each image frame. The estimated relative depth follows the reference stage movement as long as the sharpness of the window changes. If the sharpness value does not change, which indicates the focus plane does not intersect with the microstructure, the proposed method assumes that the object is static. This could also be attributed to limitations of the used optimization method, which was the Quasi-Newton optimization algorithm. When the focus plane intersects the microstructure again (i.e. part of the object is in focus), the relative depth of the feature can be estimated, as shown in Fig. 7.

It is worth noting that the calculated sharpness measures for each individual feature can also reveal information about the object orientation. In particular, Fig. 3 (right) depicts the selected features as projected on the image and their corresponding sharpness values. It is shown that the features on the left of the microgear are at lower depths compared to the features on the right. This can also be visually verified since the left features are more blurry than the ones on the right. This information can be fused with the results from the 3D estimation component of the framework to account for misalignments in the orientation or detect the out of focus parts of the microstructure. Therefore, the local depth estimation relates the local z-displacements of the object features to the estimated orientation.

E. 2D position and 3D model-based orientation estimation

1) Results and discussion: The corresponding orientation of the microstructure was estimated using the method described in Section II-E. As indicated by the local depth estimation, the 3D orientation of the object is not parallel to the focus plane but the object is slightly rotated around the X and Y axis of the global frame. The estimated orientation with respect to the global frame and the 2D position of the object are equal to:

\[
R = R_x(-2.2081^\circ) R_y(2.1893^\circ) R_z(-0.6422^\circ) \quad (9)
\]
\[
t_x = 320.3724, \quad t_y = 275.8510 \quad (10)
\]

The corresponding matched template and the extracted contour are shown in Fig. 8.

IV. CONCLUSIONS

In this paper, two depth estimation methods are presented for transparent, laser-driven microrobots. A global and a local
method of depth estimation of the transparent microstructure are described. These methods aim to derive an estimation for the sharpness model with respect to the overall z-translation of the object and depth changes of individual features of the microstructure. The calibration methods presented for both methodologies are object and lighting condition specific and need to be performed prior to the depth estimation routine. The combination of these two methods aims at distinguishing the cause of image sharpness variations. These variations can be attributed either to object translation along the microscope z-axis detected by the global approach or to 3D rotation detected by the local approach. Hence, the local method is capable of identifying which parts of the microstructure are in and out of focus in combination with the 3D estimated orientation. The global sharpness can be approximated by a sum of Gaussian curves for interfering features at different depths due to transparency. The local sharpness model is approximated by one Gaussian curve for distinct object features. The local method can reveal information about the object orientation and can be potentially combined with the model-based approach to estimate 3D orientation. By combining the two methods, the framework can account either for errors that occur from the template matching or the local depth estimation.

REFERENCES