

# ADAPTIC

## User Manual

Revision 1.3b

**B.A. Izzuddin**

March 2009

Systems and Mechanics Section  
Department of Civil and Environmental Engineering  
Imperial College  
London SW7 2BU

| <b>Table of Contents</b>                           | <b>Page</b> |
|--|-------------|
| <b>CHAPTER 1. INTRODUCTION.....</b>                | <b>1</b>    |
| 1.1 TYPES OF ANALYSIS .....                        | 2           |
| 1.1.1 Static analysis – proportional loading ..... | 2           |
| 1.1.2 Static analysis – time-history loading ..... | 2           |
| 1.1.3 Dynamic analysis .....                       | 2           |
| 1.1.4 Eigenvalue analysis.....                     | 2           |
| 1.2 STRUCTURAL MODELLING.....                      | 3           |
| 1.2.1 Elastic Modelling .....                      | 3           |
| 1.2.2 Plastic Hinge Modelling.....                 | 3           |
| 1.2.3 Elasto-Plastic Modelling.....                | 3           |
| 1.2.4 Adaptive Elasto-Plastic Modelling.....       | 3           |
| 1.2.5 Joints and Boundary Conditions .....         | 3           |
| 1.2.6 Dynamic Characteristics Modelling .....      | 4           |
| <b>CHAPTER 2. USING ADAPTIC.....</b>               | <b>5</b>    |
| 2.1 ADAPTIC DATA FILE .....                        | 5           |
| 2.2 STARTING ADAPTIC .....                         | 5           |
| 2.3 ADAPTIC OUTPUT FILES.....                      | 5           |
| <b>CHAPTER 3. MATERIAL MODELS.....</b>             | <b>6</b>    |
| <b>CHAPTER 4. JOINT ELEMENT CURVES .....</b>       | <b>33</b>   |
| <b>CHAPTER 5. CROSS-SECTION TYPES .....</b>        | <b>41</b>   |
| <b>CHAPTER 6. ELEMENT TYPES.....</b>               | <b>60</b>   |
| <b>CHAPTER 7. DATA SYNTAX.....</b>                 | <b>103</b>  |
| 7.1 INTRODUCTION .....                             | 103         |
| 7.2 GENERAL FACILITIES .....                       | 104         |
| 7.2.1 Continuation.....                            | 105         |
| 7.2.2 Comments.....                                | 106         |
| 7.2.3 Incrementation .....                         | 107         |
| 7.3 INPUT MODULES .....                            | 108         |
| 7.3.1 Analysis.....                                | 109         |
| 7.3.2 Default parameters.....                      | 110         |
| 7.3.3 Materials .....                              | 111         |
| 7.3.4 Sections .....                               | 112         |
| 7.3.5 Patterns .....                               | 113         |
| 7.3.6 Groups.....                                  | 114         |
| 7.3.7 Structural.nodal.coordinates.....            | 115         |
| 7.3.8 Non.structural.nodal.coordinates .....       | 116         |
| 7.3.9 Element.connectivity .....                   | 117         |
| 7.3.10 Imperfections.....                          | 118         |
| 7.3.11 Restraints .....                            | 119         |
| 7.3.12 Conditions .....                            | 120         |
| 7.3.13 Linear.curves.....                          | 121         |
| 7.3.14 Integration.scheme .....                    | 123         |
| 7.3.15 Applied.loading .....                       | 124         |
| 7.3.16 Equilibrium.stages .....                    | 126         |
| 7.3.17 Phases .....                                | 127         |
| 7.3.18 Iterative.strategy .....                    | 129         |
| 7.3.19 Convergence.criteria.....                   | 131         |
| 7.3.20 Output .....                                | 133         |
| 7.3.21 Lanczos.eigenvalue .....                    | 134         |
| <b>CHAPTER 8. POST-PROCESSING.....</b>             | <b>136</b>  |

|                                    |  |            |
|------------------------------------|--|------------|
| 8.1                                | START-UP .....   | 136        |
| 8.2                                | ADAPTIC_GRAPHS .....                                   | 137        |
| 8.2.1                              | General Facilities.....                                | 137        |
| 8.2.2                              | File .....   | 138        |
| 8.2.3                              | Graphs.....  | 139        |
| 8.2.4                              | Customize .....  | 140        |
| 8.3                                | ADAPTIC_SHAPES .....                                   | 141        |
| 8.3.1                              | General Facilities.....                                | 141        |
| 8.3.2                              | File .....   | 143        |
| 8.3.3                              | Shapes .....   | 144        |
| 8.3.4                              | Contours.....  | 145        |
| 8.3.5                              | View.....  | 146        |
| <b>CHAPTER 9.    EXAMPLES.....</b> |  | <b>147</b> |
| 9.1                                | SPACE DOME SUBJECT TO VERTICAL APEX LOAD.....          | 147        |
| 9.1.1                              | Data file.....   | 148        |
| 9.1.2                              | Structural behaviour .....                             | 150        |
| 9.1.3                              | Output file .....                                      | 152        |
| 9.2                                | K-FRAME SUBJECT TO VERTICAL LOAD .....                 | 155        |
| 9.2.1                              | Data file.....   | 156        |
| 9.2.2                              | Structural behaviour .....                             | 158        |
| 9.2.3                              | Output file .....                                      | 160        |
| 9.3                                | LEE'S FRAME .....                                      | 163        |
| 9.3.1                              | Data file.....   | 164        |
| 9.3.2                              | Structural behaviour .....                             | 166        |
| 9.3.3                              | Output file .....                                      | 168        |
| 9.4                                | FIXED ENDED BEAM-COLUMN .....                          | 171        |
| 9.4.1                              | Data file.....   | 172        |
| 9.4.2                              | Structural behaviour .....                             | 174        |
| 9.4.3                              | Output file .....                                      | 175        |
| 9.5                                | TWO-STOREY .....                                       | 181        |
| 9.5.1                              | Data file.....   | 182        |
| 9.5.2                              | Structural behaviour .....                             | 184        |
| 9.5.3                              | Output file .....                                      | 185        |
| 9.6                                | STEEL FRAME SUBJECT TO EXPLOSION AND FIRE LOADING..... | 201        |
| 9.6.1                              | Data file.....   | 202        |
| 9.6.2                              | Structural behaviour .....                             | 205        |
| 9.6.3                              | Output file .....                                      | 207        |
| 9.7                                | APEXES .....   | 222        |

# Chapter 1. INTRODUCTION

ADAPTIC is an adaptive static and dynamic structural analysis program which has been developed to provide an efficient tool for the nonlinear analysis of steel and composite frames, slabs, shells and integrated structures. The program features are described briefly hereafter.

The initial development of ADAPTIC was driven by the needs of the offshore industry for an accurate yet efficient nonlinear analysis of offshore jackets subject to extreme static and dynamic loading. This motivated the development of pioneering adaptive nonlinear dynamic analysis techniques for framed structures, accounting for geometric and material nonlinearity, which formed the basis of Prof. Izzuddin's PhD thesis, and which were extensively applied in nonlinear structural analysis under earthquake loading. Since then the program has been extensively developed to deal with other extreme loading, such as fire and blast, as well as numerous additional structural forms, such as R/C and steel-decked composite slabs, cable and membrane structures, and curved shells. Most of these novel developments have been published in leading international scientific and professional journals as well as in international conferences (see <http://www.imperial.ac.uk/people/b.izzuddin/publications>).

This version of the manual (V1.1) covers mainly the frame analysis capabilities of ADAPTIC. The more recent developments dealing with slabs and shells will be described in forthcoming versions of the manual. Therefore, the following discussions focus on the nonlinear analysis of plane and space frames.

Inelastic analysis of steel frames may be performed by either of two methodologies. The first is an approximate solution using ideal plastic hinge elements, while the second is a more accurate solution employing elements which account for the spread of plasticity across the section depth and along the member length. For reinforced concrete and composite frames, inelastic analysis is performed using the second approach only.

The loading can be either applied forces or prescribed displacements/accelerations at nodal points. The loads can vary proportionally under static conditions, or can vary independently in the time or pseudo-time domains. The latter variation can be utilised for static or dynamic analysis.

## 1.1 Types of Analysis

Loads can be applied at the nodal positions for the translational and rotational freedoms in the three global directions (X, Y, Z). A load can be an applied force or a prescribed displacement/acceleration. The only restriction on the application of loads is that a load corresponding to a structural freedom should only be specified once, and that the loaded freedom should not be restrained. This requires that ground excitation, for example, should be specified as an applied acceleration at the ground nodal freedoms, and that these freedoms should not be restrained.

Static loads applied only once to the structure at the start of analysis. Any further loads applied during proportional or time-history loading are applied incrementally on top of these loads.

The initial loads are useful for modelling the structure dead weight. Also, they can model initial support settlement through using a displacement load at a support nodal freedom.

### 1.1.1 Static analysis – proportional loading

These are loads which vary proportionally according to one load factor. The behaviour of a structure under proportional loading can be studied in the post-ultimate range using the displacement control strategy. These loads cannot be applied with time-history loads within the same analysis.

### 1.1.2 Static analysis – time-history loading

These are loads which can vary independently in the time or pseudo-time domain. As such, if the structure has reached a stage where the loads cannot be incremented as specified by the user, the analysis is terminated since the program cannot establish how the user would want to continue the analysis.

Time-history loads are useful for modelling cyclic loading under various force or displacement regimes.

### 1.1.3 Dynamic analysis

Dynamic loads can be specified in a similar way to time-history loads and can be applied forces or prescribed accelerations. Note that the latter allow the modelling of ground excitation, which is different from the case of static analysis where support motion is indicated by means of prescribed displacements. The ability to model loads varying independently in the time domain allows asynchronous excitation to be represented with relative ease.

### 1.1.4 Eigenvalue analysis

Eigenvalue analysis is performed using the efficient [Lanczos](#) algorithm, which requires as input the number of modes within the range of frequencies of interest as well as the number of iterative steps. This algorithm can also be used with dynamic analysis, where the frequencies and modes are obtained during analysis using the tangent stiffness.

## 1.2 Structural Modelling

The following sections describe how various analysis assumptions can be modelled using the ADAPTIC elements, which are discussed in detail in [Chapter 6](#). Note that different assumptions can be utilised in the same analysis for different members of the structure. Note also that similar element types usually exist for 2D and 3D analysis, distinguished by the last number in the element type identifier (e.g. [qph2](#) & [qph3](#))

### 1.2.1 Elastic Modelling

Quartic elastic elements ([qel2](#), [qel3](#)) can be used to model the beam-column effect and large displacements for selected structural members. One quartic element is capable of representing the beam-column action and large displacements for a whole member.

### 1.2.2 Plastic Hinge Modelling

Quartic plastic hinge element ([qph2](#), [qph3](#)) have the same elastic representation power of elements ([qel2](#), [qel3](#)) but can represent material inelasticity through the utilisation of zero-length plastic hinges at the element end nodes. The introduction of these plastic hinges depends on the interaction between the bending moments at the element ends and the axial force, established from the specification of the element [cross-section](#).

### 1.2.3 Elasto-Plastic Modelling

Detailed elasto-plastic modelling, based on the inelastic uniaxial material response, can be performed using cubic elasto-plastic elements ([cbp2](#), [cbp3](#)), which accurately model the spread of plasticity across the cross-section through the utilisation of material monitoring point. To represent the spread of inelasticity along the member length, a number of cubic elements, usually over 5, are required per member.

### 1.2.4 Adaptive Elasto-Plastic Modelling

Adaptive analysis can be applied in the elasto-plastic analysis of steel frames to reduce the modelling task, which previously required a fine mesh of cubic elements all over the structure, and to enable the analysis to be performed quite efficiently. The concept of adaptive analysis entails the utilisation of elastic quartic element ([qdp2](#), [qdp3](#)) which would sub-divide into inelastic cubic elements ([cbp2](#), [cbp3](#)) when inelasticity is detected during analysis. The analysis is started using only one quartic element per member, with element refinement performed automatically when necessary in zones along the element which are pre-defined by the user.

### 1.2.5 Joints and Boundary Conditions

Joint behaviour can be modelled by means of joint elements ([jel2](#), [jel3](#)) with de-coupled axial, shear and moment actions. These joint elements can have any orientation, and may utilise a number of force-displacement relationships described in [Chapter 4](#).

The joint elements may also be used to model special boundary conditions, such as inclined supports, soil-structure interaction and structural gaps, through choosing appropriate terms for the force-displacement relationships.

## 1.2.6 Dynamic Characteristics Modelling

The dynamic characteristics of the structure, namely mass and damping, are modelled by means of non-structural elements which must be included for dynamic analysis to be performed. The dynamic element types are:

| Type  | Description                      |
|---|----------------------------------|
| <a href="#"><u>cnm2</u></a> , <a href="#"><u>cnm3</u></a> | Lumped mass elements             |
| <a href="#"><u>lnm2</u></a> , <a href="#"><u>lnm3</u></a> | Linear distributed mass elements |
| <a href="#"><u>cbm2</u></a> , <a href="#"><u>cbm3</u></a> | Cubic distributed mass elements  |
| <a href="#"><u>cnd2</u></a> , <a href="#"><u>cnd3</u></a> | Dashpot damping elements         |
| <a href="#"><u>rld2</u></a> , <a href="#"><u>rld3</u></a> | Rayleigh damping elements        |

# Chapter 2. USING ADAPTIC

## 2.1 ADAPTIC Data File

In order to perform nonlinear structural analysis using ADAPTIC, the problem data is stored in a data file which the program reads and processes. Such data specifies the structural configuration and the loading applied to structure, and must follow the syntax described in the [Data Syntax](#) chapter.

All ADAPTIC data files must have a ".dat" extension (e.g. one\_storey.dat , SW\_2.1.dat). A new data file may be created through modifying an existing data file or through typing the data from scratch. The former approach is usually more convenient, especially for parametric studies when only some data entries require modification.

## 2.2 Starting ADAPTIC

ADAPTIC currently runs on Linux workstations, where it is started using the following command:

```
{prompt} adaptic filename
```

Note that the *filename* does not include the ".dat" extension (e.g. adaptic one\_storey).

ADAPTIC can also be run in the background using the following command:

```
{prompt} adaptic filename > filename.log &
```

where *filename.log* is a file which stores the job progress.

The execution of ADAPTIC invokes two successive stages. The first is a data reading stage, where the problem details are read from the data file, and several temporary files are created which incorporate problem and plotting information. The second is the analysis stage, where the information is retrieved from the temporary files and the nonlinear analysis is undertaken as specified. If the program seems to hang up before entering the reading stage, make sure that the two files *param.inc* and *stat.x* are removed from the working directory.

## 2.3 ADAPTIC Output Files

Upon successful completion of an ADAPTIC run, three additional files corresponding to *filename* should exist (*filename.out*, *filename.num* & *filename.plt*). The first file echoes the data file and contains the solution progress log. The second file contains the numerical results at all requested load/time steps. The third file is a plot file used by the post-processing programs.

Numerical results may be obtained through direct extraction from *filename.num*. Graphical visualisation of the results is also available through a number of post-processing programs described in the [Post-Processing](#) chapter.



# Chapter 3. MATERIAL MODELS

The ADAPTIC library includes a number of uniaxial material models which can be used to model steel, concrete and other materials with similar behavioural characteristics. The models and their applicability are briefly described below, with full details given in next pages:

| <u>Model</u>                | <u>Applicability</u>                                 |
|-----------------------------|--|
| <a href="#"><u>stl1</u></a> | Bilinear steel model with kinematic strain-hardening |
| <a href="#"><u>stl2</u></a> | Multisurface steel model                             |
| <a href="#"><u>con1</u></a> | Simple trilinear concrete model                      |
| <a href="#"><u>con2</u></a> | Constant confinement concrete model                  |
| <a href="#"><u>con3</u></a> | Variable confinement concrete model                  |

Cubic elasto-plastic formulations ([cbp2](#), [cbp3](#)) utilise the full inelastic characteristics of the above models.

Quartic plastic hinge formulations ([qph2](#), [qph3](#)) utilise only the yield characteristics of the models.

The elastic formulations utilise only the elastic characteristics of the models.

This section describes the material models available in ADAPTIC. Each model is referred to by a unique name, displayed at the top of the following pages, and requires the specification of a number of properties in the order indicated.

*stl1*

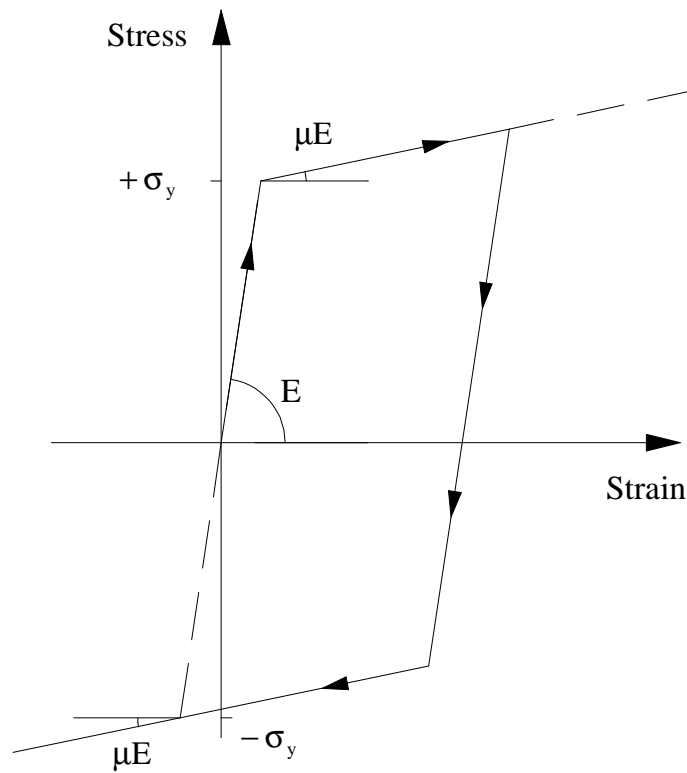
---

---

|                          |  |                |
|--------------------------|--|----------------|
| <b>Description</b>       | Bilinear elasto-plastic model with kinematic strain hardening. |                |
| <b>No. of properties</b> | 3  |                |
| <b>Properties</b>        | Young's modulus  | ( E )          |
|                          | Yield strength   | ( $\sigma_y$ ) |
|                          | [ Strain-hardening factor ( $\mu$ ) ]                          |                |
| <b>Application</b>       | Uniaxial modelling of mild steel                               |                |

---

---



*Material model stl1*

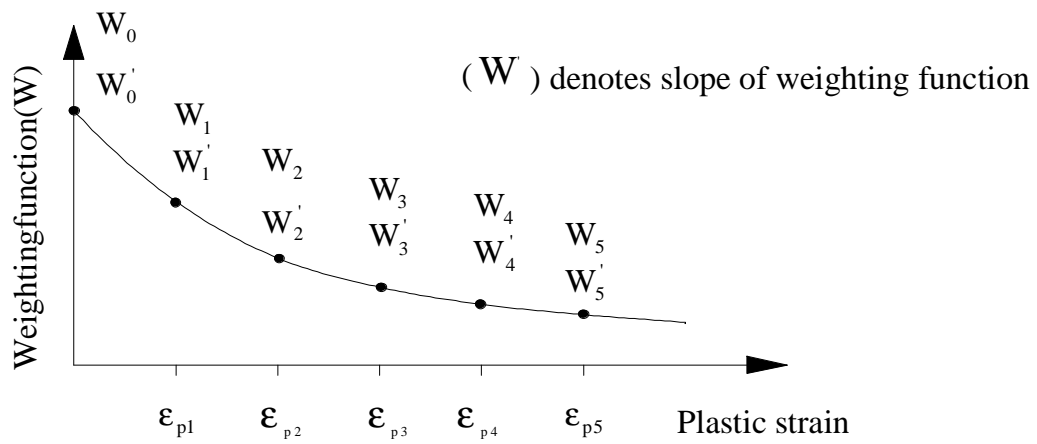
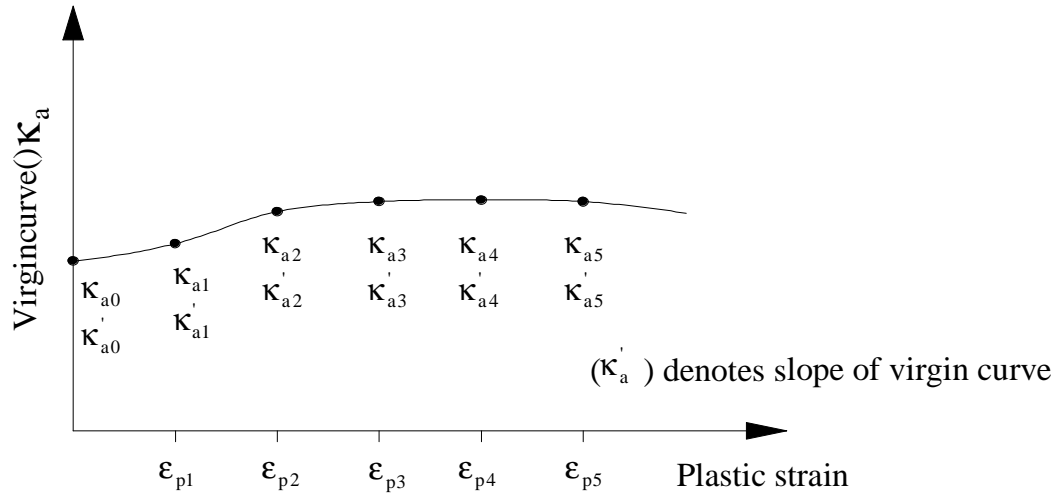
---

---

|                          |   |
|--------------------------|---|
| <b>Description</b>       | Multi-surface model for cyclic plasticity.  |
| <b>No. of properties</b> | 42  |
| <b>Properties</b>        | Young's modulus ( E )<br>Plastic strains used for curves description<br>$(\epsilon_{p1}, \epsilon_{p2}, \dots, \epsilon_{p5})$<br>Virgin stress-plastic strain properties<br>$(\kappa_{a0}, \kappa'_{a0}, \kappa_{a1}, \kappa'_{a1}, \dots, \kappa_{a5}, \kappa'_{a5})$<br>Cyclic stress-plastic strain properties<br>$(\kappa_{b0}, \kappa'_{b0}, \kappa_{b1}, \kappa'_{b1}, \dots, \kappa_{b5}, \kappa'_{b5})$<br>Weighting function properties<br>$(W_0, W'_0, W_1, W'_1, \dots, W_5, W'_5)$ |
| <b>Application</b>       | Cyclic behaviour of steel modelling hardening, softening and mean stress relaxation.  |
| <b>Restrictions</b>      | No descending branch beyond ultimate point<br>(i.e $\kappa'_{a5} > 0, \kappa'_{b5} > 0$ ).  |

---

---



*Material model stl2*

### *stl3*

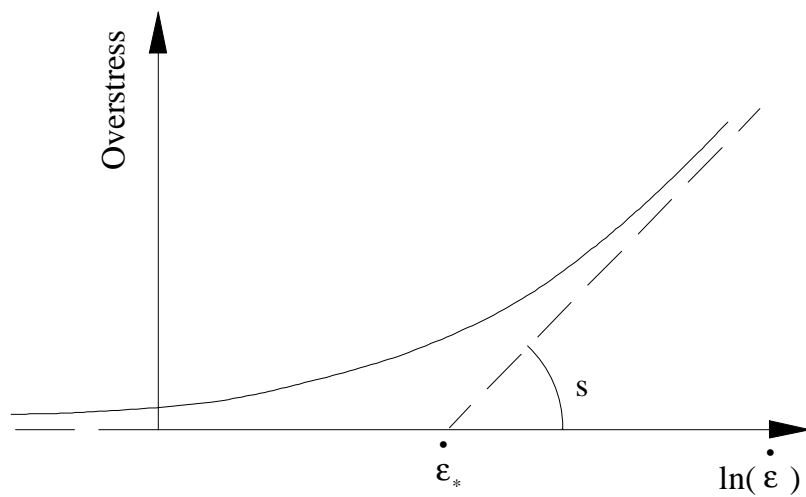
---

---

|                          |  |
|--------------------------|--|
| <b>Description</b>       | Rate-sensitive bilinear elasto-plastic model with kinematic strain hardening.  |
| <b>No. of properties</b> | 5  |
| <b>Properties</b>        | Young's modulus (E)<br>Yield strength ( $\sigma_y$ )<br>Strain-hardening factor ( $\mu$ )<br>Rate-sensitive parameter (s)<br>Rate-sensitive parameter ( $\dot{\epsilon}$ ) |
| <b>Application</b>       | Uniaxial modelling of mild steel   |

---

---

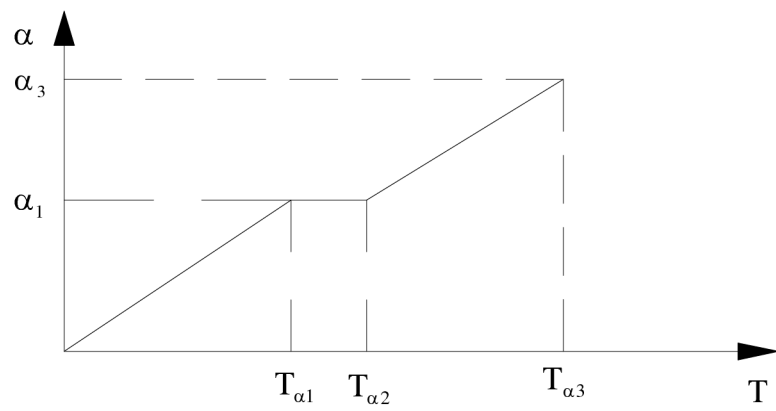
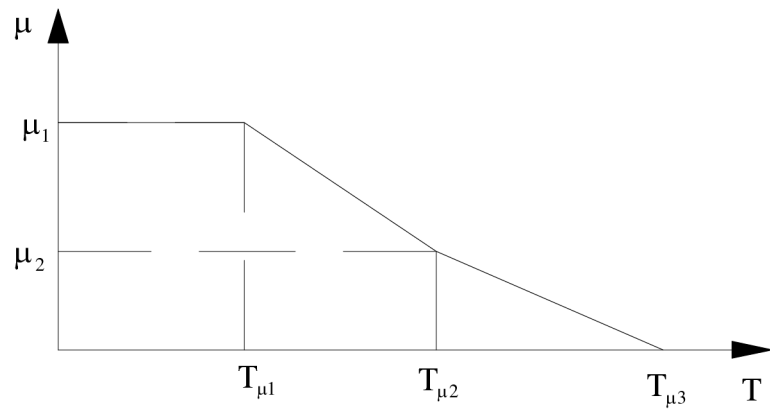
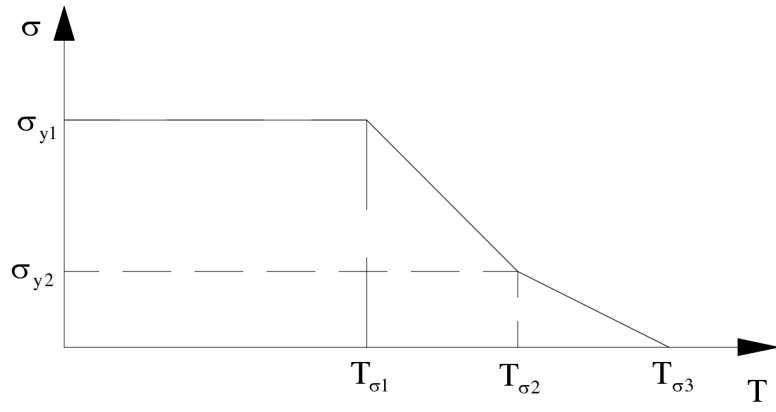


*Material model stl3*

|                                 |  |
|---------------------------------|--|
| <b><i>Description</i></b>       | Bilinear material model  |
| <b><i>No. of properties</i></b> | 20   |
| <b><i>Properties</i></b>        | Young's modulus and temperatures used for trilinear description:<br>$(E_1, E_2, T_1, T_2, T_3)$<br>Yield strength and temperatures for trilinear description<br>$(\sigma_{y1}, \sigma_{y2}, T_{\sigma1}, T_{\sigma2}, T_{\sigma3})$<br>Strain-hardening factor and temperatures for trilinear description:<br>$(\mu_1, \mu_2, T_{\mu1}, T_{\mu2}, T_{\mu3})$<br>Thermal strain and temperatures<br>$(\alpha_1, \alpha_3, T_{\alpha1}, T_{\alpha2}, T_{\alpha3})$ |
| <b><i>Application</i></b>       | Requires the specification of Young's modulus, the yield strength, the strain-hardening factor, the thermal strain and their variations with temperature.  |
| <b><i>Restrictions</i></b>      |  |

---

---



*Material model stl4*

## *stl5*

---

---

|                                 |   |
|---------------------------------|---|
| <b><i>Description</i></b>       | Creep model   |
| <b><i>No. of properties</i></b> | 28  |
| <b><i>Properties</i></b>        | The first 20 properties are the same as those of the bilinear model.<br>Material constants for modelling creep<br>(A, B, C, D, F, G, $\Delta H$ , R, $\sigma^*$ ) |
| <b><i>Application</i></b>       | In addition to the 20 parameters for the bilinear material model, 8 more parameters are required to specify the creep response of the material                    |
| <b><i>Restrictions</i></b>      |   |

---

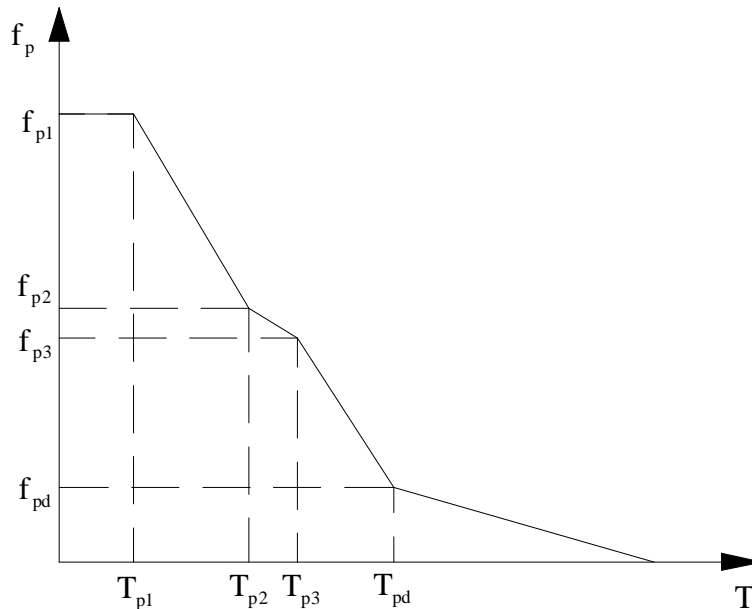
---



|                          |  |
|--------------------------|--|
| <b>Description</b>       | Elliptical model   |
| <b>No. of properties</b> | 36   |
| <b>Properties</b>        | <p>Young's modulus and corresponding temperatures<br/> <math>(E_1, E_2, E_3, E_4, T_1, T_2, T_3, T_4, T_5)</math></p> <p>Yield strength and corresponding temperatures<br/> <math>(f_{y1}, f_{y2}, f_{y3}, f_{y4}, T_{y1}, T_{y2}, T_{y3}, T_{y4}, T_{y5})</math></p> <p>Proportional limit and corresponding temperatures<br/> <math>(f_{p1}, f_{p2}, f_{p3}, f_{p4}, T_{p1}, T_{p2}, T_{p3}, T_{p4}, T_{p5})</math></p> <p>Thermal strain and corresponding temperatures<br/> <math>(\alpha_1, \alpha_2, \alpha_3, \alpha_4, T_{\alpha1}, T_{\alpha2}, T_{\alpha3}, T_{\alpha4}, T_{\alpha5})</math></p> |

**Application** requires 36 parameters in total to describe Young's modulus, the proportional limit, the yield strength, the thermal strain and their variations with temperature. The nine parameters used to define the proportional limit and its variation with temperature is illustrated in figure. The other parameters are defined in the same sequence.

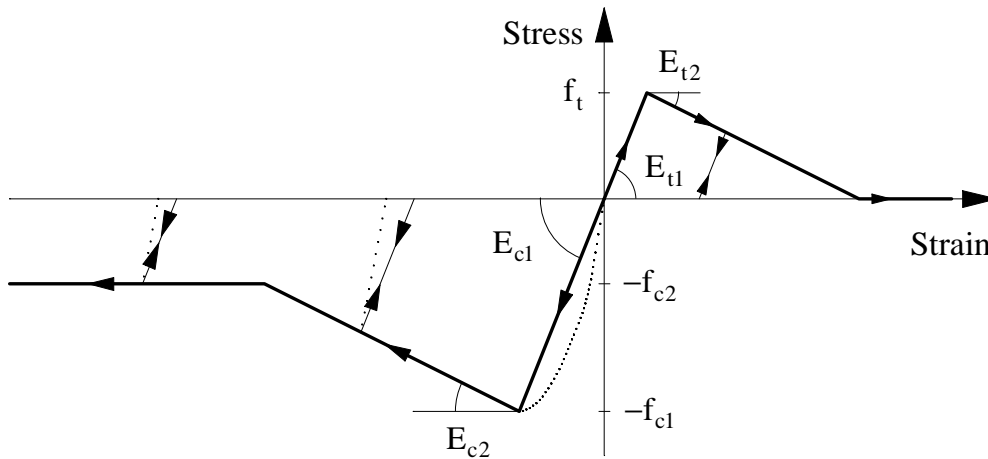
**Restrictions**



*Material model stl10*

*con1*

|                          |   |               |
|--------------------------|---|---------------|
| <b>Description</b>       | Trilinear concrete model, with optional tensile response and quadratic initial compressive response.                        |               |
| <b>No. of properties</b> | 4   |               |
| <b>Properties</b>        | Secant compressive stiffness  | $(E_{c1})$    |
|                          | Compressive strength  | $(f_{c1})$    |
|                          | Compressive softening stiffness   | $(E_{c2})$    |
|                          | Residual compressive strength   | $(f_{c2})$    |
|                          | [ Initial tensile stiffness   | $(E_{t1})$    |
|                          | Tensile strength  | $(f_t)$       |
|                          | Tensile softening stiffness   | $(E_{t2})$    |
|                          | [Value of $\alpha = (E_{c1}^t - E_{c1})/E_{c1}$   | $([0,1])$ ] ] |
| <b>Application</b>       | Simplified uniaxial modelling of concrete material.   |               |
| <b>Notes</b>             | $E_{c1}^t$ is the initial tangent modulus in compression.<br>$\alpha > 0$ implies a quadratic initial compressive response. |               |



*Material model con1*

## con2

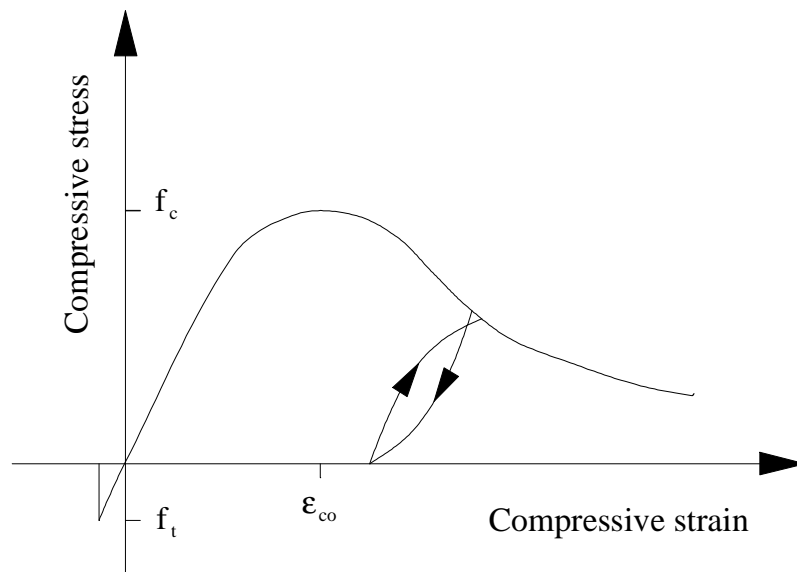
---

---

|                          |   |
|--------------------------|---|
| <b>Description</b>       | Uniaxial constant confinement concrete model.   |
| <b>No. of properties</b> | 4   |
| <b>Properties</b>        | Concrete compressive strength ( $f_c$ )<br>Concrete tensile strength ( $f_t$ )<br>Crushing strain ( $\epsilon_{co}$ )<br>Confinement factor ( $k$ ) |
| <b>Application</b>       | Uniaxial modelling of concrete assuming constant confinement.   |
| <b>Restrictions</b>      | Parameter units must be in Newtons and Millimetres.<br>The confinement factor must be greater or equal to 1.  |

---

---



*Material model con2*

*con3*

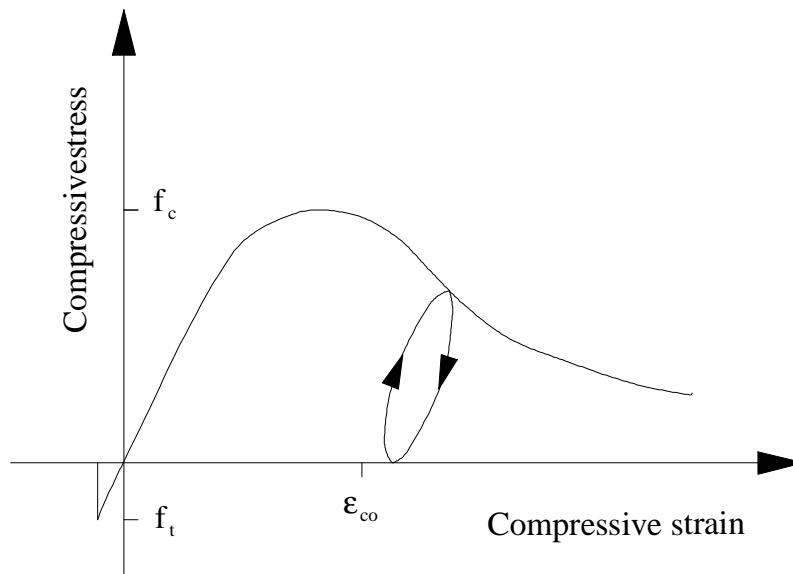
---

---

|                          |  |                     |
|--------------------------|--|---------------------|
| <b>Description</b>       | Uniaxial variable confinement concrete model.  |                     |
| <b>No. of properties</b> | 10   |                     |
| <b>Properties</b>        | Concrete compressive strength  | ( $f_c$ )           |
|                          | Concrete tensile strength  | ( $f_t$ )           |
|                          | Crushing strain  | ( $\epsilon_{co}$ ) |
|                          | Poisson's ratio of concrete  | ( $\nu$ )           |
|                          | Yield stress of stirrups   | ( $\sigma_y$ )      |
|                          | Young's modulus of stirrups  | ( $E$ )             |
|                          | Strain hardening of stirrups   | ( $\mu$ )           |
|                          | Diameter of stirrups   | ( $\phi$ )          |
|                          | Stirrups spacing   | ( $s$ )             |
|                          | Diameter of concrete core  | ( $\Phi_c$ )        |
| <b>Application</b>       | Uniaxial modelling of concrete accounting for variable confinement effects, which are influenced by the core area within the stirrups, stirrups size and material, and stirrups spacing. |                     |
| <b>Restrictions</b>      | Parameter units must be in Newtons and Millimetres.  |                     |

---

---



*Material model con3*

---



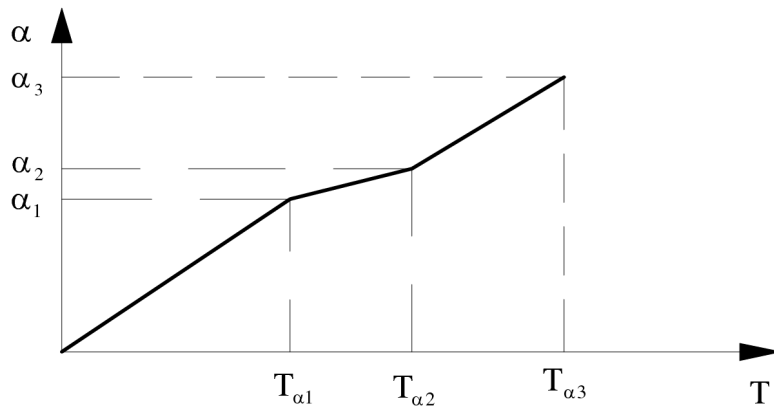
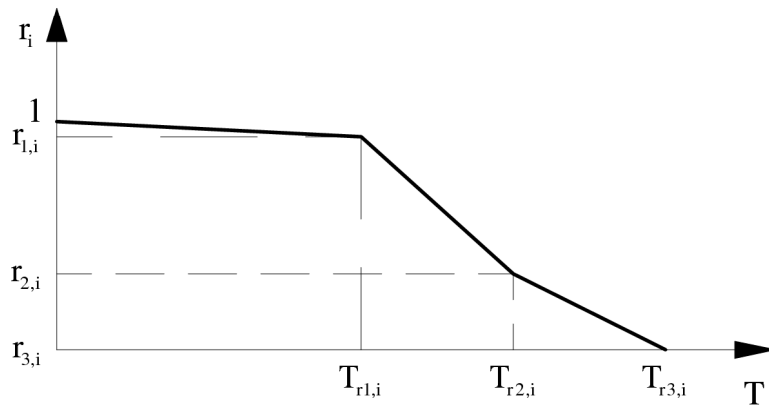
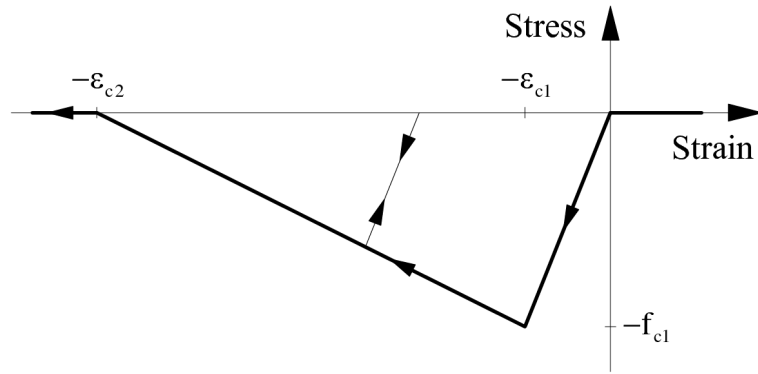
---

|                          |   |
|--------------------------|---|
| <b>Description</b>       | Trilinear compressive concrete model for elevated temperature, with zero tensile response.  |
| <b>No. of properties</b> | 28  |
| <b>Properties</b>        | <p>Compressive strength and its reduction factors <math>\left( r_1 = \frac{f_{c1(T)}}{f_{c1(0)}} \right)</math>:</p> <p><math>(f_{c1}, T_{r1,1}, r_{1,1}, T_{r2,1}, r_{2,1}, T_{r3,1}, r_{3,1})</math></p> <p>Peak compressive strain and temperature factors <math>\left( r_2 = \frac{\epsilon_{c1(T)}}{\epsilon_{c1(0)}} \right)</math></p> <p><math>(\epsilon_{c1}, T_{r1,2}, r_{1,2}, T_{r2,2}, r_{2,2}, T_{r3,2}, r_{3,2})</math></p> <p>Limit compressive strain and temperature factors <math>\left( r_3 = \frac{\epsilon_{c2(T)}}{\epsilon_{c2(0)}} \right)</math></p> <p><math>(\epsilon_{c2}, T_{r1,3}, r_{1,3}, T_{r2,3}, r_{2,3}, T_{r3,3}, r_{3,3})</math></p> <p>Thermal strain and temperatures</p> <p><math>(0(\text{unused}), T_{\alpha 1}, \alpha_1, T_{\alpha 2}, \alpha_2, T_{\alpha 3}, \alpha_3)</math></p> |
| <b>Application</b>       | Requires the specification of the compressive strength, the peak compressive strain, the limit compressive strain at zero stress, the thermal strain and their variations with temperature. Note that $r_2$ and $r_3$ can be greater than 1.  |
| <b>Restrictions</b>      |   |

---



---



*Material model con6*

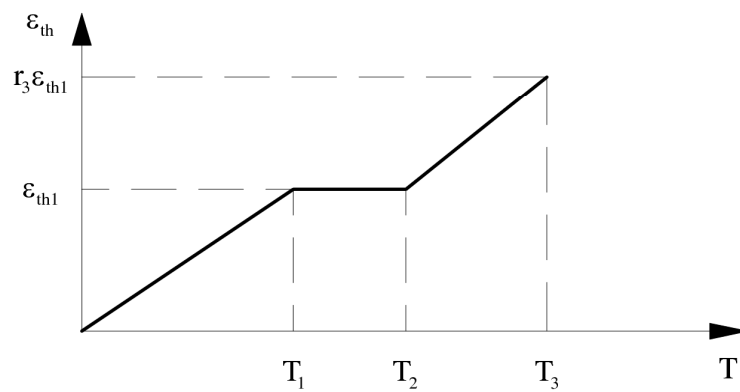
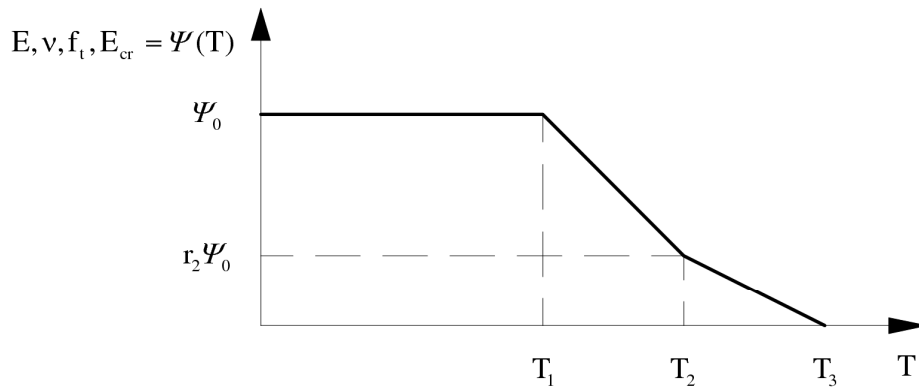
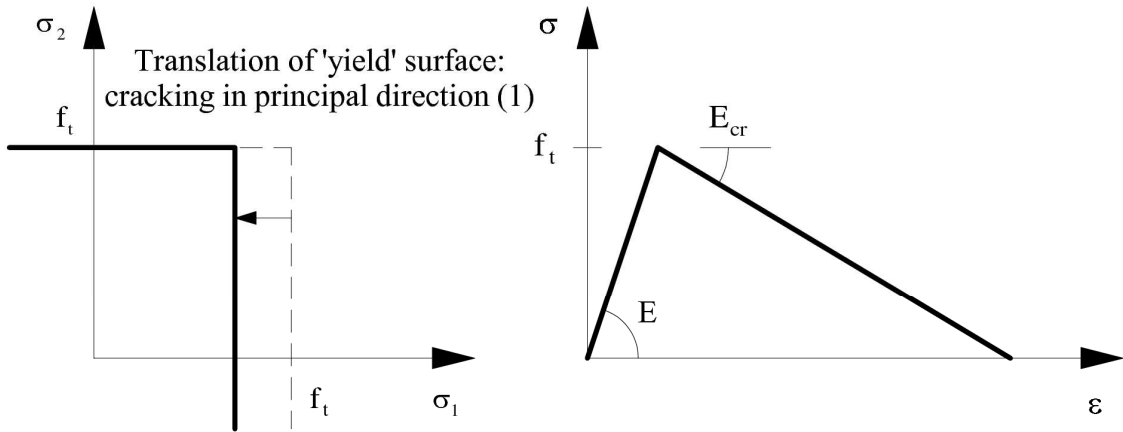
---

---

|                          |   |
|--------------------------|---|
| <b>Description</b>       | Rotating-crack elevated-temperature model for concrete with linear compressive response.  |
| <b>No. of properties</b> | 25  |
| <b>Properties</b>        | Young's modulus and temperatures:<br>( $E_0, r_2, T_1, T_2, T_3$ )<br>Poisson's ratio and temperatures:<br>( $\nu_0, r_2, T_1, T_2, T_3$ )<br>Tensile strength and temperatures:<br>( $f_{to}, r_2, T_1, T_2, T_3$ )<br>Softening slope and temperatures:<br>( $E_{cr0}, r_2, T_1, T_2, T_3$ )<br>Thermal strain and temperatures<br>( $\epsilon_{th1}, r_3, T_1, T_2, T_3$ ) |
| <b>Application</b>       | Plasticity-based model of concrete taking account of tensile cracking and elevated temperature.   |
| <b>Restrictions</b>      |   |

---

---



*Material model con9*



---



---

|                                  |  |                  |                         |  |                          |                 |        |                      |                      |                  |                      |                                  |     |                           |      |
|----------------------------------|--|------------------|-------------------------|--|--------------------------|-----------------|--------|----------------------|----------------------|------------------|----------------------|----------------------------------|-----|---------------------------|------|
| <b>Description</b>               | Uniaxial Concrete model for long term analysis.  |                  |                         |  |                          |                 |        |                      |                      |                  |                      |                                  |     |                           |      |
| <b>No. of properties</b>         | 6  |                  |                         |  |                          |                 |        |                      |                      |                  |                      |                                  |     |                           |      |
| <b>Properties</b>                | <table border="0"> <tr> <td>Type of analysis</td> <td>1 (linear viscoelastic)</td> </tr> <tr> <td></td> <td>2 (brittle viscoelastic)</td> </tr> <tr> <td>Time of casting</td> <td>[days]</td> </tr> <tr> <td>Compressive strength</td> <td>[N/mm<sup>2</sup>]</td> </tr> <tr> <td>Tensile strength</td> <td>[N/mm<sup>2</sup>]</td> </tr> <tr> <td>Relative humidity of environment</td> <td>[%]</td> </tr> <tr> <td>Notional size of member *</td> <td>[mm]</td> </tr> </table>   | Type of analysis | 1 (linear viscoelastic) |  | 2 (brittle viscoelastic) | Time of casting | [days] | Compressive strength | [N/mm <sup>2</sup> ] | Tensile strength | [N/mm <sup>2</sup> ] | Relative humidity of environment | [%] | Notional size of member * | [mm] |
| Type of analysis                 | 1 (linear viscoelastic)  |                  |                         |  |                          |                 |        |                      |                      |                  |                      |                                  |     |                           |      |
|                                  | 2 (brittle viscoelastic)   |                  |                         |  |                          |                 |        |                      |                      |                  |                      |                                  |     |                           |      |
| Time of casting                  | [days]   |                  |                         |  |                          |                 |        |                      |                      |                  |                      |                                  |     |                           |      |
| Compressive strength             | [N/mm <sup>2</sup> ]   |                  |                         |  |                          |                 |        |                      |                      |                  |                      |                                  |     |                           |      |
| Tensile strength                 | [N/mm <sup>2</sup> ]   |                  |                         |  |                          |                 |        |                      |                      |                  |                      |                                  |     |                           |      |
| Relative humidity of environment | [%]  |                  |                         |  |                          |                 |        |                      |                      |                  |                      |                                  |     |                           |      |
| Notional size of member *        | [mm]   |                  |                         |  |                          |                 |        |                      |                      |                  |                      |                                  |     |                           |      |
| <b>Application</b>               | <p>The long-term concrete model can be employed for long-term analysis. Two different options are allowed:</p> <ul style="list-style-type: none"> <li>- Linear viscoelastic concrete</li> <li>- Brittle viscoelastic concrete</li> </ul> <p>In the linear viscoelastic analysis both creep and shrinkage phenomena are evaluated according to the CEB-FIP Model Code 90<sup>[1]</sup>. The Volterra's integral equation is solved by developing the relaxation function in series of exponential functions and applying the trapezoidal rule<sup>[2,3]</sup>.</p> <p>In the brittle viscoelastic analysis, the concrete is considered linear viscoelastic in compression and in tension before cracking. In cracked phase a brittle law is assumed and both creep and shrinkage are not taken into account.</p>  |                  |                         |  |                          |                 |        |                      |                      |                  |                      |                                  |     |                           |      |
| <b>References</b>                | <p>[1] CEB 1993, CEB Bull. N°213/214: CEB-FIP Model Code 90. Comité Euro-International du Béton, Lausanne, Switzerland, 1993.</p> <p>[2] Amadio, C., Fragiaco, M., and Macorini, L., "A New Effective F.E. Formulation for Studying the Long-Term Behaviour of Continuous Steel-Concrete Composite Beams", Proceedings of the Fifth World Congress on Computational Mechanics (WCCM V), July 7-12, 2002, Vienna, Austria, Editors: Mang, H.A. <i>et al.</i>, Publisher: Vienna University of Technology, Austria.</p> <p>[3] Fragiaco, M., "A finite element model for long-term analysis of timber-concrete composite beams", submitted to <i>Computer &amp; Structures</i>.</p> <p>(*) Given by the ratio <math>2A_c/u</math>, where <math>A_c</math> is the cross section and <math>u</math> is the perimeter of the member in contact with the atmosphere.</p> |                  |                         |  |                          |                 |        |                      |                      |                  |                      |                                  |     |                           |      |

---



---

---



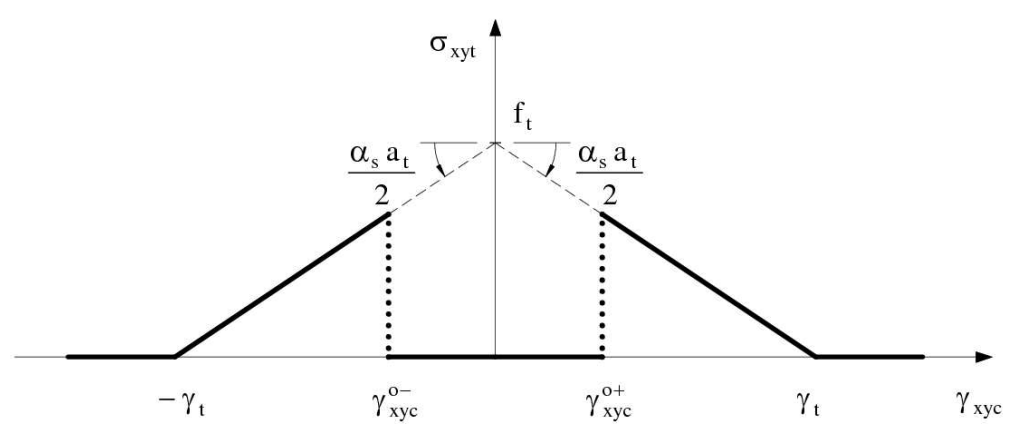
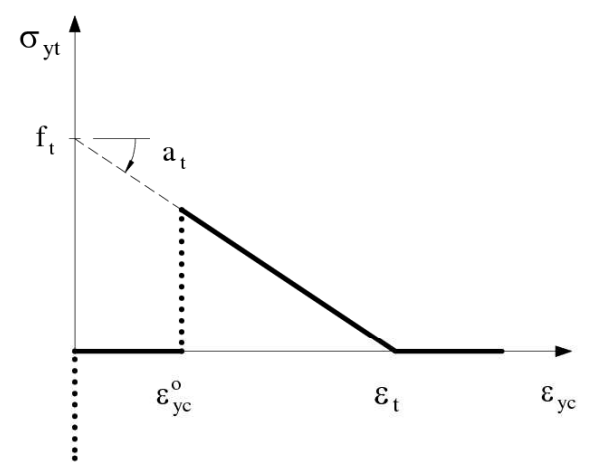
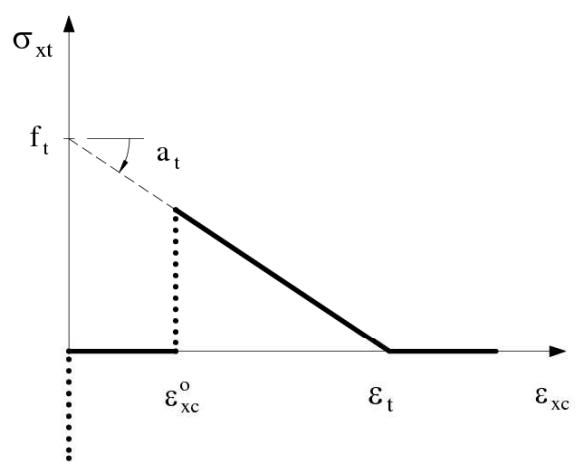
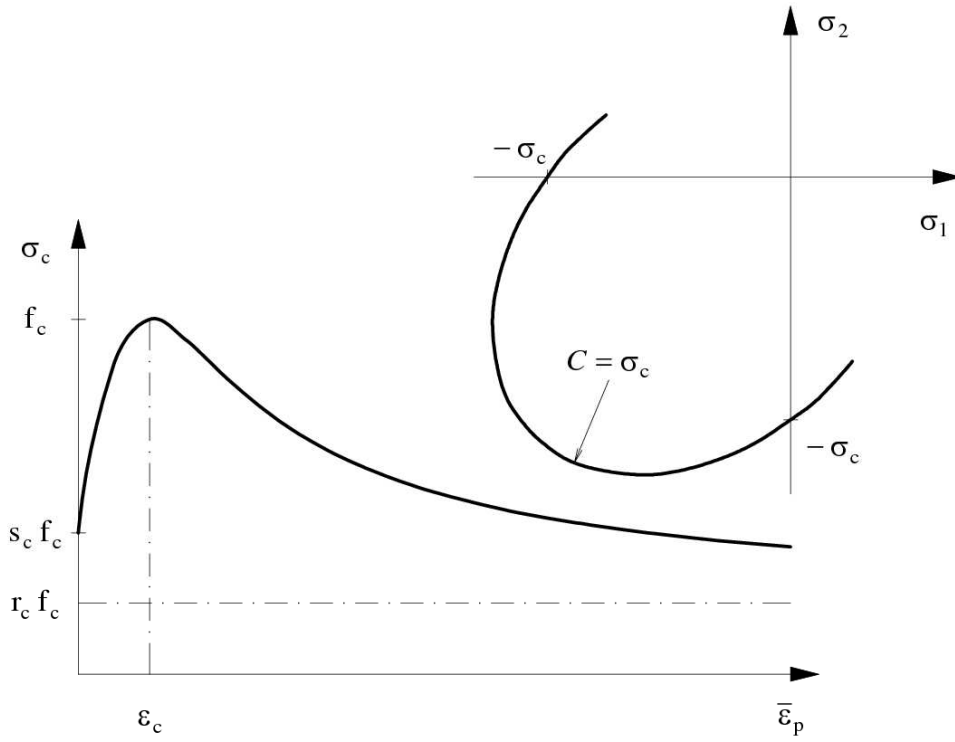
---

|                          |   |
|--------------------------|---|
| <b>Description</b>       | Fixed-crack elevated-temperature model for concrete.  |
| <b>No. of properties</b> | 37  |
| <b>Properties</b>        | <p>Young's modulus and temperatures:<br/> <math>(E_0, r_2, T_1, T_2, T_3)</math></p> <p>Possion's ratio and temperatures:<br/> <math>(\nu_0, r_2, T_1, T_2, T_3)</math></p> <p>Tensile strength and temperatures:<br/> <math>(f_{t0}, r_2, T_1, T_2, T_3)</math></p> <p>Tensile softening slope and temperatures:<br/> <math>(a_{t0}, r_2, T_1, T_2, T_3)</math></p> <p>Thermal strain and temperatures<br/> <math>(\epsilon_{th1}, r_3, T_1, T_2, T_3)</math></p> <p>Compressive strength and temperatures:<br/> <math>(f_{c0}, r_2, T_1, T_2, T_3)</math></p> <p>Normalised initial compressive strength: <math>(s_c)</math></p> <p>Normalised residual compressive strength: <math>(r_c)</math></p> <p>Normalised strain increment beyond <math>\epsilon_c</math>: <math>(m_c)</math></p> <p>Factor for biaxial compressive interaction: <math>(b_c)</math></p> <p>Elastic shear retention factor: <math>(\beta_s)</math></p> <p>Factor scaling direct tensile stresses for shear interaction: <math>(\Phi_s)</math></p> <p>Normalised shear softening relative to direct tensile softening: <math>(\gamma_s)</math></p> |
| <b>Application</b>       | <p>Representation of tensile cracking and compressive nonlinearity, including softening effects.</p> <p>Modelling of crack opening and closure, the latter being an important requirement under dynamic loading and fire conditions</p> <p>Consideration of the effects of elevated temperature, both in terms of the resulting thermal strains and the change of material properties</p>   |
| <b>Restrictions</b>      |   |

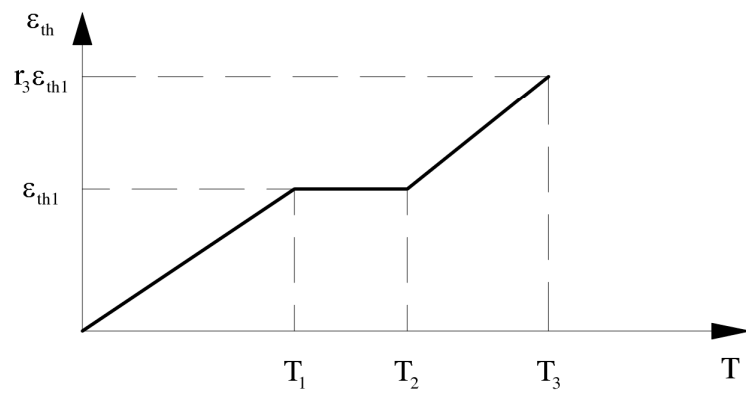
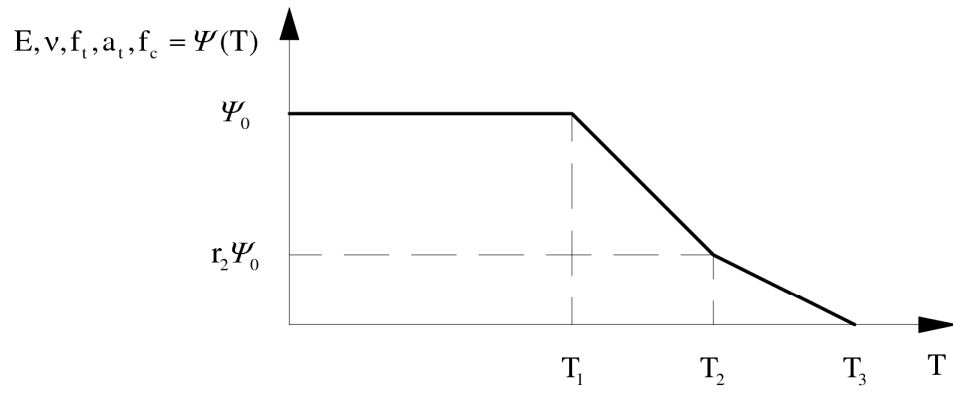
---



---



Material model *con11* (Cont'd...)



*Material model con11*

---

---

|                          |  |
|--------------------------|--|
| <b>Description</b>       | Material properties for connection components/connected member at elevated temperature.  |
| <b>No. of properties</b> | 45   |
| <b>Properties</b>        | Ultimate strength, temperatures and reduction factors for quadlinear description:<br>$(\sigma_u, T_{r1,1}, r_{1,1}, T_{r2,1}, r_{2,1}, T_{r3,1}, r_{3,1}, T_{r4,1}, r_{4,1})$<br>Young's modulus, temperatures and reduction factors:<br>$(E, T_{r1,2}, r_{1,2}, T_{r2,2}, r_{2,2}, T_{r3,2}, r_{3,2}, T_{r4,2}, r_{4,2})$<br>Reduced strain hardening coefficient, temperatures and reduction factors:<br>$(\mu_r, T_{r1,3}, r_{1,3}, T_{r2,3}, r_{2,3}, T_{r3,3}, r_{3,3}, T_{r4,3}, r_{4,3})$<br>Yield strength , temperatures and reduction factors:<br>$(\sigma_y, T_{r1,4}, r_{1,4}, T_{r2,4}, r_{2,4}, T_{r3,4}, r_{3,4}, T_{r4,4}, r_{4,4})$<br>Strain hardening coefficient, temperatures and reduction factors:<br>$(\mu, T_{r1,5}, r_{1,5}, T_{r2,5}, r_{2,5}, T_{r3,5}, r_{3,5}, T_{r4,5}, r_{4,5})$ |
| <b>Application</b>       | Requires the specification of the compressive strength, the peak compressive strain, the limit compressive strain at zero stress, the thermal strain and their variations with temperature. Note that $r_2$ and $r_3$ can be greater than 1.   |
| <b>Restrictions</b>      | Can be used to define material properties for joint element <a href="#">jbc2</a> .   |

---

---

## *beth*

---

---

|                                 |   |
|---------------------------------|---|
| <b><i>Description</i></b>       | Elastic isotropic material model with thermal strains.  |
| <b><i>No. of properties</i></b> | 3   |
| <b><i>Properties</i></b>        | Young's modulus ( E )<br>Poisson's ratio ( $\nu$ )<br>[ Coefficient of thermal expansion ( $\alpha$ ) ] |
| <b><i>Application</i></b>       | Can be used for 1D, 2D and 3D elements.   |

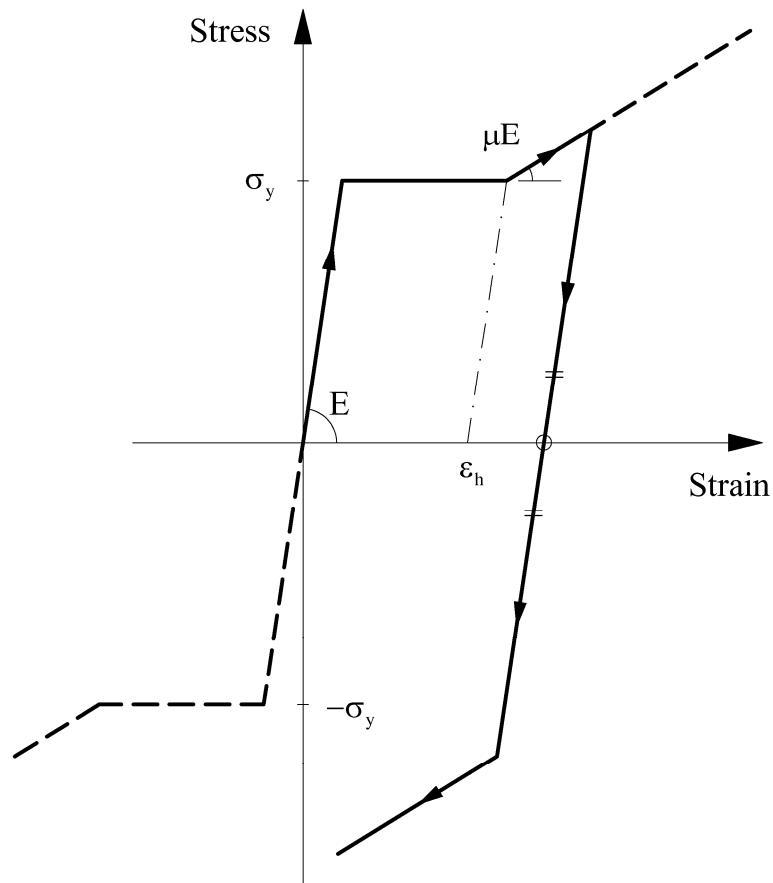
---

---

---

|                          |  |                  |
|--------------------------|--|------------------|
| <b>Description</b>       | Biaxial/triaxial elasto-plastic material model with <i>isotropic</i> strain-hardening. |                  |
| <b>No. of properties</b> | 5  |                  |
| <b>Properties</b>        | Young's modulus  | ( $E$ )          |
|                          | Possion's ratio  | ( $\nu$ )        |
|                          | Yield strength   | ( $\sigma_y$ )   |
|                          | Strain-hardening parameter   | ( $\mu$ )        |
|                          | Plastic strain at onset of hardening   | ( $\epsilon_h$ ) |
| <b>Application</b>       | Can be used for 1D, 2D and 3D elements   |                  |

---



*Material model bnsi*

*bnsk*

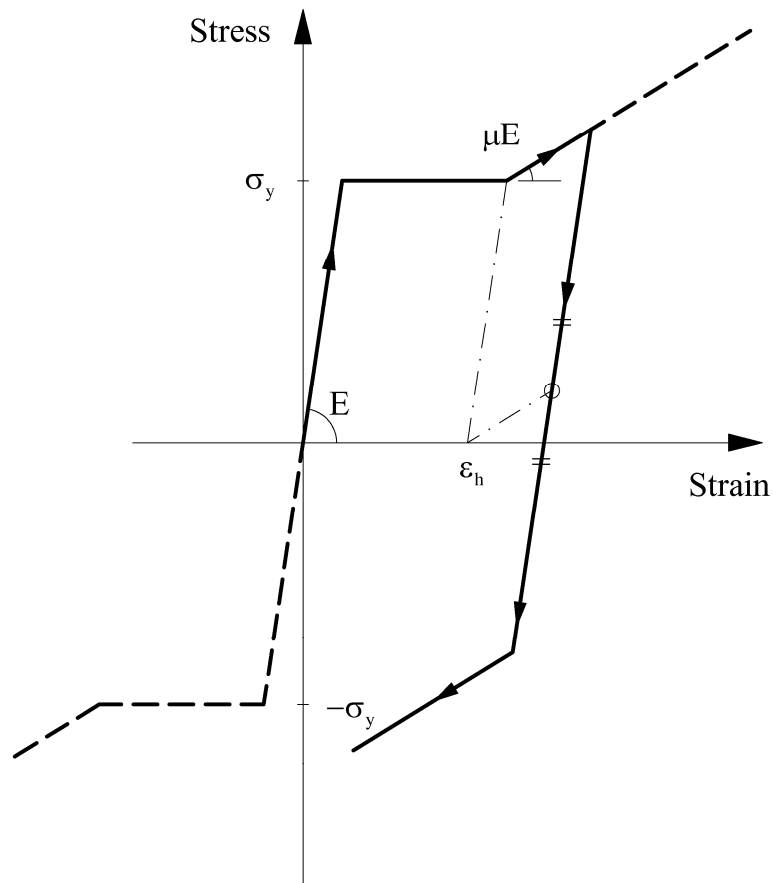
---

---

|                          |  |                  |
|--------------------------|--|------------------|
| <b>Description</b>       | Biaxial/triaxial elasto-plastic material model with <i>kinematic</i> strain-hardening. |                  |
| <b>No. of properties</b> | 5  |                  |
| <b>Properties</b>        | Young's modulus  | ( E )            |
|                          | Possion's ratio  | ( $\nu$ )        |
|                          | Yield strength   | ( $\sigma_y$ )   |
|                          | Strain-hardening parameter   | ( $\mu$ )        |
|                          | Plastic strain at onset of hardening   | ( $\epsilon_h$ ) |
| <b>Application</b>       | Can be used for 1D, 2D and 3D elements   |                  |

---

---



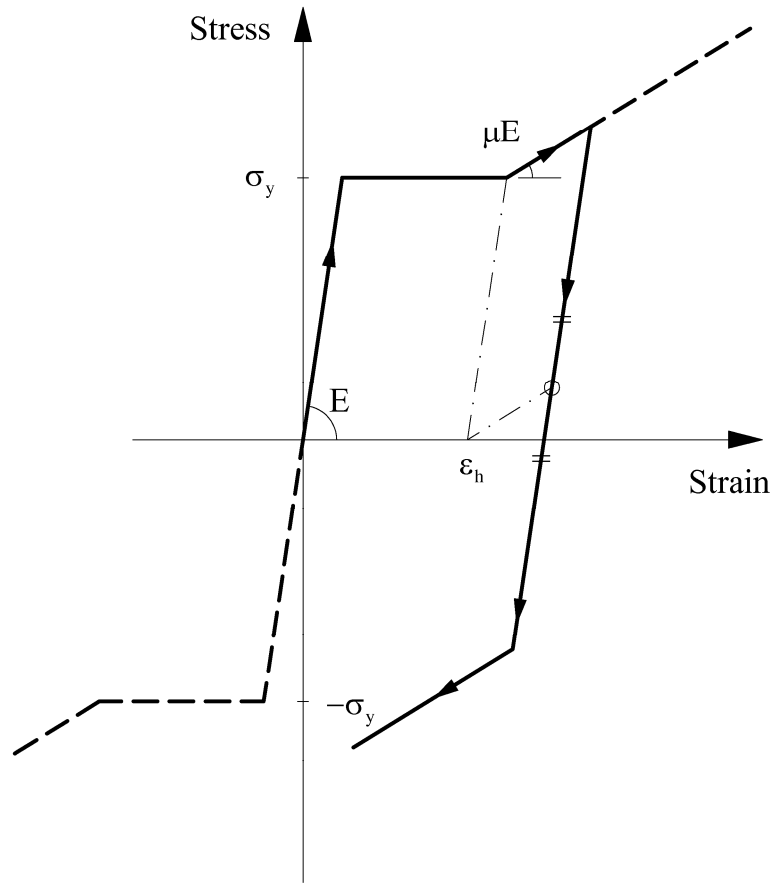
Material model *bnsk*



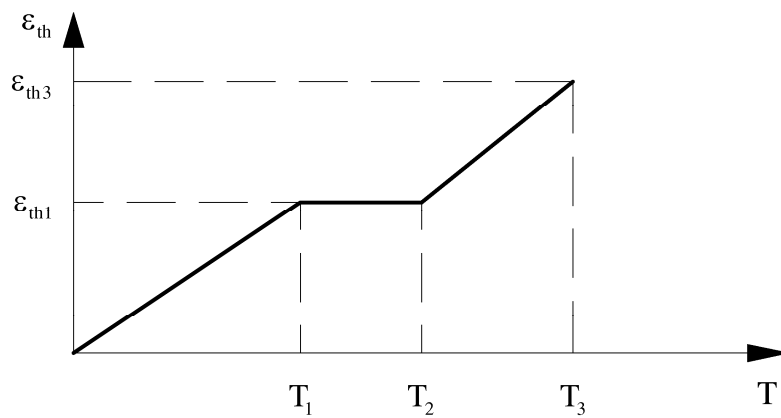
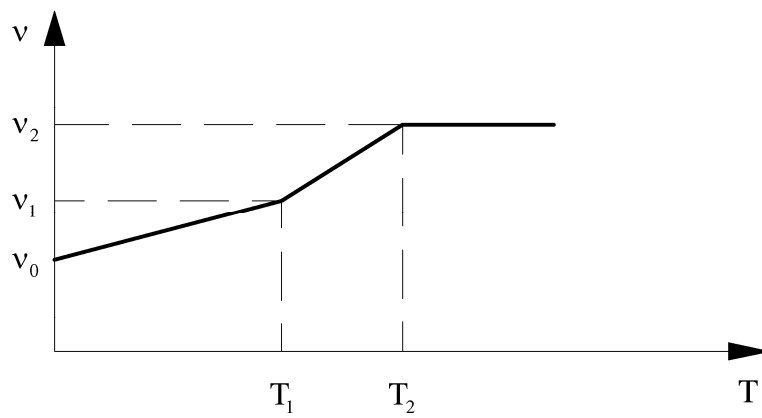
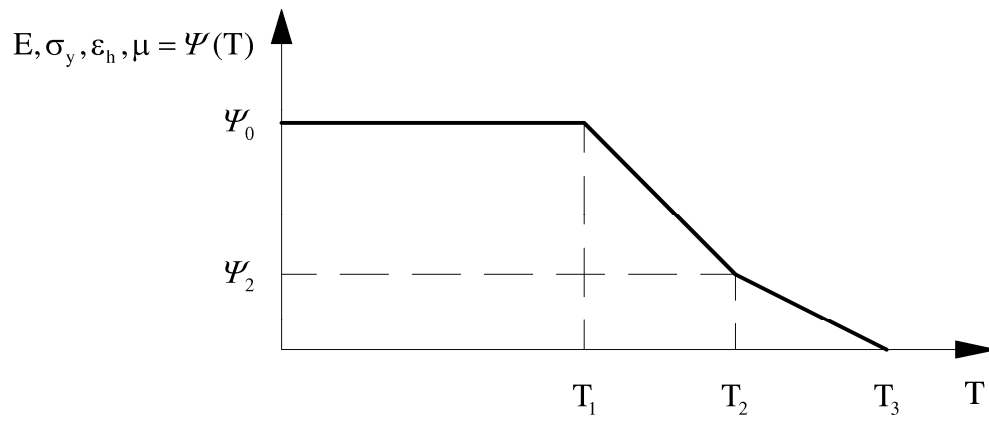
|                          |  |
|--------------------------|--|
| <b>Description</b>       | Triaxial elasto-plastic material model with <i>kinematic</i> strain-hardening and elevated temperature effects.  |
| <b>No. of properties</b> | 30   |
| <b>Properties</b>        | Young's modulus and temperatures:<br>( $E_0, E_2, T_1, T_2, T_3$ )<br>Yield strength and temperatures<br>( $\sigma_{y0}, \sigma_{y2}, T_1, T_2, T_3$ )<br>Plastic strain at onset of hardening<br>( $\varepsilon_{h0}, \varepsilon_{h2}, T_1, T_2, T_3$ )<br>Strain-hardening parameter<br>( $\mu_0, \mu_2, T_1, T_2, T_3$ )<br>Poisson's ratio and temperatures:<br>( $\nu_0, \nu_1, \nu_2, T_1, T_2$ )<br>Thermal strain and temperatures<br>( $\varepsilon_{th1}, \varepsilon_{th3}, T_1, T_2, T_3$ ) |
| <b>Application</b>       | 3D brick elements  |

---

---



*Material model **tpth** (Cont'd...)*



*Material model **tpth***

## **Chapter 4. JOINT ELEMENT CURVES**

This section describes the force-displacement curves available in ADAPTIC for use by joint elements. Each curve is referred to by a unique name, displayed at the top of the following pages, and requires the specification of a number of parameters.

## *lin*

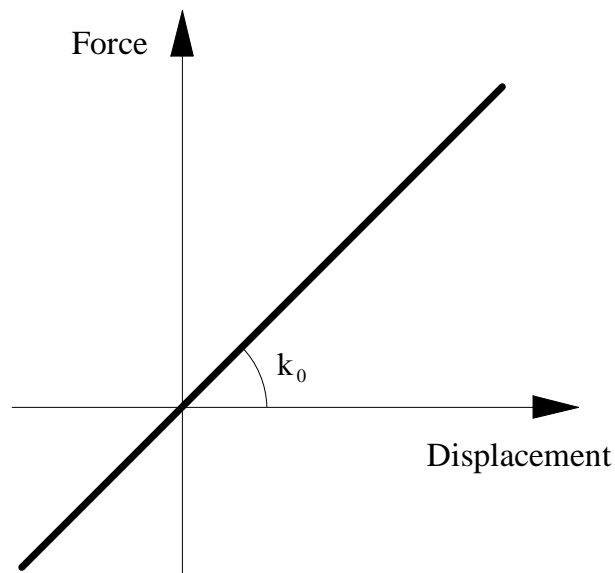
---

---

|                        |                                       |
|------------------------|---------------------------------------|
| <b>Description</b>     | Linear elastic curve type.            |
| <b>Parameters</b>      | $k_0$                                 |
| <b>Characteristics</b> | Linear elastic curve.                 |
| <b>Application</b>     | Elastic joint action characteristics. |
| <b>Restrictions</b>    |                                       |

---

---



*Force-displacement curve **lin***

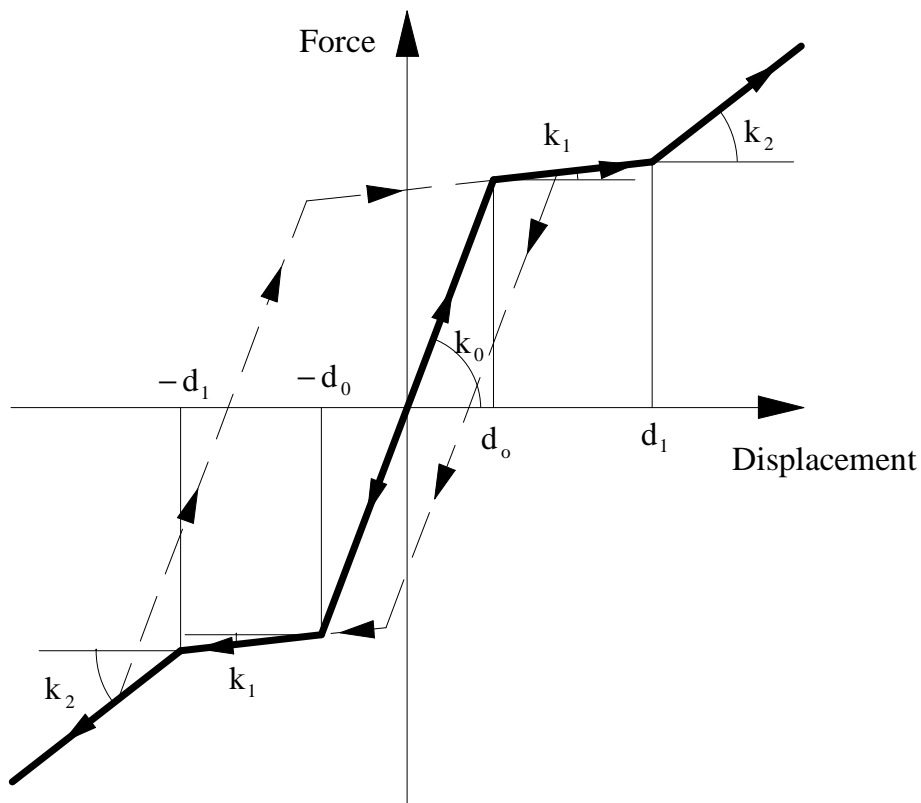
---

---

|                        |   |
|------------------------|---|
| <b>Description</b>     | Trilinear symmetric elasto-plastic curve type.  |
| <b>Parameters</b>      | $k_0$ , $d_0$ , $k_1$ , $d_1$ & $k_2$ , specified in this order.  |
| <b>Characteristics</b> | Trilinear symmetric elasto-plastic curve.<br>Unloading is performed kinematically to the extension of the second branch of the curve. |
| <b>Application</b>     | Elasto-plastic joint action.  |
| <b>Restrictions</b>    | All $k$ 's must be positive.<br>$k_1$ & $k_2$ must not be more than $k_0$ .   |

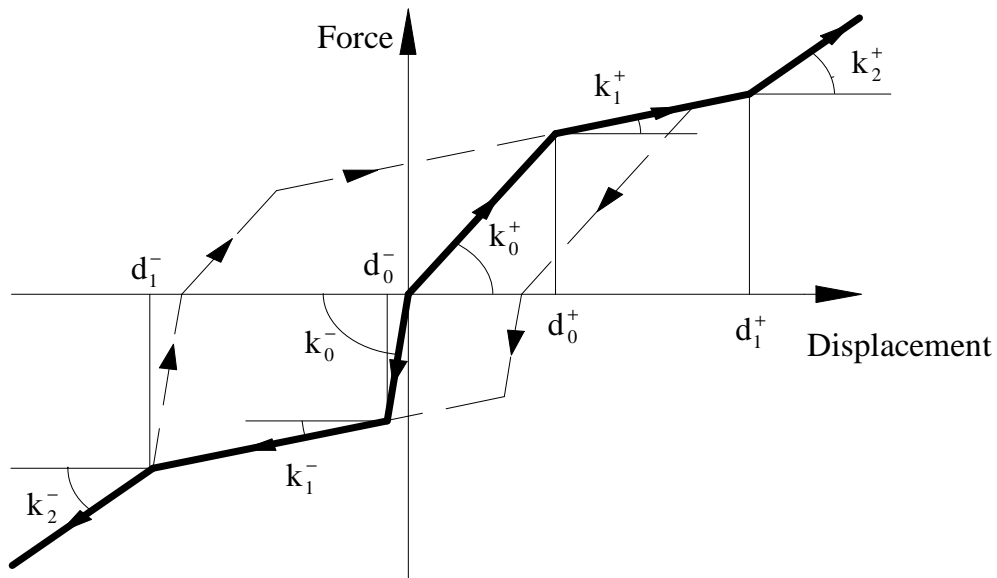
---

---



*Force-displacement curve smtr*

|                        |  |
|------------------------|--|
| <b>Description</b>     | Trilinear asymmetric elasto-plastic curve type.  |
| <b>Parameters</b>      | $(k_0, d_0, k_1, d_1, k_2)^+$ & $(k_0, d_0, k_1, d_1, k_2)^-$ specified in this order.   |
| <b>Characteristics</b> | Trilinear asymmetric elasto-plastic curve.<br>Unloading is performed kinematically to the extension of the second branch of the reloading curve.   |
| <b>Application</b>     | Elasto-plastic joint action. Structural gaps.<br>The following parameters represent a curve with zero resistance until a specific negative displacement $-D$ is achieved:<br>$(?, 0, 0, ?, 0, ?, 0, 0, -D, ?)$ |
| <b>Restrictions</b>    | All $k$ 's must be positive. $k_1$ & $k_2$ must not be more than $k_0$ for the positive and negative displacement regions.   |



*Force-displacement curve astr*

## *rigid*

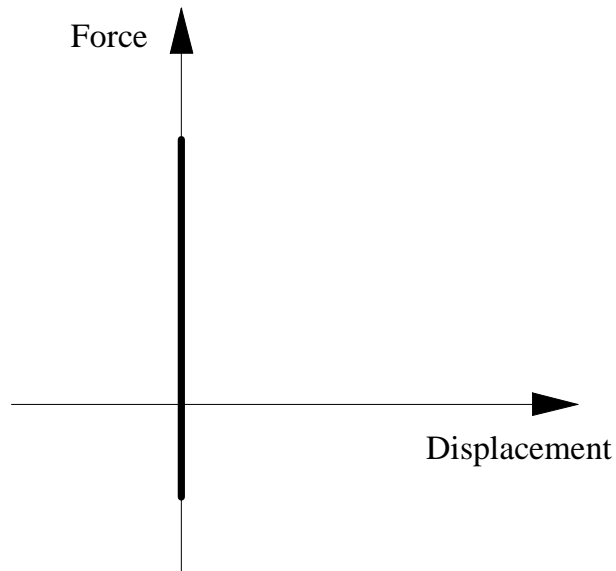
---

---

|                        |  |
|------------------------|--|
| <b>Description</b>     | Rigid curve type.  |
| <b>Parameters</b>      | None.  |
| <b>Characteristics</b> | Rigid curve.   |
| <b>Application</b>     | Constrains a local freedom to zero.<br>Avoids numerical problems that can occur with the <a href="#">lin</a> curve type using a large stiffness. |
| <b>Restrictions</b>    |  |

---

---



*Force-displacement curve **rigid***



## *contact*

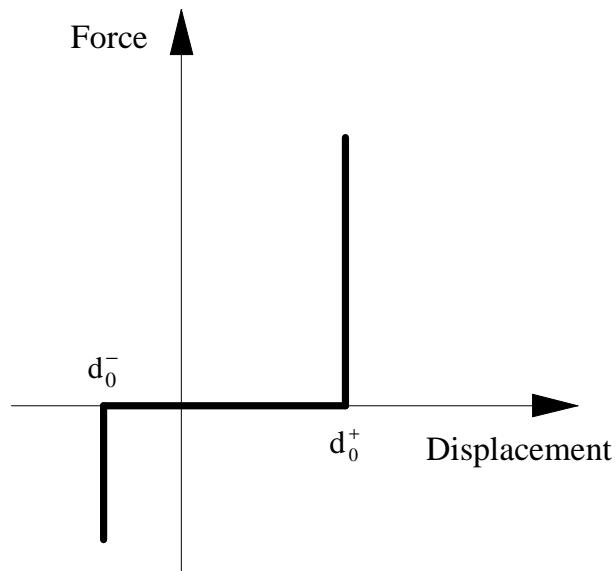
---

---

|                        |   |
|------------------------|---|
| <b>Description</b>     | Contact curve type.   |
| <b>Parameters</b>      | $d_0^-$ & $d_0^+$ .   |
| <b>Characteristics</b> | Gap-contact curve, with a gap between $d_0^-$ and $d_0^+$ . |
| <b>Application</b>     | Modelling of gaps with arbitrary lower/upper limits.        |
| <b>Restrictions</b>    |   |

---

---



*Force-displacement curve **contact***

## *plastic*

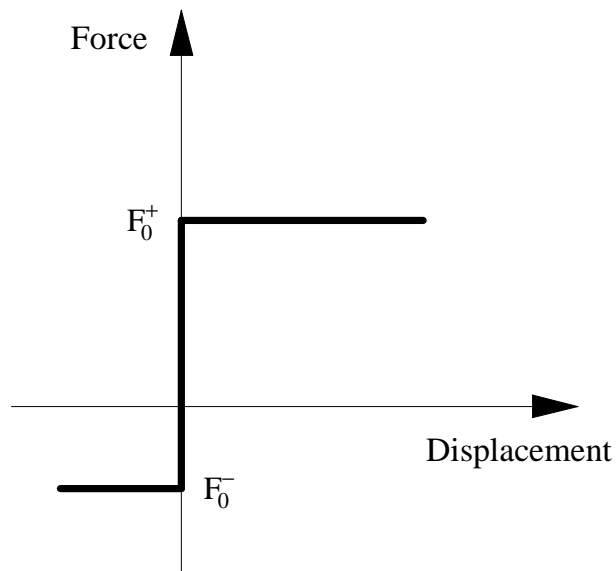
---

---

|                        |  |
|------------------------|--|
| <b>Description</b>     | Plastic curve type.  |
| <b>Parameters</b>      | $F_0^-$ & $F_0^+$ .  |
| <b>Characteristics</b> | Rigid plastic curve, with plastic limits $F_0^-$ & $F_0^+$ .           |
| <b>Application</b>     | Modelling of rigid response with arbitrary lower/upper plastic limits. |
| <b>Restrictions</b>    |  |

---

---



*Force-displacement curve plastic*

## *radcont*

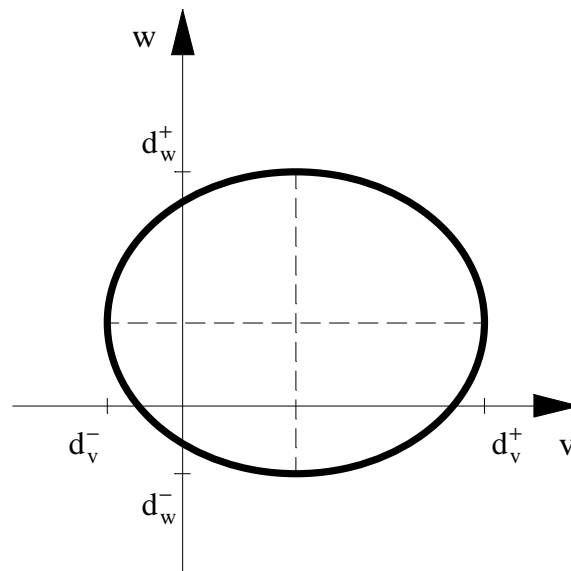
---

---

|                        |  |
|------------------------|--|
| <b>Description</b>     | Radial contact curve.  |
| <b>Parameters</b>      | $(d_v^- \text{ \& } d_v^+)$ or $(d_w^- \text{ \& } d_w^+)$ .                                   |
| <b>Characteristics</b> | Coupled gap-contact curve between local v and w freedoms.<br>Elliptical gap.                   |
| <b>Application</b>     | Contact between concentric circular tubular members, for which the gap is defined by a circle. |
| <b>Restrictions</b>    | Element type <a href="#">jel3</a> .<br>To be used simultaneously for local v and w freedoms.   |

---

---



*Contact gap for curve **radcont***

# Chapter 5. CROSS-SECTION TYPES

The ADAPTIC library also includes a number of pre-defined cross-section types described briefly below:

| <b><u>Type</u></b>          | <b><u>Description</u></b>                 |
|-----------------------------|---|
| <a href="#"><u>rss</u></a>  | Rectangular solid section                 |
| <a href="#"><u>chs</u></a>  | Circular hollow section                   |
| <a href="#"><u>isec</u></a> | General purpose I- or T-section           |
| <a href="#"><u>pnci</u></a> | Partially encased composite I-section     |
| <a href="#"><u>fnci</u></a> | Fully encased composite I-section         |
| <a href="#"><u>rccs</u></a> | Reinforced concrete column section        |
| <a href="#"><u>rcts</u></a> | Reinforced concrete T-section             |
| <a href="#"><u>flxw</u></a> | Reinforced concrete flexural wall section |

The degree of accuracy in modelling the above sections depends on the formulation utilising the cross-section.

Cubic formulations ([cbp2](#), [cbp3](#)) provide detailed modelling of a cross-section through its discretisation into a number of areas where the uniaxial material response is monitored according to the previous material models.

Plastic-hinge formulations ([gph2](#), [gph3](#)) derive a plastic interaction surface between the cross-sectional bending moments and axial force, which is combined with the associated flow rule to provide approximate modelling of steel members. The plastic hinge capability is not extended to reinforced concrete sections.

Elastic formulations utilise constant elastic rigidities for bending, axial and torsional actions derived for given cross-sectional configurations. As such they are only accurate for steel members, since they do not account for concrete cracking.

This section describes the cross-section types available in ADAPTIC. Each type is referred to by a unique name, displayed at the top of the following pages, and requires the specification of a number of materials and dimensions in the order indicated.

*rss*

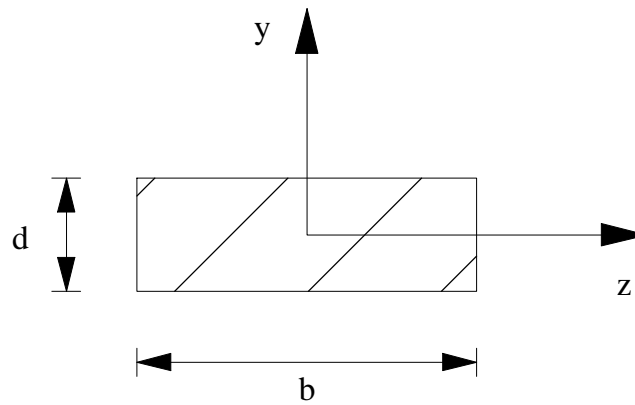
---

---

|                          |   |
|--------------------------|---|
| <b>Description</b>       | Rectangular solid section.                      |
| <b>No. of materials</b>  | 1   |
| <b>No. of dimensions</b> | 2   |
| <b>Dimensions</b>        | Width ( b )<br>Depth ( d )                      |
| <b>Application</b>       | Rectangular solid sections of uniform material. |

---

---



*Section rss*

*chs*

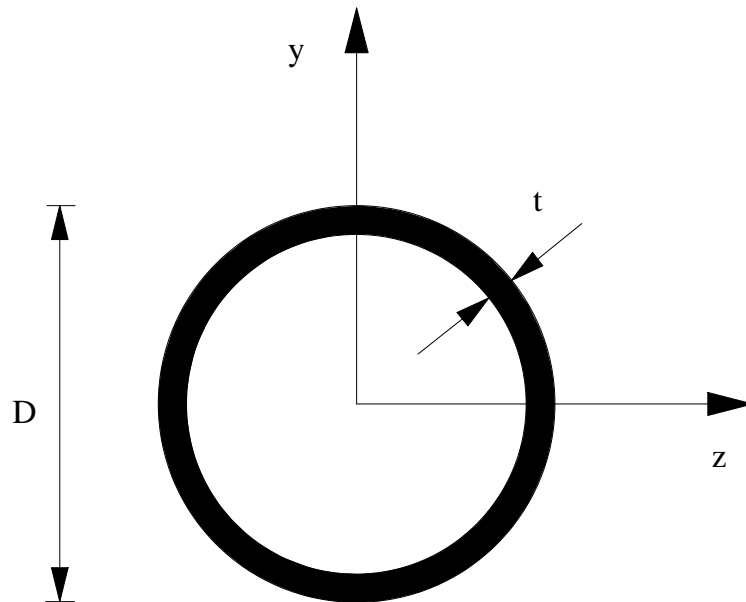
---

---

|                          |   |
|--------------------------|---|
| <b>Description</b>       | Thin circular hollow section.                 |
| <b>No. of materials</b>  | 1   |
| <b>No. of dimensions</b> | 2   |
| <b>Dimensions</b>        | Outer diameter ( D )<br>Tube thickness ( t )  |
| <b>Application</b>       | Circular hollow sections of uniform material. |

---

---



*Section chs*

## *isec*

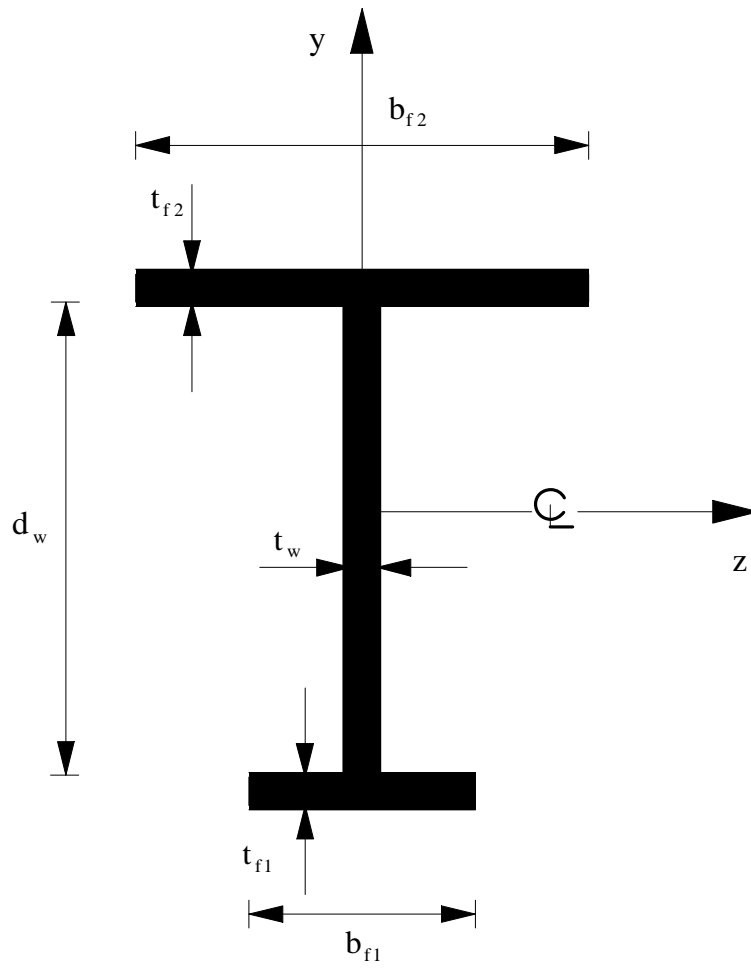
---

---

|                                 |  |
|---------------------------------|--|
| <b><i>Description</i></b>       | General purpose I- or T-section.             |
| <b><i>No. of materials</i></b>  | 1  |
| <b><i>No. of dimensions</i></b> | 6  |
| <b><i>Dimensions</i></b>        | Bottom flange width            ( $b_{f1}$ )  |
|                                 | Bottom flange thickness        ( $t_{f1}$ )  |
|                                 | Top flange width                ( $b_{f2}$ ) |
|                                 | Top flange thickness          ( $t_{f2}$ )   |
|                                 | Web depth                        ( $d_w$ )   |
|                                 | Web thickness                  ( $t_w$ )     |
| <b><i>Application</i></b>       | I- or T-sections of uniform material.        |

---

---



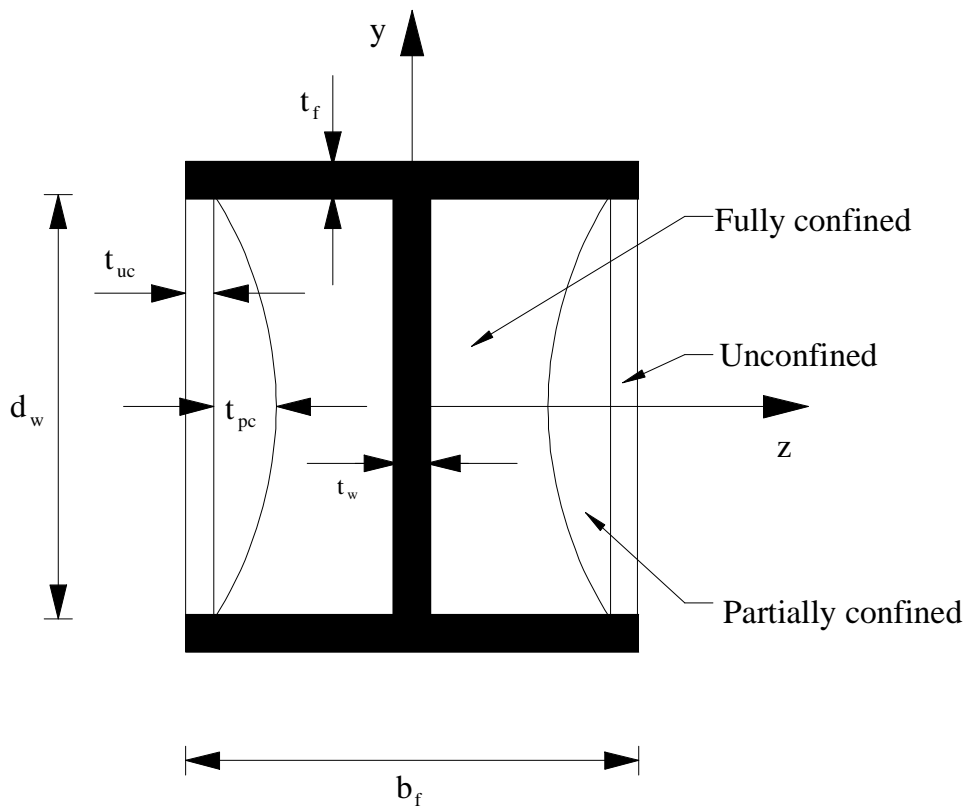
*Section isec*



|                          |  |                           |
|--------------------------|--|---------------------------|
| <b>Description</b>       | Partially encased composite I-section.   |                           |
| <b>No. of materials</b>  | 4, specified in this order:<br>I-section<br>Unconfined region<br>Partially confined region<br>Fully confined region  |                           |
| <b>No. of dimensions</b> | 6  |                           |
| <b>Dimensions</b>        | Flange width   | ( $b_f$ )                 |
|                          | Flange thickness   | ( $t_f$ )                 |
|                          | Web depth  | ( $d_w$ )                 |
|                          | Web thickness  | ( $t_w$ )                 |
|                          | Unconfinement ratio  | ( $r_{uc}$ ) <sup>*</sup> |
|                          | Partial confinement ratio  | ( $r_{pc}$ ) <sup>*</sup> |
| <b>Application</b>       | Partially encased composite I-sections, with three different concrete materials to represent confinement effects.  |                           |
|                          | (*) $r_{uc} = 2 t_{uc} / (b_f - t_w)$ & $r_{pc} = 2 t_{pc} / (b_f - t_w)$ , where $t_{uc}$ and $t_{pc}$ are the thickness of the unconfined and confined parts of the section, respectively. |                           |

---

---

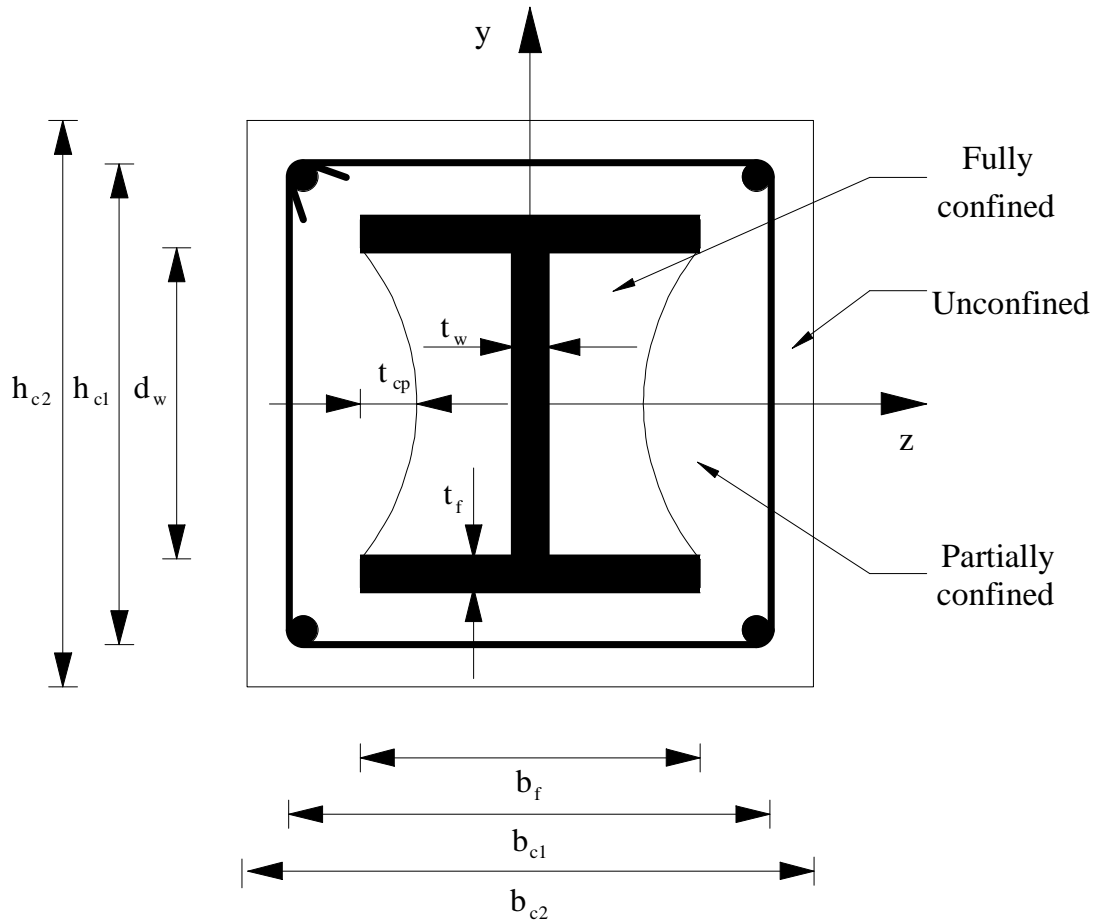


*Section pnci*

|                          |   |               |
|--------------------------|---|---------------|
| <b>Description</b>       | Fully-encased composite I-section.  |               |
| <b>No. of materials</b>  | 4, specified in this order:<br>I-section<br>Unconfined region<br>Partially confined region<br>Fully confined region           |               |
| <b>No. of dimensions</b> | 9   |               |
| <b>Dimensions</b>        | Flange width  | ( $b_f$ )     |
|                          | Flange thickness  | ( $t_f$ )     |
|                          | Web depth   | ( $d_w$ )     |
|                          | Web thickness   | ( $t_w$ )     |
|                          | Partial confinement ratio   | ( $r_{pc}$ )* |
|                          | Stirrup width   | ( $b_{cl}$ )  |
|                          | Section width   | ( $b_{c2}$ )  |
|                          | Stirrup depth   | ( $h_{cl}$ )  |
|                          | Section depth   | ( $h_{c2}$ )  |
| <b>Application</b>       | Fully encased composite I-sections, with three different concrete materials to represent confinement effects.                 |               |
|                          | (*) $r_{pc} = 2 t_{pc} / (b_f - t_w)$ , where $t_{pc}$ is the depth of the partially confined part beyond the section flange. |               |

---

---

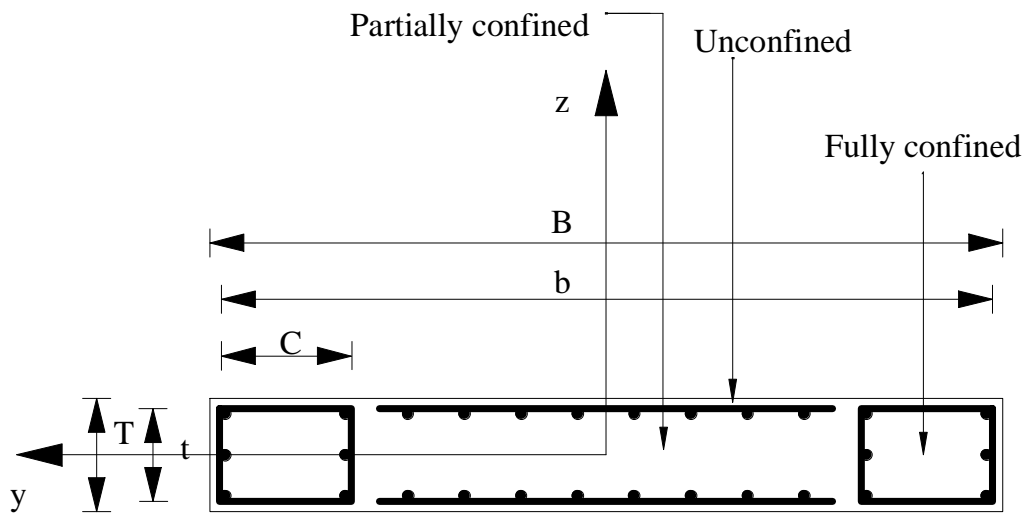


*Section fnci*

|                          |  |
|--------------------------|--|
| <b>Description</b>       | Flexural wall section.   |
| <b>No. of materials</b>  | 4, specified in this order:<br>Reinforcement<br>Unconfined region<br>Partially confined region<br>Fully confined region  |
| <b>No. of dimensions</b> | 2D analysis:<br>5 + 2 ( Reinforcement <u>layers</u> on one side of z-axis )<br>3D analysis:<br>5 + 3 ( Reinforcement <u>bars</u> in one y-z quadrant )   |
| <b>Dimensions</b>        | Wall width ( B )<br>Confined width ( b )<br>Wall thickness ( T )<br>Confined thickness ( t )<br>Depth of fully confined region ( C )<br>2D analysis:<br>( $A_i, y_i$ ) for each reinforcement <u>layer</u> on one side of the z-axis.<br>3D analysis:<br>( $A_i, y_i, z_i$ ) for each reinforcement <u>bar</u> in the positive y-z quadrant. |
| <b>Application</b>       | Symmetric flexural walls.  |
| <b>Restrictions</b>      | Section is assumed symmetric about the y-z origin, hence only one side of the reinforcement need to be specified.  |

---

---



*Section flxw*

## *rccs*

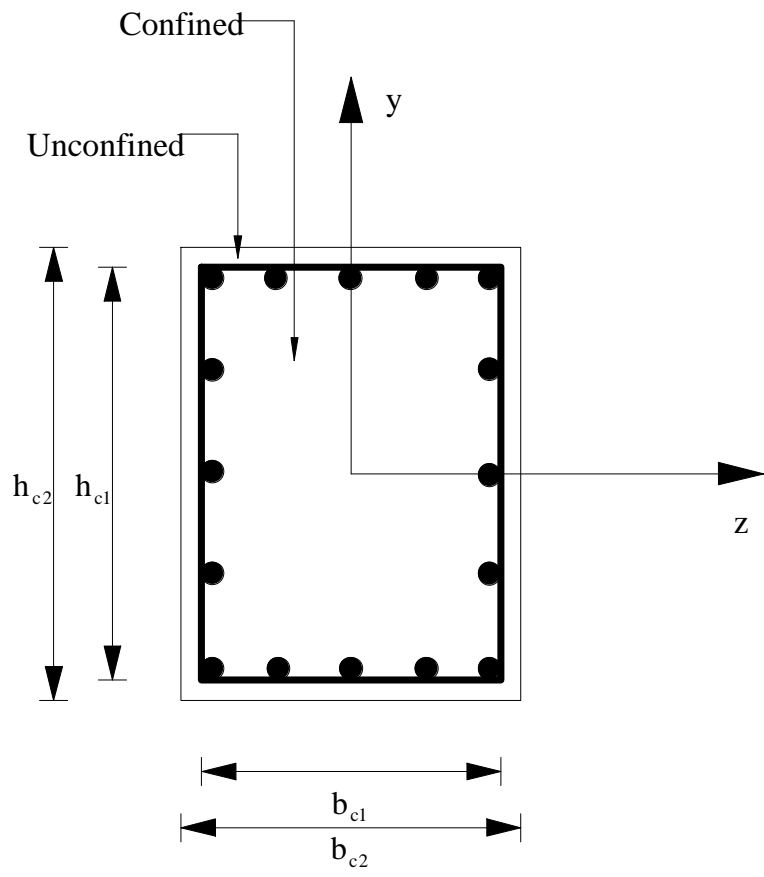
---

---

|                                 |  |
|---------------------------------|--|
| <b><i>Description</i></b>       | Reinforced concrete column section.  |
| <b><i>No. of materials</i></b>  | 3, specified in this order:<br>Reinforcement<br>Unconfined region<br>Confined region   |
| <b><i>No. of dimensions</i></b> | 2D analysis:<br>4 + 2 ( Reinforcement <u>layers</u> on one side of z-axis )<br>3D analysis:<br>4 + 3 ( Reinforcement <u>bars</u> in one y-z quadrant )   |
| <b><i>Dimensions</i></b>        | Section depth ( $h_{c1}$ )<br>Stirrup depth ( $h_{c2}$ )<br>Section width ( $b_{c1}$ )<br>Stirrup width ( $b_{c2}$ )<br>2D analysis:<br>( $A_i, y_i$ ) for each reinforcement <u>layer</u> on one side of the z-axis.<br>3D analysis:<br>( $A_i, y_i, z_i$ ) for each reinforcement <u>bar</u> in the positive y-z quadrant. |
| <b><i>Application</i></b>       | Symmetric reinforced concrete columns.   |
| <b><i>Restrictions</i></b>      | Section is assumed symmetric about the y-z origin, hence only one side of the reinforcement need to be specified.  |

---

---



*Section **RCC***



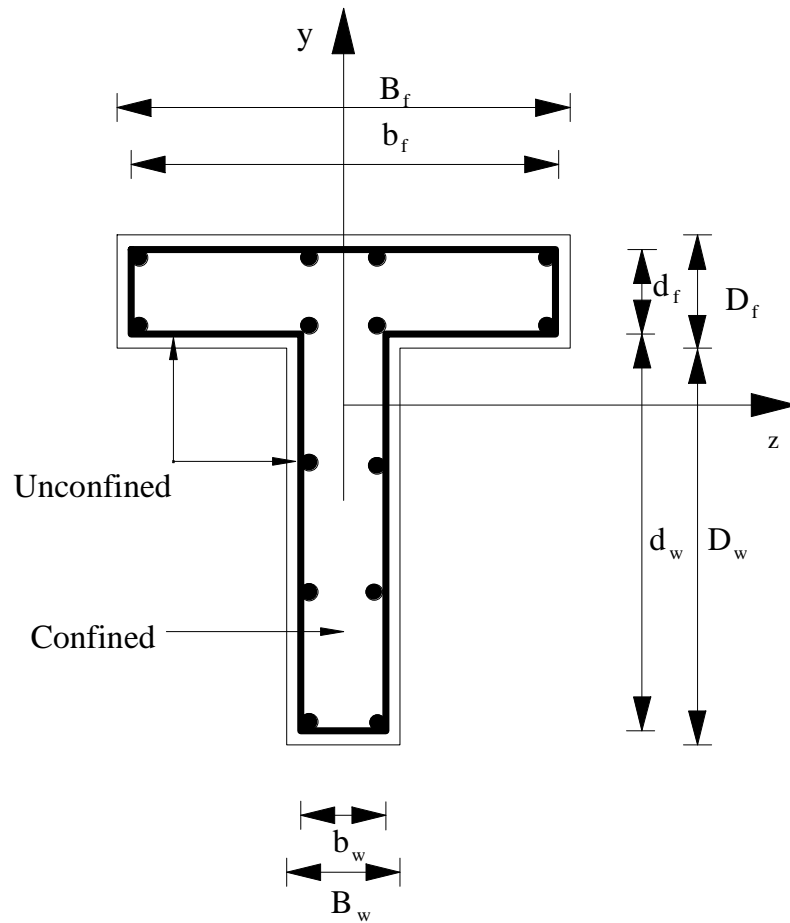
---



---

|                          |  |
|--------------------------|--|
| <b>Description</b>       | Reinforced concrete T-section.   |
| <b>No. of materials</b>  | 3, specified in this order:<br>Reinforcement<br>Unconfined region<br>Confined region   |
| <b>No. of dimensions</b> | 2D analysis:<br>8 + 2 ( Reinforcement <u>layers</u> )<br>3D analysis:<br>8 + 3 ( Reinforcement <u>bars</u> on one side of y-axis )   |
| <b>Dimensions</b>        | Slab thickness                      ( $D_f$ )<br>Beam depth                         ( $D_w$ )<br>Confined depth in slab           ( $d_f$ )<br>Confined depth in beam           ( $d_w$ )<br>Slab effective width               ( $B_f$ )<br>Beam width                         ( $B_w$ )<br>Confined width in slab           ( $b_f$ )<br>Confined width in beam           ( $b_w$ )<br>2D analysis:<br>( $A_i, d_i^*$ ) for each reinforcement <u>layer</u> .<br>3D analysis:<br>( $A_i, d_i^*, z_i$ ) for each reinforcement <u>bar</u> on one side of<br>the y-axis. |
| <b>Application</b>       | Modelling of R/C beams with an effective slab width.   |
| <b>Restrictions</b>      | Symmetric section about the y-axis.<br>(*) $d_i$ is the distance of reinforcement layer/bar (i) from the bottom<br>fibre of the section.   |

---

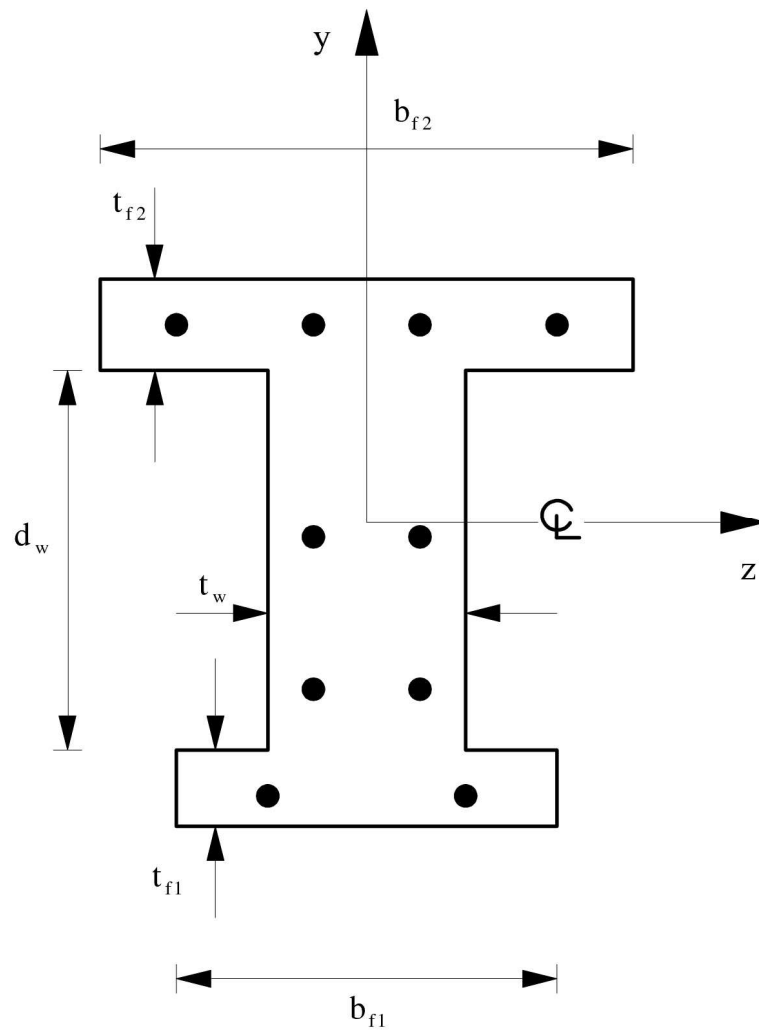


*Section rcts*

|                          |  |
|--------------------------|--|
| <b>Description</b>       | General purpose reinforced concrete I- or T-section.   |
| <b>No. of materials</b>  | 1  |
| <b>No. of dimensions</b> | 2D analysis:<br>6 + 2 ( Reinforcement <u>layers</u> )  |
| <b>Dimensions</b>        | Bottom flange width ( $b_{f1}$ )<br>Bottom flange thickness ( $t_{f1}$ )<br>Top flange width ( $b_{f2}$ )<br>Top flange thickness ( $t_{f2}$ )<br>Web depth ( $d_w$ )<br>Web thickness ( $t_w$ )<br>2D analysis:<br>( $A_i, d_i^*$ ) for each reinforcement <u>layer</u> . |
| <b>Application</b>       | General reinforced concrete I- or T-sections.  |
| <b>Restrictions</b>      | Symmetric section about the y-axis.<br>(* ) $d_i$ is the distance of reinforcement layer/bar (i) from the bottom fibre of the section.   |

---

---



*Section rcgs*

---



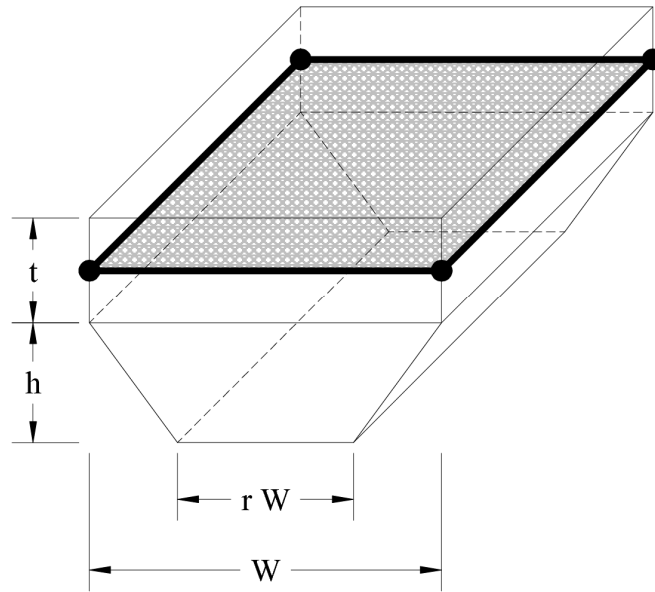
---

|                                 |  |                    |
|---------------------------------|--|--------------------|
| <b><i>Description</i></b>       | Composite floor slab section   |                    |
| <b><i>No. of materials</i></b>  | 4 specified in this order:<br>Deck parallel to the rib<br>Deck perpendicular to the rib<br>Reinforcement<br>Concrete                 |                    |
| <b><i>No. of dimensions</i></b> | 12   |                    |
| <b><i>Dimensions</i></b>        | Depth of cover:  | ( t )              |
|                                 | Depth of rib   | ( h )              |
|                                 | Rib geometric ratio  | ( r )              |
|                                 | Thickness of steel deck  | ( t <sub>d</sub> ) |
|                                 | Reinforcement area per unit length<br>in local x-direction   | ( t <sub>x</sub> ) |
|                                 | Location of reinforcement in x-direction<br>above (+)/below (-) reference mid-plane  | ( d <sub>x</sub> ) |
|                                 | Reinforcement area per unit length<br>in local y-direction   | ( t <sub>y</sub> ) |
|                                 | Location of reinforcement in y-direction<br>above (+)/below (-) reference mid-plane  | ( d <sub>y</sub> ) |
|                                 | The remaining 4 dimensions are for two additional<br>reinforcement layers in x and y-directions.                                     |                    |
| <b><i>Application</i></b>       | Composite floor slab cross-section consisting of ribbed<br>reinforced concrete acting compositely with trapezoidal steel<br>decking. |                    |

---



---



*Section **cslb***

## **Chapter 6. ELEMENT TYPES**

This section describes the element types available in ADAPTIC. Each type is referred to by a unique name, displayed at the top of the following pages, and requires the specification of a number of entries for its groups, connectivity and other modules.

## cbe2

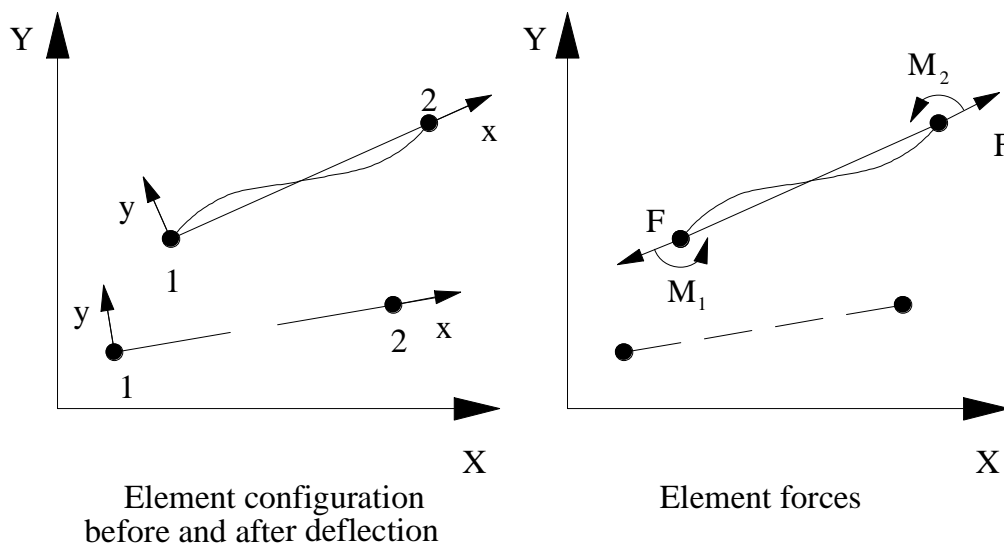
---

---

|                        |  |
|------------------------|--|
| <b>Description</b>     | Cubic 2D elastic element with uncoupled bending and axial actions.   |
| <b>Nodes</b>           | 2  |
| <b>Characteristics</b> | Accounts for large nodal displacements, but requires a number of elements to represent a member with significant beam-column action. |
| <b>Application</b>     | Elastic analysis of plane frames   |
| <b>Restrictions</b>    | Unable to model concrete cracking.   |
| <b>Group header</b>    | <b>sec.name</b> : An identifier referring to one of the <a href="#">cross-sections</a> declared in the <b>sections</b> module.       |

---

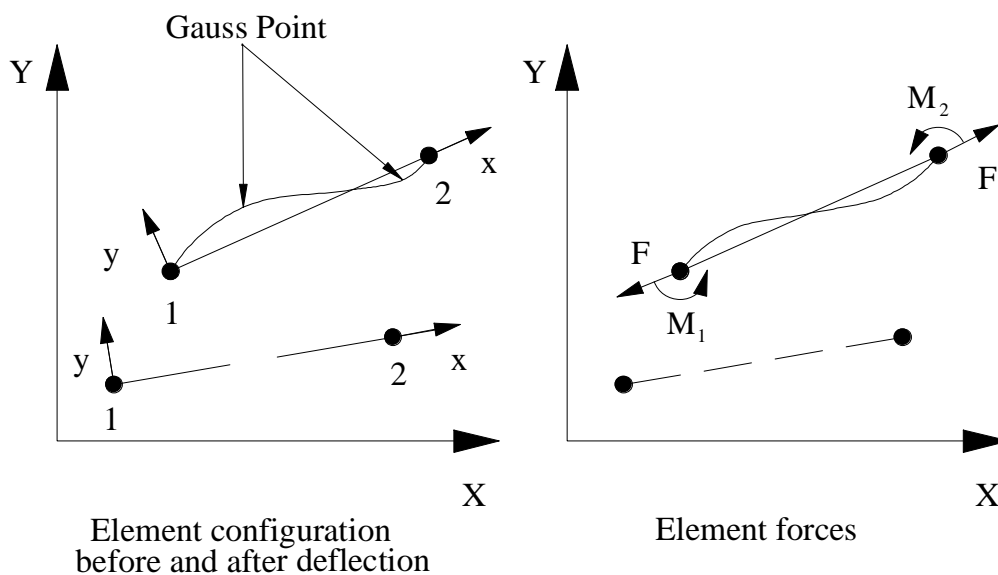
---



*Configuration and forces in local system of element type cbe2*



|                          |  |
|--------------------------|--|
| <b>Description</b>       | Cubic elasto-plastic 2D beam-column element.   |
| <b>Monitoring points</b> | 25 points usually adequate; depends on section type.   |
| <b>Nodes</b>             | 2  |
| <b>Characteristics</b>   | <p>Geometric and material nonlinearities.</p> <p>Numerical integration performed over two Gauss points.</p> <p>A number of monitoring areas used at each Gauss section to monitor material direct stress and strains.</p> <p>Predicts global member behaviour based on a material stress-strain relationship.</p> <p>A number of elements per member, usually over 5, must be used for reasonable accuracy in inelastic modelling.</p> |
| <b>Application</b>       | Modelling of inelastic members in plane frames.  |
| <b>Restrictions</b>      |  |
| <b>Group header</b>      | <p><b>sec.name:</b> An identifier referring to one of the <a href="#">cross-sections</a> declared in the <b>sections</b> module.</p> <p><b>monitoring.points:</b> Defines the number of points for monitoring stresses and strains within a <a href="#">cross-section</a>.</p>   |



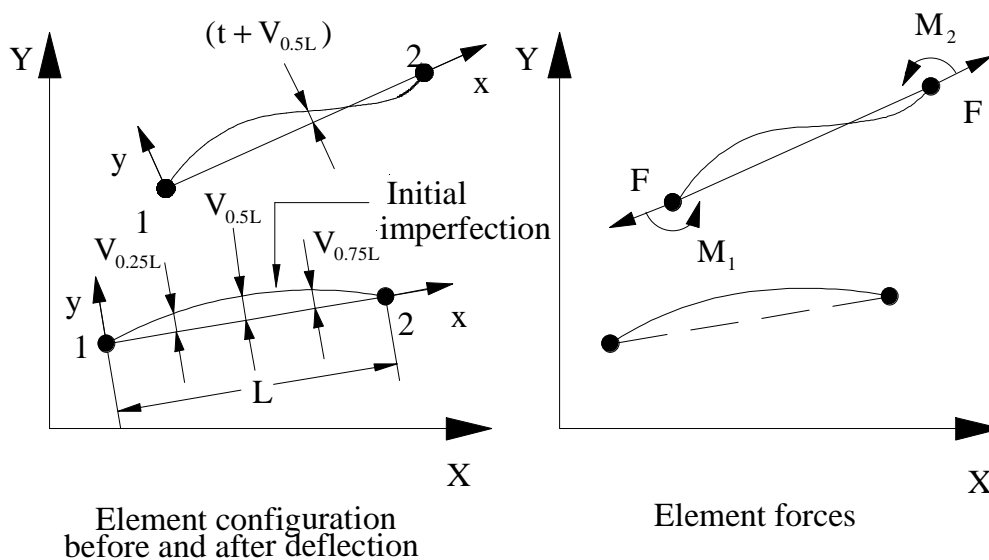
Configuration and forces in local system of element type *cbp2*

## qel2

---

|                        |   |
|------------------------|---|
| <b>Description</b>     | Quartic elastic 2D beam-column element.   |
| <b>Nodes</b>           | 2   |
| <b>Imperfections</b>   | $V_{0.25L}$ , $V_{0.5L}$ , $V_{0.75L}$ can be specified.  |
| <b>Characteristics</b> | Geometric nonlinearities. Large displacements and beam-column effect of perfect/imperfect members.<br><br>One element type <i>qel2</i> is usually sufficient to represent the beam-column effect and large displacement response of a whole elastic member. |
| <b>Application</b>     | Geometric nonlinearities in elastic plane frames.   |
| <b>Restrictions</b>    | Unable to model concrete cracking.  |
| <b>Group header</b>    | <b>sec.name</b> : An identifier referring to one of the <a href="#">cross-sections</a> declared in the <b>sections</b> module.  |

---



Configuration and forces in local system of element type *qel2*

## *qph2*

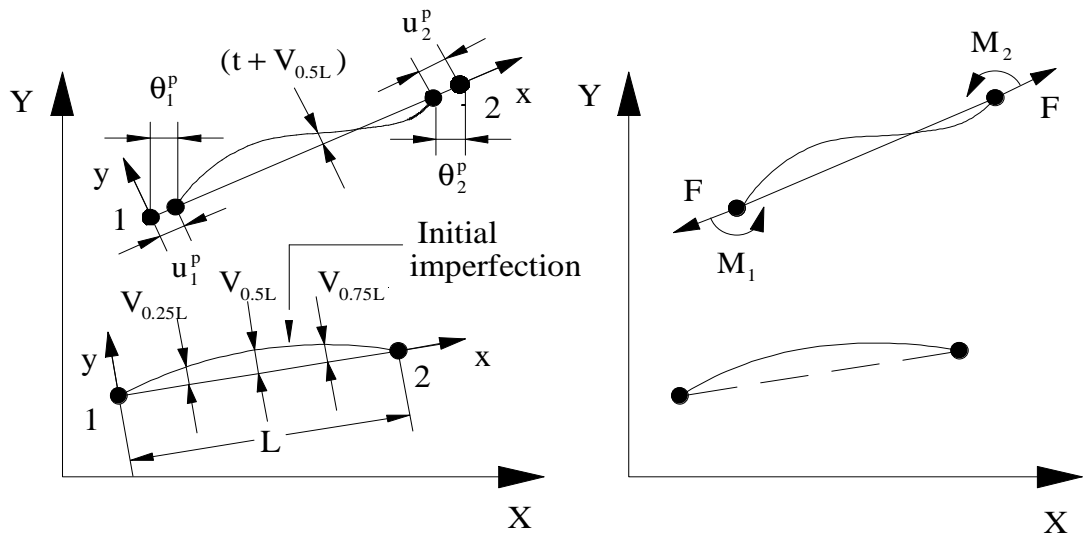
---

---

|                        |   |
|------------------------|---|
| <b>Description</b>     | Quartic plastic hinge 2D beam-column element with an option for automatic subdivision.  |
| <b>Nodes</b>           | 2   |
| <b>Subdivision</b>     | Automatic subdivision into two elements if a plastic hinge is detected within the element may be requested.   |
| <b>Imperfections</b>   | $V_{0.25L}$ , $V_{0.5L}$ , $V_{0.75L}$ can be specified.  |
| <b>Characteristics</b> | <p>Geometric and material nonlinearities.</p> <p>Suitable for members in which the spread of plasticity is not important and the section response is elastic-plastic without strain-hardening.</p> <p>Rotational and axial plastic hinge displacements are allowed at the two ends of the element.</p> <p>One element type <i>qph2</i> is usually sufficient to model a whole member, and the option of subdivision allows for the case of member buckling.</p> |
| <b>Application</b>     | Large displacement plastic-hinge analysis of plane frames   |
| <b>Restrictions</b>    | Not applicable to reinforced concrete or composite members.   |
| <b>Group header</b>    | <p><b>sec.name</b>: An identifier referring to one of the <a href="#">cross-sections</a> declared in the <b>sections</b> module.</p> <p><b>subdivision</b>: Gives the option for automatic subdivision plastic hinge elements:</p> <p>=( <b>t</b>   <b>true</b> )    consider element subdivision</p> <p>=( <b>f</b>   <b>false</b> )    ignore element subdivision</p>   |

---

---



Element configuration  
before and after deflection

Element forces

*Configuration and forces in local system of element type **qph2***

## *qdp2*

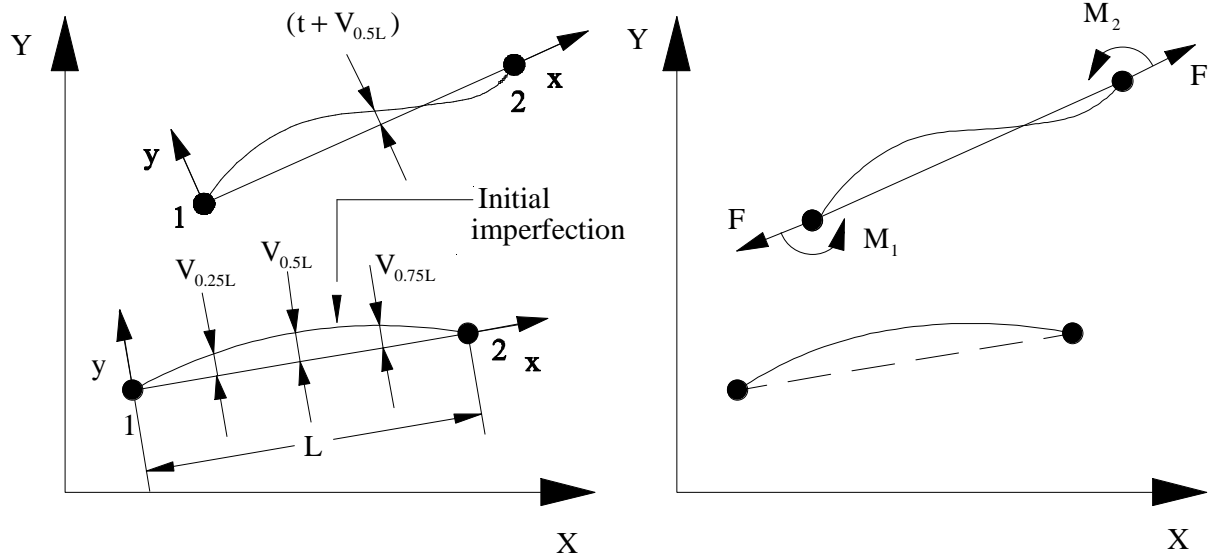
---

---

|                            |  |
|----------------------------|--|
| <b>Description</b>         | Quartic elastic 2D beam-column element utilising automatic q mesh refinement.  |
| <b>Subdivision pattern</b> | Relative lengths in ratio form of zones where inelasticity is checked for automatic mesh refinement.   |
| <b>Nodes</b>               | 2  |
| <b>Imperfections</b>       | $V_{0.25L}$ , $V_{0.5L}$ , $V_{0.75L}$ can be specified  |
| <b>Characteristics</b>     | <p>Geometric and material nonlinearities.</p> <p>Large displacement and beam-column effect of perfect/imperfect members.</p> <p>One element type <i>qdp2</i> is usually sufficient to represent a whole member.</p> <p>Element <i>qdp2</i> subdivides into elements <a href="#">cbp2</a>, specified under <b>cbp2.grp.name</b>, if inelasticity is detected in the zones defined by the subdivision <a href="#">pattern pat.name</a>.</p> <p>Accuracy increases with the number of sub-elements type <a href="#">cbp2</a> specified in the subdivision pattern.</p> <p>After subdivision, elements <a href="#">cbp2</a> are inserted in the inelastic zones, while the elastic zones are kept as element type <i>qdp2</i>.</p> |
| <b>Application</b>         | Adaptive modelling of inelastic members in plane frames.   |
| <b>Restrictions</b>        | Applies only to cross-sections with materials <a href="#">stl1</a> , <a href="#">stl2</a> & <a href="#">stl3</a> .   |
| <b>Group header</b>        | <p><b>cbp2.grp.name</b>: Specifies the group identifier of elements type <a href="#">cbp2</a> used in automatic mesh refinement.</p> <p><b>pat.name</b>: An identifier referring to a subdivision <a href="#">pattern</a> in the <b>patterns</b> module.</p>   |

---

---



Element configuration  
before and after deflection

Element forces

*Configuration and forces in local system of element type **qdp2***

## lnk2

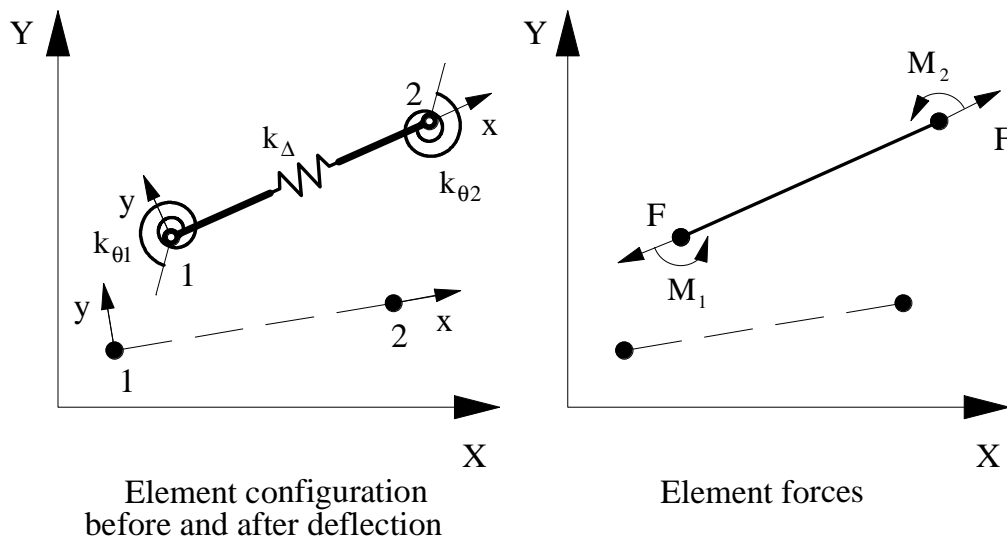
---

---

|                        |  |
|------------------------|--|
| <b>Description</b>     | 2D link element with discrete axial/rotational springs.  |
| <b>Nodes</b>           | 2  |
| <b>Characteristics</b> | Geometric nonlinearity.<br>3 independent spring stiffnesses, each taking either a constant numerical value or a <b>rigid</b> value.                                  |
| <b>Application</b>     | Rigid link.<br>Elastic bar with pinned ends.   |
| <b>Restrictions</b>    |  |
| <b>Group header</b>    | <b>stiffness.parameters</b> : numerical or <b>rigid</b> values for each of the spring stiffnesses, $k_{\theta 1}$ , $k_{\theta 2}$ and $k_{\Delta}$ , in this order. |

---

---



Configuration and forces in local system of element type *lnk2*

## spe2

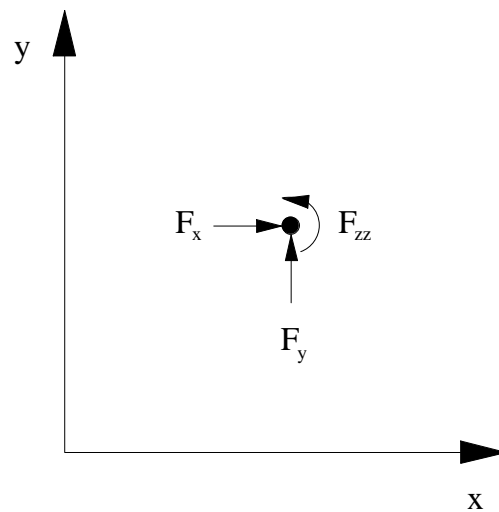
---

---

|                             |  |
|-----------------------------|--|
| <b>Description</b>          | Linear 2D nodal spring element.  |
| <b>Stiffness parameters</b> | Two global translational stiffnesses and one rotational stiffness can be specified in the following order:<br>$K_x, K_y, K_{zz}$                                     |
| <b>Nodes</b>                | 1  |
| <b>Characteristics</b>      | Models elastic boundaries for plane frame analysis.<br>Requires the definition of only one node, with the other node assumed fixed against translation and rotation. |
| <b>Application</b>          | Plane frame boundaries.  |
| <b>Restrictions</b>         | Cannot be used to join two elements. For that purpose use <a href="#">jel2</a> .   |
| <b>Group header</b>         | <code>stiffness.parameters</code> : Defines stiffness parameters.  |

---

---



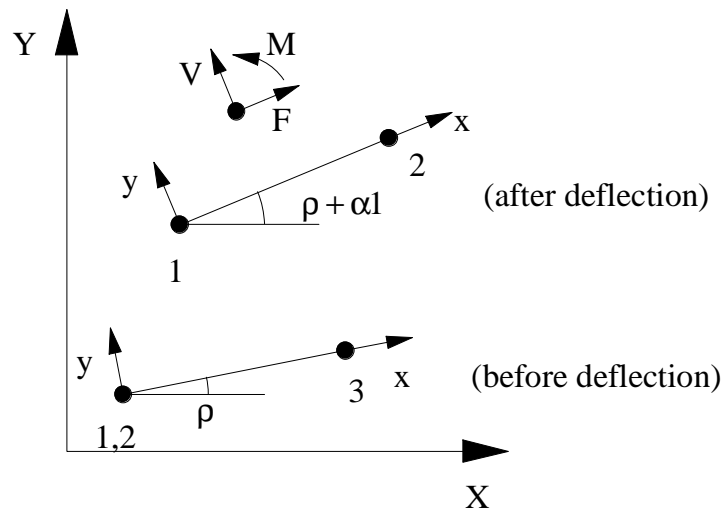
*Forces for element type spe2*



|                        |   |
|------------------------|---|
| <b>Description</b>     | 2D joint element with uncoupled axial, shear and moment actions.  |
| <b>Curve types</b>     | Models used for the joint force-displacement curves, specified for F (axial), V (shear) and M (moment), respectively.<br>Each of these models may be any of those described in <a href="#">Chapter 4</a> .  |
| <b>Parameters</b>      | Parameters for each of the three models specified for F, V and M.   |
| <b>Nodes</b>           | 3   |
| <b>Characteristics</b> | Nodes (1) and (2) must be initially coincident.<br>Node (3) is only used to define the x-axis of the joint and can be a non-structural node.<br>The orientation of the joint x-axis after deformation is determined by its initial orientation and the global rotation of node (1). |
| <b>Application</b>     | Plane frame analysis.<br>Can be used to model pin joints, inclined supports, elasto-plastic joint behaviour, soil-structure interaction and structural gaps, through employing appropriate joint curves.  |
| <b>Restrictions</b>    | Element has a zero initial length, since nodes (1) and (2) must be coincident.<br>Cannot be used to model coupled axial, shear and moment actions.  |
| <b>Group header</b>    | <code>curve.types</code> : Defines curve types for joint elements.<br><code>parameters</code> : Defines parameters for the joint elements.  |

---

---

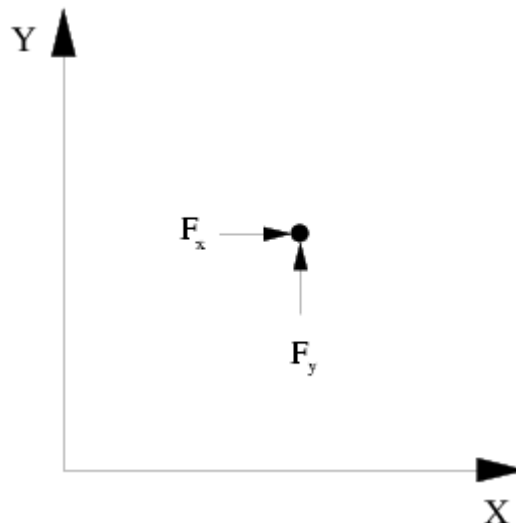


*Forces for element type **j12***

|                        |   |
|------------------------|---|
| <b>Description</b>     | Concentrated ( lumped ) 2D mass element.  |
| <b>Nodes</b>           | 1   |
| <b>Characteristics</b> | Models lumped mass for dynamic analysis.<br>Allows full 2x2 translational mass matrix to be defined.<br>Lumped element mass, specified according to one of:<br>$M_x$ (default $M_y = M_x$ & $M_{xy} = 0$ )<br>$M_x, M_y$ (default $M_{xy} = 0$ )<br>$M_x, M_y, M_{xy}$<br>Allows specification of mass-proportional damping at group level. |
| <b>Application</b>     | Dynamic analysis of plane frames.   |
| <b>Restrictions</b>    |   |
| <b>Group header</b>    | <b>mass</b> : Element mass.<br><b>[damping.parameter]</b> : optional parameter for mass-proportional Rayleigh damping; defaults to the value of <b>mass.damping.parameter</b> specified in the <a href="#">default.parameters</a> module.   |

---

---



*Forces for element type **cnm2***

## *cnd2*

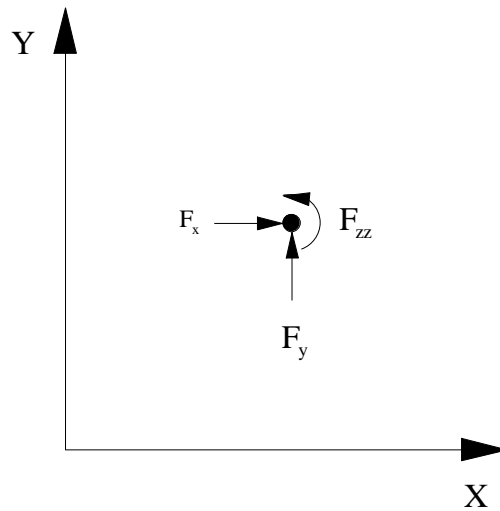
---

---

|                           |   |
|---------------------------|---|
| <b>Description</b>        | Concentrated (dashpot) 2D viscous damping element.  |
| <b>Damping parameters</b> | Two translational and one rotational damping coefficients, specified in this order:<br>$C_x$ , $C_y$ , $C_{zz}$ |
| <b>Nodes</b>              | 1   |
| <b>Characteristics</b>    | Models nodal viscous damping for dynamic analysis.  |
| <b>Application</b>        | Dynamic analysis of plane frames.   |
| <b>Restrictions</b>       |   |
| <b>Group header</b>       | <code>damping.parameters:</code> Defines dashpot damping parameters.  |

---

---



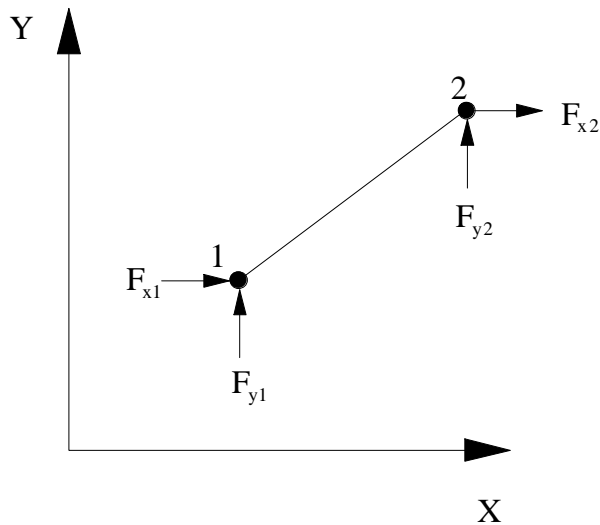
*Forces for element type **cnd2***

## *lnm2*

---

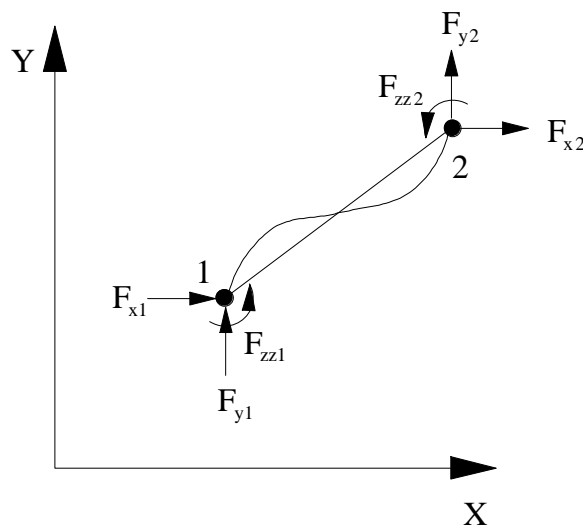
|                        |   |
|------------------------|---|
| <b>Description</b>     | Linear 2D mass element.   |
| <b>Nodes</b>           | 2   |
| <b>Characteristics</b> | Simplified modelling of uniformly distributed mass for dynamic analysis. Assumes the mass to lie on a rigid straight line between the two end nodes.<br><br>Allows specification of mass-proportional damping at group level.                                 |
| <b>Application</b>     | Dynamic analysis of plane frames.   |
| <b>Restrictions</b>    |   |
| <b>Group header</b>    | <b>mass</b> /length: Mass per unit length.<br><br>[ <b>damping.parameter</b> ]: optional parameter for mass-proportional Rayleigh damping; defaults to the value of <b>mass.damping.parameter</b> specified in the <a href="#">default.parameters</a> module. |

---



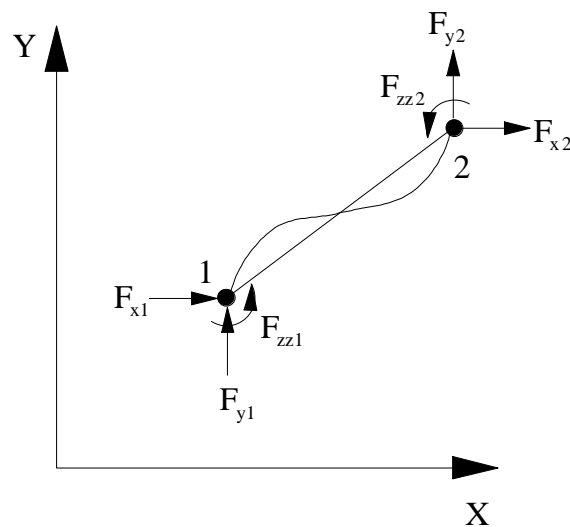
*Forces for element type lnm2*

|                        |   |
|------------------------|---|
| <b>Description</b>     | Cubic 2D distributed mass element   |
| <b>Nodes</b>           | 2   |
| <b>Characteristics</b> | <p>Models uniformly distributed mass in dynamic analysis.</p> <p>Uses an Updated Lagrangian formulation with a cubic shape function for the transverse displacement and a linear distribution for the axial displacement.</p> <p>Allows different axial (<math>m_a</math>) and transverse (<math>m_t</math>) distributed mass.</p> <p>Mass per unit length, specified according to one of:</p> <p style="margin-left: 40px;"><math>m_a</math> (default <math>m_t = m_a</math>)</p> <p style="margin-left: 40px;"><math>m_a, m_t</math></p> <p>Allows specification of mass-proportional damping at group level.</p> |
| <b>Application</b>     | Dynamic analysis of plane frames.   |
| <b>Restrictions</b>    |   |
| <b>Group header</b>    | <p><b>mass</b>/length: Mass per unit length.</p> <p>[<b>damping.parameter</b>]: optional parameter for mass-proportional Rayleigh damping; defaults to the value of <b>mass.damping.parameter</b> specified in the <a href="#">default.parameters</a> module.</p>   |



Forces for element type **cbm2**

|                        |   |
|------------------------|---|
| <b>Description</b>     | Rayleigh damping 2D element   |
| <b>Mass/length</b>     | Mass per unit length  |
| <b>Parameters</b>      | Two proportionality constants ( $a_1$ & $a_2$ ) of mass and stiffness respectively, specified in that order.  |
| <b>Nodes</b>           | 2   |
| <b>Characteristics</b> | Models Rayleigh damping effects.<br>All <b>rld2</b> elements must have the same constant ( $a_1$ & $a_2$ ) to model conventional Rayleigh damping.  |
| <b>Application</b>     | Dynamic analysis of plane frames.   |
| <b>Restrictions</b>    | ( $a_1$ ) should be set to zero for dynamic analysis involving ground excitation, otherwise damping would be proportional to absolute rather than relative frame velocity.  |
| <b>Group header</b>    | <b>sec.name</b> :An identifier referring to one of the <a href="#">cross-sections</a> declared in the <b>sections</b> module.<br><b>mass/length</b> : Mass per unit length.<br><b>parameters</b> : Defines parameters of Rayleigh damping elements. |



*Forces for element type rld2*

|                      |   |
|----------------------|---|
| <b>Description</b>   | 2D/3D joint element with coupling between axial force and moment but uncouple with shear.   |
| <b>Types</b>         | Three entries are required:<br><ol style="list-style-type: none"><li>1) 'steel' for bare steel or 'composite' for composite connection.</li><li>2) connection type:<br/>'flush.endplate'<br/>'extended.endplate'<br/>'web.angles'<br/>'top.and.seat'<br/>'combined.web/top/seat'<br/>'finplate'</li><li>3) behaviour of panel zone, either 'rigid' if panel zone behaviour is omitted or 'flexible' if the flexibility of the panel zone is included.</li></ol>   |
| <b>Material name</b> | Three material properties are required by using material model <a href="#">gen1</a> . The first material provides the properties of the connecting elements e.g. plates, angle. The second material is the properties of bolts. The third material is the properties of the connected member i.e. column and beam.  |
| <b>Parameters</b>    | Number of parameters vary according to connection type: <ul style="list-style-type: none"><li>• Flush endplate (13 parameters)</li><li>• Extended endplate (26 parameters)</li><li>• Double web angles (12 parameters)</li><li>• Top and seat angles (23 parameters)</li><li>• Combination of top, seat and web angles (34 parameters)</li><li>• Finplate (8 parameters)</li></ul> <ol style="list-style-type: none"><li>1. Flush end plate<ul style="list-style-type: none"><li>• Bolt diameter,</li><li>• Area of bolt shank,</li><li>• Thickness of bolt head,</li><li>• Thickness of nut,</li><li>• Thickness of washer,</li><li>• Distance from endplate edge to bolt head/nut/washer edge,</li><li>• Distance of bolt head/nut /washer whichever is appropriate,</li><li>• Distance from edge of bolt head/nut/ washer to fillet of endplate to beam web,</li><li>• Total depth of endplate,</li><li>• Thickness of endplate,</li><li>• Endplate width,</li></ul></li></ol> |

---

---



- 
- 
- Minimum bolt pitch,
  - Coefficient for the computation of the effective width for the bolt-row below the beam tension flange.

## 2. Extended end plate

The geometrical properties of the extended endplate are double the properties of the flush endplate, accounting for different orientation of the T-stub components, but the details and order are the same. The only exception is for the last parameter, where the length of the extended part of the endplate is required.

## 3. Double web angles

- Bolt diameter,
- Area of bolt shank,
- Total depth of angle,
- Angle thickness,
- Gauge length of beam leg,
- Bolt clearance,
- Minimum bolt pitch,
- Gauge length of column leg,
- Distance from bolt line to free edge of column leg,
- Distance from bolt line to free edge of beam leg,
- Angle radius,
- Diameter of M16 bolts.

## 4. Top and seat angles

For top angle (12 parameters):

- Bolt diameter,
- Area of bolt shank,
- Total depth of angle,
- Angle thickness,
- Gauge length of beam leg,
- Bolt clearance,
- Minimum bolt pitch,
- Gauge length of column leg,
- Distance from bolt line to free edge of column leg,
- Distance from bolt line to free edge of beam leg,
- Angle radius,
- Diameter of M16 bolts.

Similar dimensions are needed for seat angle (11 parameters) except for the diameter of M16 bolts.

## 5. Combination of top, seat and web angles

Connection parameters for this type are the combination of web angle and top and seat angles.

---

---

---

---

## 6. Finplate

- Bolt diameter,
- Bolt hole diameter,
- Total depth of plate,
- Plate thickness,
- Gauge length,
- Width of plate,
- Minimum bolt pitch,
- Diameter of M16 bolts.

After the connection parameters are entered, another 14 parameters are needed: 11 parameters for the connected members, followed by Poisson ratio, number of layers and a flag to indicate preload or non-preload condition of the bolts.

Connected member parameters are:

- Column depth,
- Column flange width,
- Thickness of column flange,
- Thickness of column web,
- Column radius,
- Bolt pitch in column,
- Distance from bolt line to free edge of column flange,
- Distance from bolt line to fillet of column flange,
- Beam depth,
- Thickness of beam flange,
- Thickness of beam web.

### *Nodes*

3 (2D) used similar to [jel2](#)

4 (3D) used similar to [jel3](#)

### *Application*

Plane frame analysis.

Space frame analysis.

Can be used to model steel and composite joints.

### *Restrictions*

Element has a zero initial length, since nodes (1) and (2) must be coincident.

### *Group header*

**type:** Defines the type of connection and contribution of shear panel

**mat.name(s):** Defines the material for the connecting elements, bolts and connected member

**parameters:** Defines parameters for the joint and depends on the connection types.

---

---

## cbp3

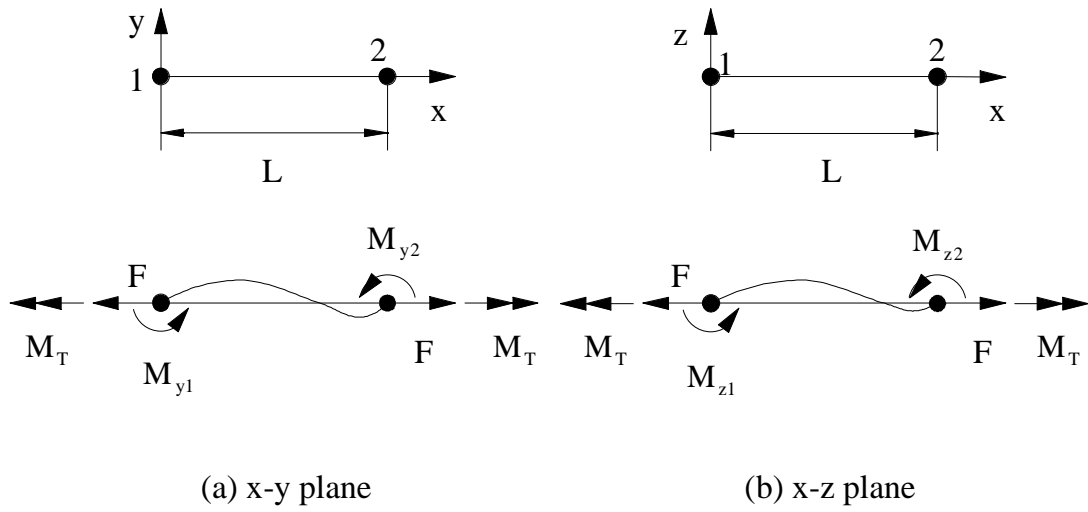
---

---

|                          |  |
|--------------------------|--|
| <b>Description</b>       | Cubic elasto-plastic 3D beam-column element.   |
| <b>Monitoring points</b> | 100 points usually adequate; depends on section type.  |
| <b>Nodes</b>             | 3  |
| <b>Characteristics</b>   | <p>Geometric and material nonlinearities.</p> <p>Numerical integration performed over two Gauss points.</p> <p>A number of monitoring areas used at each Gauss section to monitor material direct stress and strains.</p> <p>Predicts global member behaviour based on a material stress-strain relationship.</p> <p>A number of elements per member, usually over 5, must be used for reasonable accuracy in inelastic modelling.</p> <p>Nodes (1) and (2) define the element connectivity and its local x-axis. The y-axis lies in a plane defined by the x-axis and node (3), which can be a non-structural node.</p> |
| <b>Application</b>       | Modelling of inelastic members in space frames.  |
| <b>Restrictions</b>      | The elastic torsional rigidity is used, which is approximate for composite and R/C sections. Warping strains are not accounted for.  |
| <b>Group header</b>      | <p><b>sec.name</b> :An identifier referring to one of the <a href="#">cross-sections</a> declared in the <b>sections</b> module.</p> <p><b>monitoring.points</b> Defines the number of points for monitoring stresses and strains within a <a href="#">cross-section</a>.</p>  |

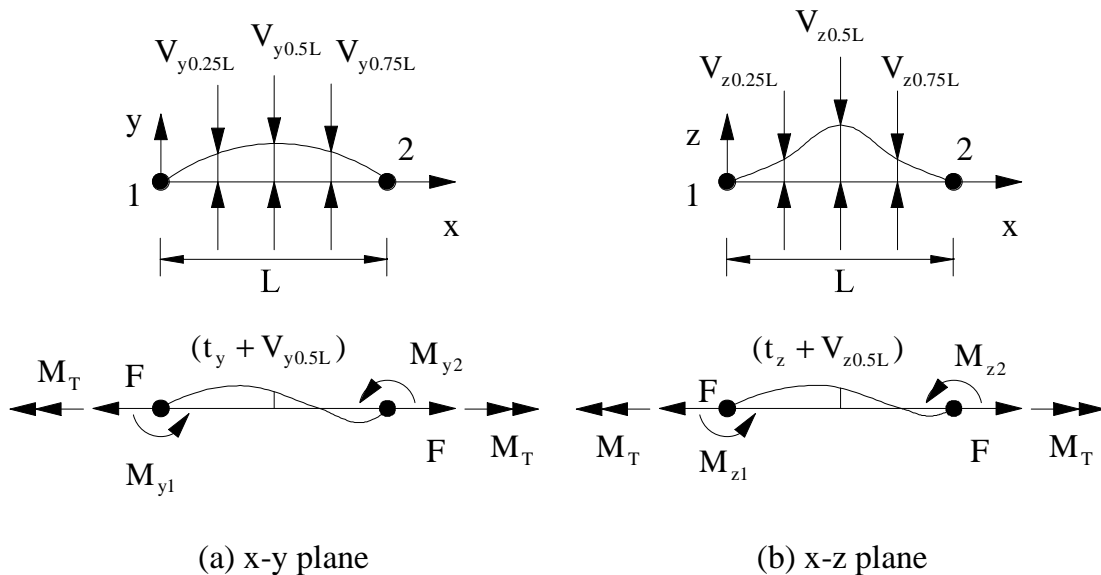
---

---



*Forces in local system of element type **cbp3***

|                        |  |
|------------------------|--|
| <b>Description</b>     | Quartic elastic 3D beam-column element.  |
| <b>Nodes</b>           | 3  |
| <b>Imperfections</b>   | $V_{y0.25L}$ , $V_{y0.5L}$ , $V_{y0.75L}$ , $V_{z0.25L}$ , $V_{z0.5L}$ , and $V_{z0.75L}$ can be specified.  |
| <b>Characteristics</b> | Geometric nonlinearities.<br>Large displacements and beam-column effect of perfect/imperfect members.<br>One element type <i>qel3</i> is usually sufficient to represent the beam-column effect and large displacement response of a whole elastic member.<br>Nodes (1) and (2) define the element connectivity and its local x-axis. The y-axis lies in a plane defined by the x-axis and node (3), which can be a non-structural node. |
| <b>Application</b>     | Geometric nonlinearities in elastic space frames.  |
| <b>Restrictions</b>    | Unable to model concrete cracking.<br>Warping strains are not accounted for.   |
| <b>Group header</b>    | <b>sec.name</b> :An identifier referring to one of the <a href="#">cross-sections</a> declared in the <b>sections</b> module.  |



*Imperfection and forces in local system of element type qel3*

## *qph3*

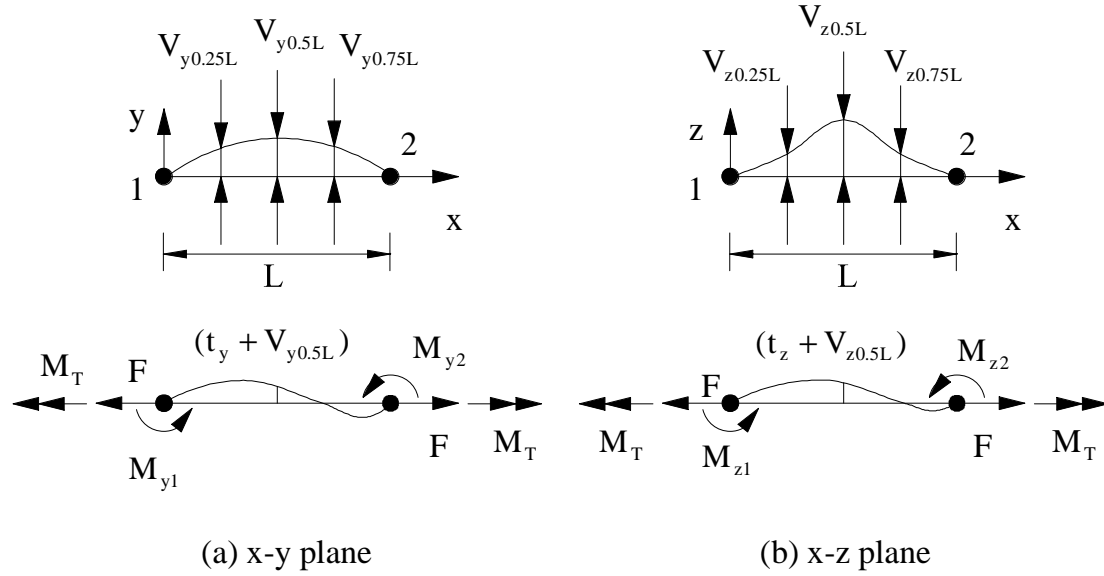
---

---

|                        |   |
|------------------------|---|
| <b>Description</b>     | Quartic plastic hinge 3D beam-column element with an option for automatic subdivision.  |
| <b>Nodes</b>           | 3   |
| <b>Subdivision</b>     | Automatic subdivision into two elements if a plastic hinge is detected within the element may be requested.   |
| <b>Imperfections</b>   | $V_{y0.25L}$ , $V_{y0.5L}$ , $V_{y0.75L}$ , $V_{z0.25L}$ , $V_{z0.5L}$ , and $V_{z0.75L}$ can be specified.   |
| <b>Characteristics</b> | <p>Geometric and material nonlinearities.</p> <p>Suitable for members in which the spread of plasticity is not important and the section response is elastic-plastic without strain-hardening.</p> <p>Rotational and axial plastic hinge displacements are allowed at the two ends of the element.</p> <p>One element type <i>qph3</i> is usually sufficient to model a whole member, and the option of subdivision allows for the case of member buckling.</p> <p>Nodes (1) and (2) define the element connectivity and its local x-axis. The y-axis lies in a plane defined by the x-axis and node (3), which can be a non-structural node.</p> |
| <b>Application</b>     | Large displacement plastic-hinge analysis of space frames   |
| <b>Restrictions</b>    | Not applicable to reinforced concrete or composite members.<br>Warping strains are not accounted for.   |
| <b>Group header</b>    | <p><b>sec.name</b>: An identifier referring to one of the <a href="#">cross-sections</a> declared in the <b>sections</b> module.</p> <p><b>subdivision</b>: Gives the option for automatic subdivision plastic hinge elements:</p> <p>=( <b>t</b>   <b>true</b> )    consider element subdivision</p> <p>=( <b>f</b>   <b>false</b> )    ignore element subdivision</p>   |

---

---



*Imperfection and forces in local system of element type **qph3***

## qdp3

---

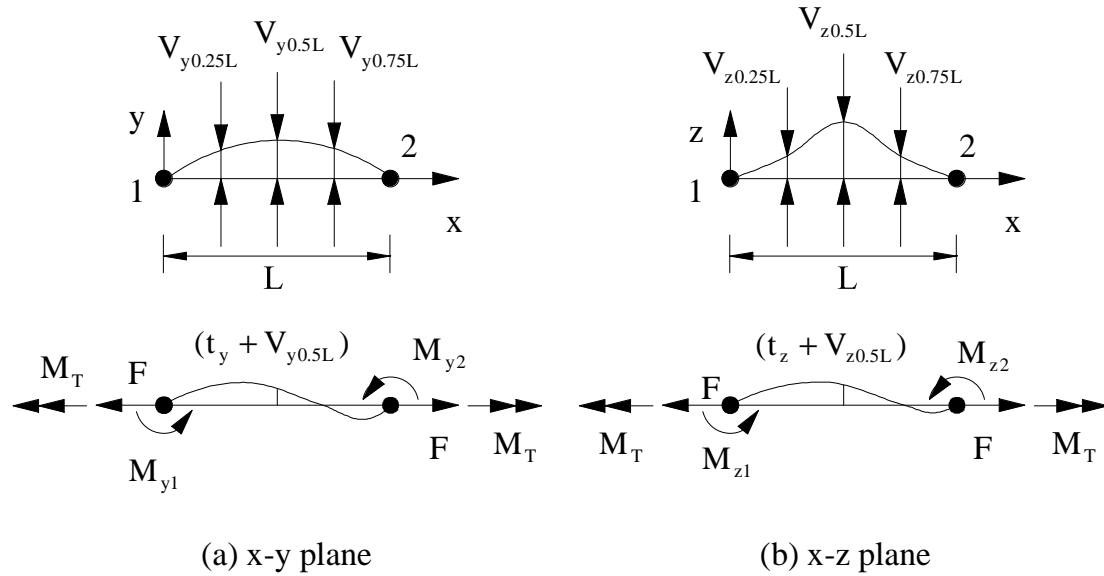
---

|                            |  |
|----------------------------|--|
| <b>Description</b>         | Quartic elastic 3D beam-column element utilising automatic mesh refinement.  |
| <b>Subdivision pattern</b> | Relative lengths in ratio form of zones where inelasticity is checked for automatic mesh refinement.   |
| <b>Nodes</b>               | 3  |
| <b>Imperfections</b>       | $V_{y0.25L}$ , $V_{y0.5L}$ , $V_{y0.75L}$ , $V_{z0.25L}$ , $V_{z0.5L}$ , and $V_{z0.75L}$ can be specified.  |
| <b>Characteristics</b>     | <p>Geometric and material nonlinearities.</p> <p>Large displacement and beam-column effect of perfect/imperfect members.</p> <p>One element type <b>qdp3</b> is usually sufficient to represent a whole member.</p> <p>Element <b>qdp3</b> subdivides into elements <b>cbp3</b>, specified under <b>cbp3.grp.name</b>, if inelasticity is detected in the zones defined by the subdivision pattern <b>pat.name</b>.</p> <p>Accuracy increases with the number of sub-elements type <b>cbp3</b> specified in the subdivision pattern.</p> <p>After subdivision, elements <b>cbp3</b> are inserted in the inelastic zones, while the elastic zones are kept as element type <b>qdp3</b>.</p> <p>Nodes (1) and (2) define the element connectivity and its local x-axis. The y-axis lies in a plane defined by the x-axis and node (3), which can be a non-structural node.</p> |
| <b>Application</b>         | Adaptive modelling of inelastic members in space frames.   |
| <b>Restrictions</b>        | Applies only to cross-sections with materials <b>stl1</b> , <b>stl2</b> & <b>stl3</b> .<br>Warping strains are not   |
| <b>Group header</b>        | <b>cbp3.grp.name</b> : Specifies the group identifier of elements type <b>cbp3</b> used in automatic mesh refinement.<br><b>pat.name</b> : An identifier referring to a subdivision <b>pattern</b> in the <b>patterns</b> module.  |

---

---





*Imperfection and forces in local system of element type qdp3*

## lnk3

---



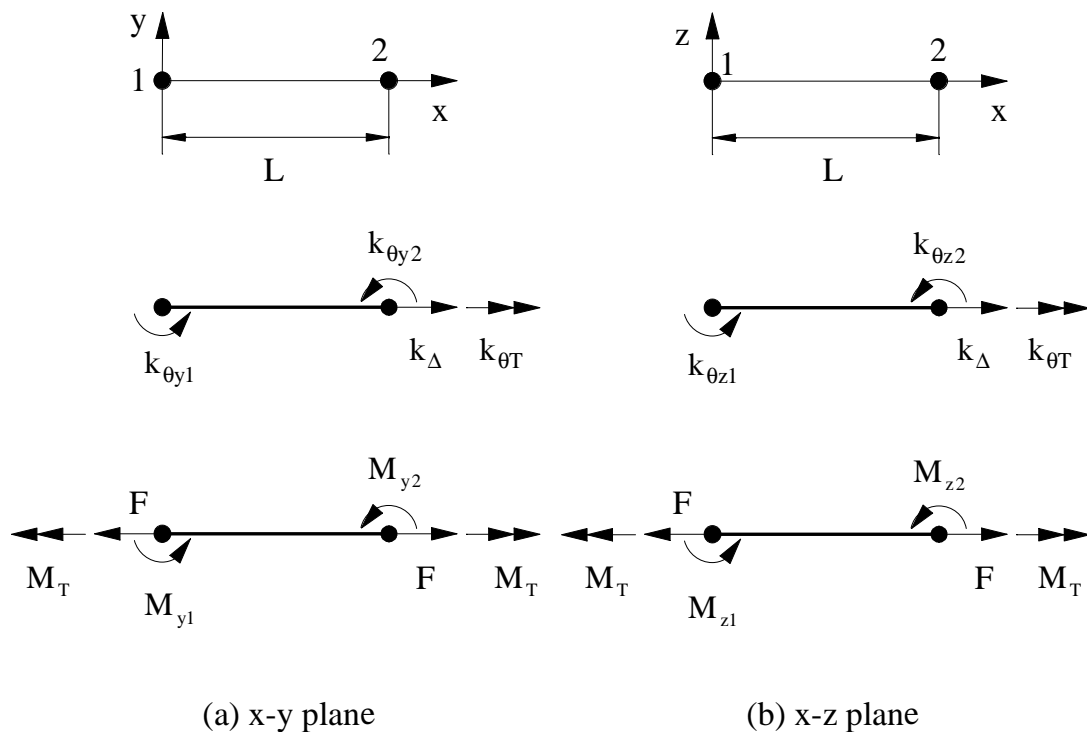
---

|                        |  |
|------------------------|--|
| <b>Description</b>     | 3D link element with discrete axial/rotational springs.  |
| <b>Nodes</b>           | 3  |
| <b>Characteristics</b> | Geometric nonlinearity.<br>Nodes (1) and (2) define the element connectivity and its local x-axis. The y-axis lies in a plane defined by the x-axis and node (3), which can be a non-structural node.                    |
| <b>Application</b>     | Rigid link.<br>Elastic bar with pinned ends.   |
| <b>Restrictions</b>    |  |
| <b>Group header</b>    | <b>stiffness.parameters:</b> numerical or <b>rigid</b> values for each of the spring stiffnesses, $k_{\theta y1}$ , $k_{\theta z1}$ , $k_{\theta y2}$ , $k_{\theta z2}$ , $k_{\Delta}$ and $k_{\theta T}$ in this order. |

---



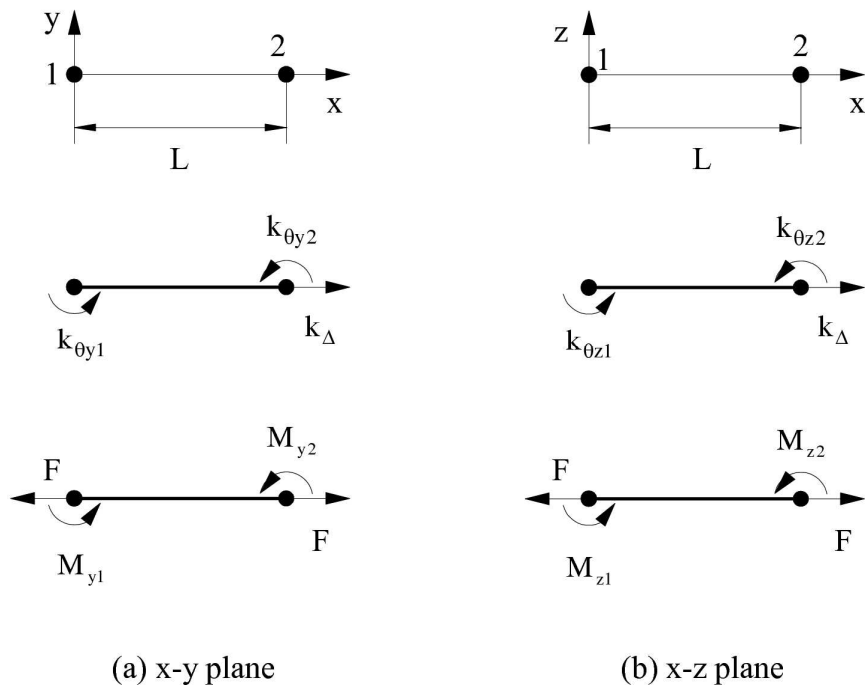
---



*Stiffness parameters and forces in local system of element type lnk3*

## Inks

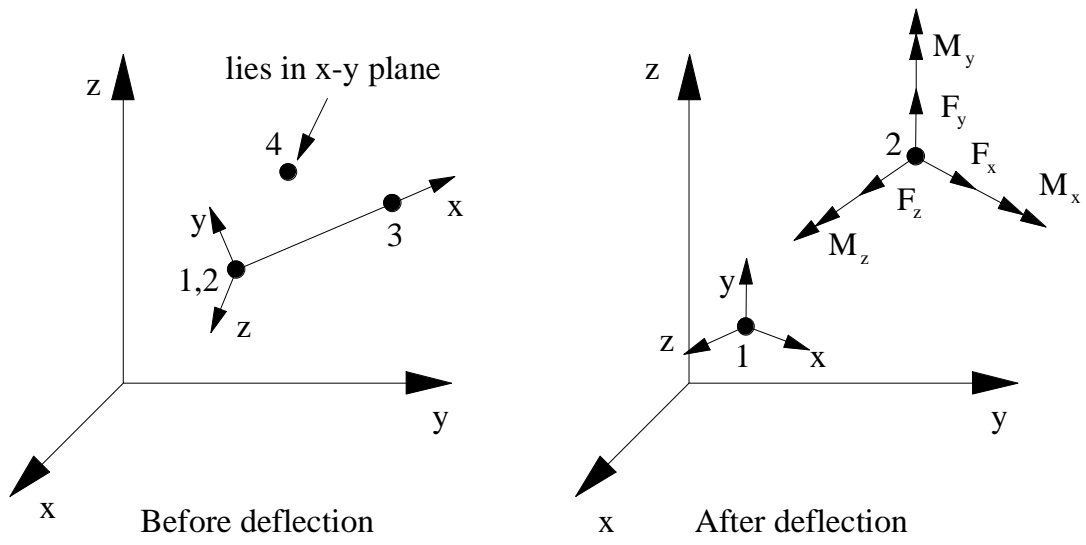
|                        |   |
|------------------------|---|
| <b>Description</b>     | 3D link element linking 6 DOF to 5 DOF nodes.   |
| <b>Nodes</b>           | 3.  |
| <b>Characteristics</b> | Geometric nonlinearity.<br><br>Nodes (1) and (2) define the element connectivity and its local x-axis. The y-axis lies in a plane defined by the x-axis and node (3), which can be a non-structural node. |
| <b>Application</b>     | Beam to slab connection.<br><br>The second node is a 5 DOF node belonging to plate/shell elements with only two rotational DOF's, including <a href="#">csl4</a> elements.                                |
| <b>Restrictions</b>    |   |
| <b>Group header</b>    | <b>stiffness.parameters:</b> numerical or <b>rigid</b> values for each of the spring stiffnesses, $k_{\theta y1}$ , $k_{\theta z1}$ , $k_{\theta y2}$ , $k_{\theta z2}$ and $k_{\Delta}$ in this order.   |



*Stiffness parameters and forces in local system of element type **Inks***

|                        |   |
|------------------------|---|
| <b>Description</b>     | 3D joint element with uncoupled axial, shear and moment actions.  |
| <b>Curve types</b>     | Models used for the joint force-displacement curves, specified for $F_x$ (axial), $F_y$ & $F_z$ (shear) and $M_x$ , $M_y$ & $M_z$ (moment), respectively.<br>Each of these models may be any of those described in <a href="#">Chapter 4</a> .  |
| <b>Parameters</b>      | Parameters for each of the six models specified for $F_x$ , $F_y$ , $F_z$ , $M_x$ , $M_y$ , $M_z$ .   |
| <b>Nodes</b>           | 4   |
| <b>Characteristics</b> | Nodes (1) and (2) must be initially coincident. Node (3) is only used to define the x-axis of the joint and can be a non-structural node. The y-axis lies in a plane defined by the x-axis and node (4), which also can be a non-structural node.<br>The orientation of the joint x-axis after deformation is determined by its initial orientation and the global rotations of node (1). |
| <b>Application</b>     | Space frame analysis.<br>Can be used to model pin joints, inclined supports, elasto-plastic joint behaviour, soil-structure interaction and structural gaps, through employing appropriate joint curves.  |
| <b>Restrictions</b>    | Element has a zero initial length, since nodes (1) and (2) must be coincident.<br>Cannot be used to model coupled axial, shear and moment actions.  |
| <b>Group header</b>    | <code>curve.types</code> : Defines curve types for joint elements.<br><code>parameters</code> : Defines parameters for the joint elements.  |

---

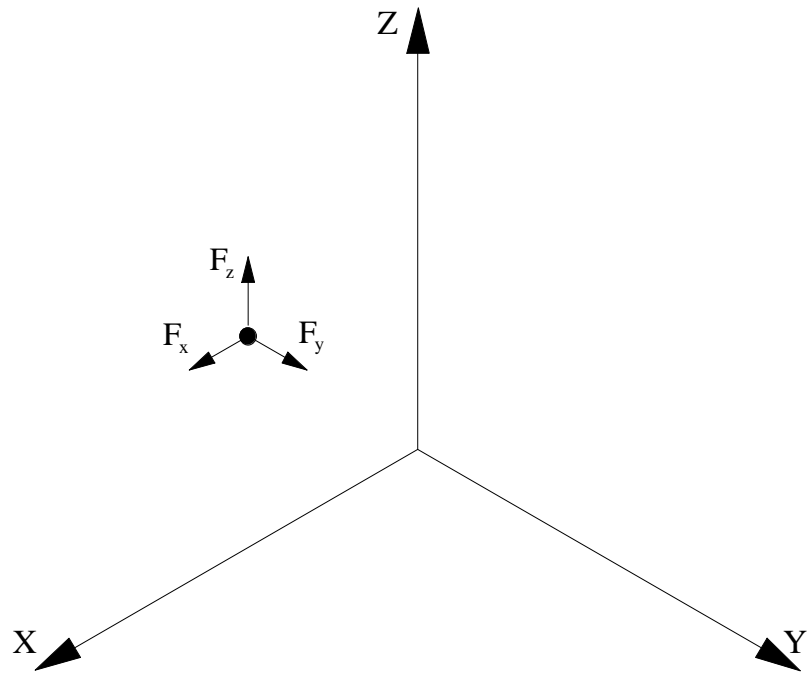


*Configuration and forces for element type j13*

|                        |   |
|------------------------|---|
| <b>Description</b>     | Concentrated ( lumped ) 3D mass element.  |
| <b>Nodes</b>           | 1   |
| <b>Characteristics</b> | Models lumped mass for dynamic analysis.<br>Allows full 3×3 translational mass matrix to be defined.<br>Lumped element mass, specified according to one of:<br>$M_x$ (default $M_y = M_z = M_x$ & $M_{xy} = M_{xz} = M_{yz} = 0$ )<br>$M_x, M_y, M_z$ (default $M_{xy} = M_{xz} = M_{yz} = 0$ )<br>$M_x, M_y, M_z, M_{xy}, M_{xz}, M_{yz}$<br>Allows specification of mass-proportional damping at group level. |
| <b>Application</b>     | Dynamic analysis of space frames, shells and 3D continuum/membrane structures.  |
| <b>Restrictions</b>    |   |
| <b>Group header</b>    | <b>mass:</b> Element mass.<br><b>[damping.parameter]:</b> optional parameter for mass-proportional Rayleigh damping; defaults to the value of <b>mass.damping.parameter</b> specified in the <a href="#">default.parameters</a> module.   |

---

---



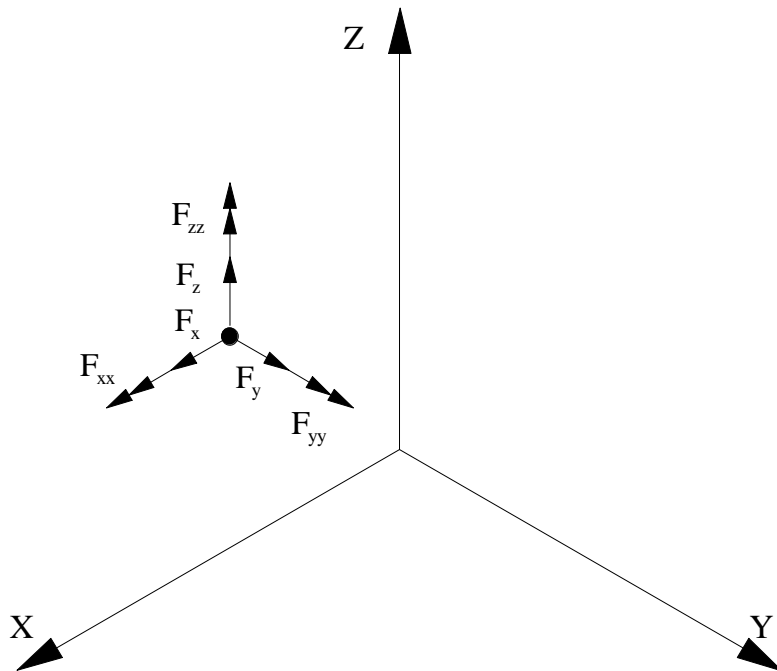
*Forces for element type **cnm3***

## *cnd3*

---

|                           |   |
|---------------------------|---|
| <b>Description</b>        | Concentrated (dashpot) 3D viscous damping element.  |
| <b>Damping parameters</b> | Three translational and three rotational damping coefficients, specified in this order:<br>$C_x, C_y, C_z$<br>$[C_{xx}, C_{yy}, C_{zz}]$                        |
| <b>Nodes</b>              | 1   |
| <b>Characteristics</b>    | Models nodal viscous damping for dynamic analysis.  |
| <b>Application</b>        | Dynamic analysis of space frames and shells.<br>Dynamic analysis of 3D continuum/membrane structures.   |
| <b>Restrictions</b>       | $C_{xx}, C_{yy}, C_{zz}$ should be specified as zero for shell nodes.<br>$[C_{xx}, C_{yy}, C_{zz}]$ should not be specified for 3D continuum/membrane analysis. |
| <b>Group header</b>       | <code>damping.parameters:</code> Defines dashpot damping parameters.  |

---



*Forces for element type cnd3*

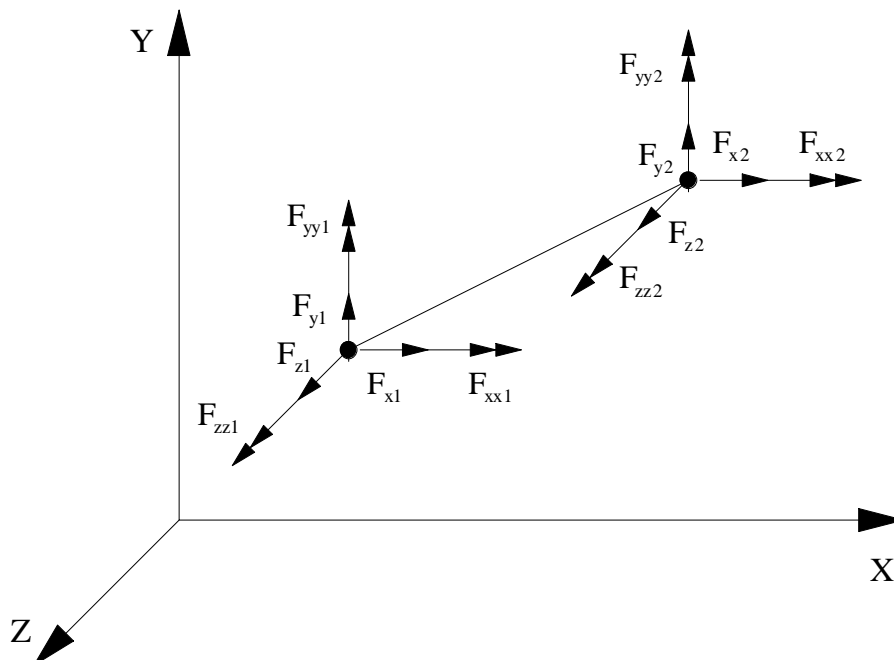


## *lnm3*

---

|                        |   |
|------------------------|---|
| <b>Description</b>     | Linear 3D mass element.   |
| <b>Nodes</b>           | 2   |
| <b>Characteristics</b> | <p>Simplified modelling of uniformly distributed mass for dynamic analysis.</p> <p>Assumes the mass to lie on a rigid straight line between the two end nodes.</p> <p>Allows specification of mass-proportional damping at group level.</p>   |
| <b>Application</b>     | Dynamic analysis of space frames.   |
| <b>Restrictions</b>    |   |
| <b>Group header</b>    | <p><code>mass</code>/length: Mass per unit length.</p> <p>[<code>damping.parameter</code>]: optional parameter for mass-proportional Rayleigh damping; defaults to the value of <code>mass.damping.parameter</code> specified in the <a href="#">default.parameters</a> module.</p> |

---



*Forces for element type lnm3*

## *cbm3*

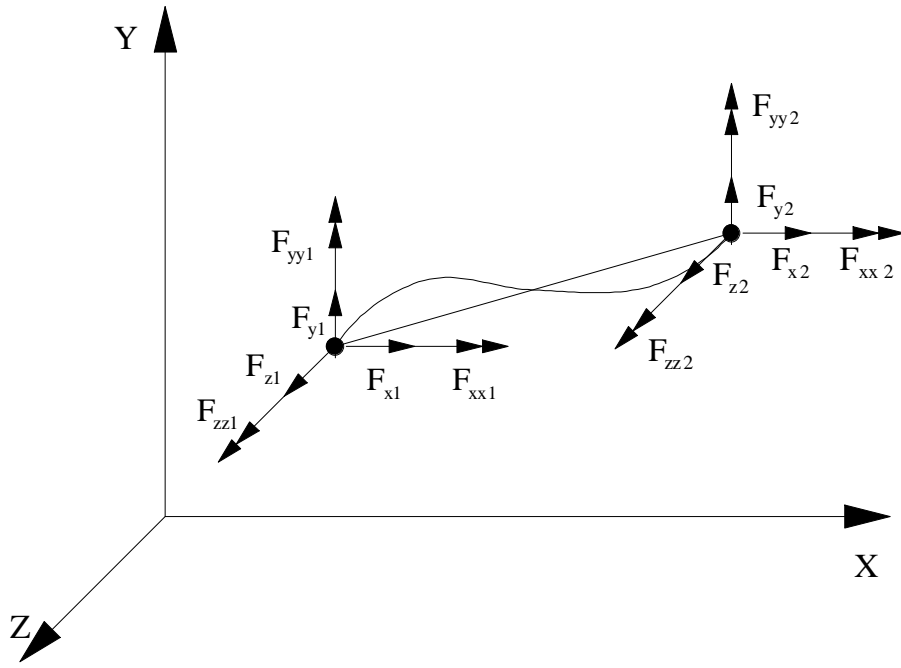
---

---

|                        |   |
|------------------------|---|
| <b>Description</b>     | Cubic 3D distributed mass element.  |
| <b>Nodes</b>           | 2   |
| <b>Characteristics</b> | <p>Models uniformly distributed mass in dynamic analysis.</p> <p>Uses an Updated Lagrangian formulation with a cubic shape function for the transverse displacement and a linear distribution for the axial displacement.</p> <p>Allows different axial (<math>m_a</math>) and transverse (<math>m_t</math>) distributed mass.</p> <p>Mass per unit length, specified according to one of:</p> <ul style="list-style-type: none"><li><math>m_a</math> (default <math>m_t = m_a</math>)</li><li><math>m_a, m_t</math></li></ul> <p>Allows specification of mass-proportional damping at group level.</p> |
| <b>Application</b>     | Dynamic analysis of space frames.   |
| <b>Restrictions</b>    |   |
| <b>Group header</b>    | <p><code>mass/length</code>: Mass per unit length.</p> <p><code>[damping.parameter]</code>: optional parameter for mass-proportional Rayleigh damping; defaults to the value of <code>mass.damping.parameter</code> specified in the <a href="#">default.parameters</a> module.</p>   |

---

---



*Forces for element type **cbm3***

## *rld3*

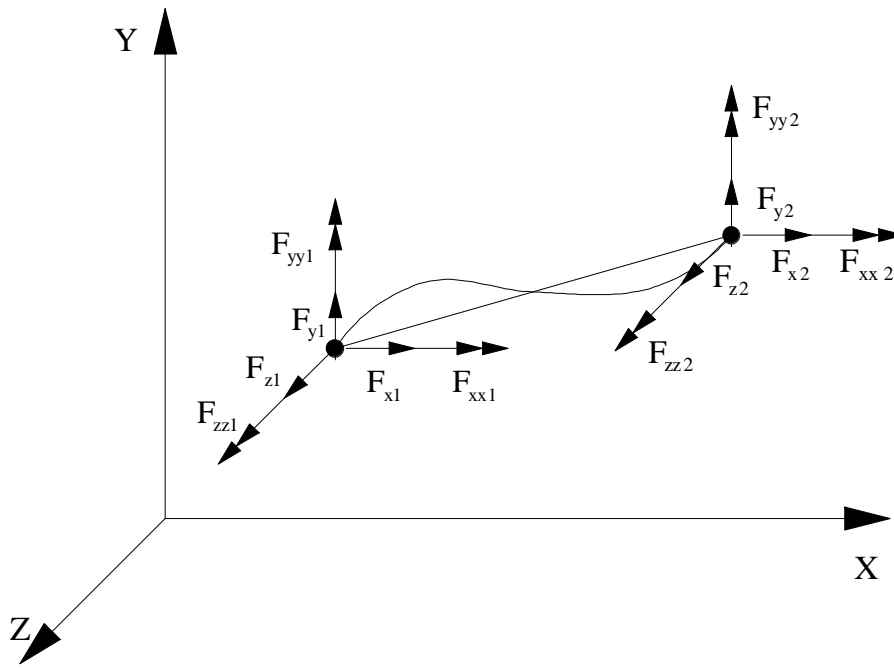
---

---

|                        |   |
|------------------------|---|
| <b>Description</b>     | Rayleigh damping 3D element   |
| <b>Mass/length</b>     | Mass per unit length  |
| <b>Parameters</b>      | Two proportionality constants ( $a_1$ & $a_2$ ) of mass and stiffness respectively, specified in that order.  |
| <b>Nodes</b>           | 3   |
| <b>Characteristics</b> | <p>Models Rayleigh damping effects.</p> <p>All <i>rld3</i> elements must have the same constant (<math>a_1</math> &amp; <math>a_2</math>) to model conventional Rayleigh damping.</p> <p>Nodes (1) and (2) define the element connectivity and its local x-axis. The y-axis lies in a plane defined by the x-axis and node (3), which can be a non-structural node.</p> |
| <b>Application</b>     | Dynamic analysis of plane frames.   |
| <b>Restrictions</b>    | ( $a_1$ ) should be set to zero for dynamic analysis involving ground excitation, otherwise damping would be proportional to absolute rather than relative frame velocity.  |
| <b>Group header</b>    | <p><b>sec.name</b> :An identifier referring to one of the <a href="#">cross-sections</a> declared in the <b>sections</b> module.</p> <p><b>mass/length</b>: Mass per unit length.</p> <p><b>parameters</b>: Defines parameters of Rayleigh damping elements.</p>  |

---

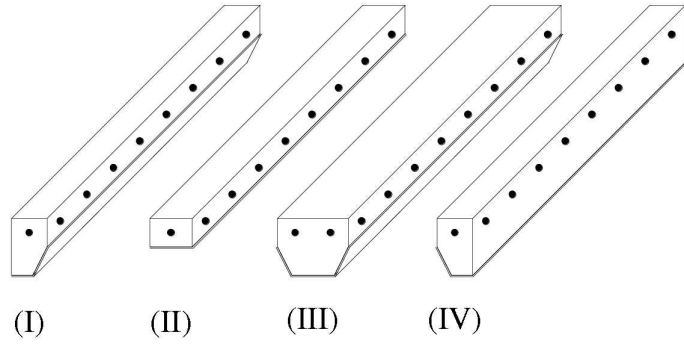
---



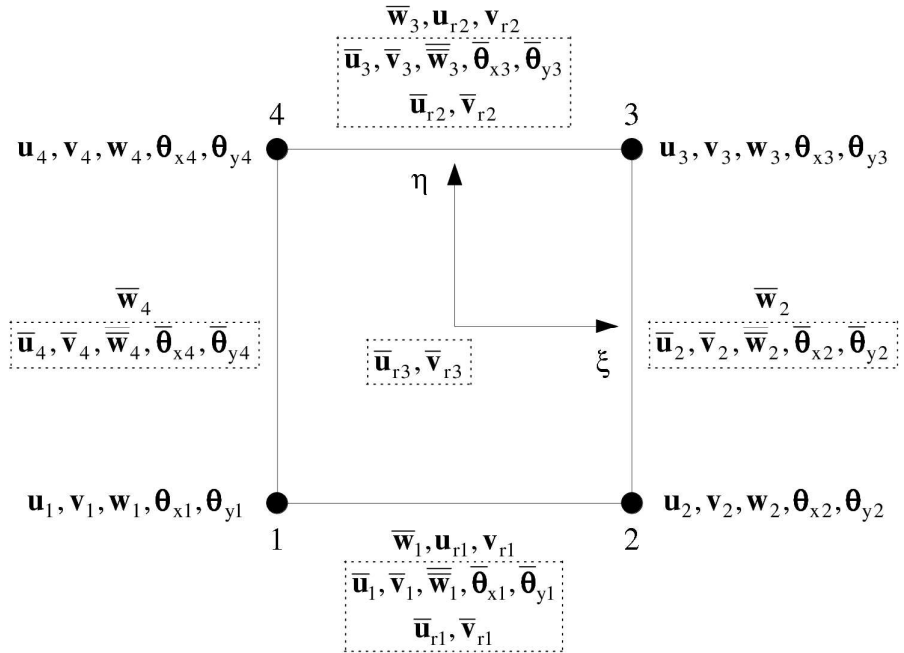
*Forces for element type rld3*

|                        |  |
|------------------------|--|
| <b>Description</b>     | 2-D flat shell element for composite floor slabs.  |
| <b>Nodes</b>           | 4  |
| <b>Characteristics</b> | <p>Geometrically orthotropic slab.</p> <p>4-noded composite and R/C slab element with additional rib and cover freedoms. It deals with the nonlinear analysis of composite floor slabs, enabling the modelling of material nonlinearities and geometric orthotropy through a modification of the Reissner-Mindlin hypothesis.</p> <p>The element can be used in a basic form employing bilinear shape functions or in a higher-order form employing quadratic shape functions for the normal rotations. This is achieved through the use of hierarchic additional freedoms, which are defined in this order:</p> $\mathbf{f}_a = \left\langle (\bar{\mathbf{w}})_{1 \rightarrow 4}, (\mathbf{u}_r, \mathbf{v}_r)_{1 \rightarrow 2}, (\bar{\mathbf{u}}, \bar{\mathbf{v}}, \bar{\mathbf{w}}, \bar{\boldsymbol{\theta}}_x, \bar{\boldsymbol{\theta}}_y)_{1 \rightarrow 4}, (\bar{\mathbf{u}}, \bar{\mathbf{v}})_{1 \rightarrow 3} \right\rangle^T$ <p>For the bilinear form, only the first 8 additional freedoms are used, with the remaining 26 additional freedoms employed in addition for the quadratic form. Individual additional freedoms may be <a href="#">restrained</a> as described in the <i>restraints</i> module.</p> <p>Elevated temperature may be specified using <a href="#">element load</a> type <i>tmp7</i> specified in this order:</p> $\langle T_1, \Delta T_1, T_2, \Delta T_2, T_3, \Delta T_3, T_4, \Delta T_4, T_5, \Delta T_5, T_6, \Delta T_6, T_7, T_8 \rangle$ <p>where <math>T_i</math> and <math>\Delta T_i</math> indicate respectively temperatures and temperature increments between the bottom of the cover and the top of the slab.</p> |
| <b>Application</b>     | Realistic modeling of composite floor slabs under extreme loading, including fire conditions.  |
| <b>Restrictions</b>    |  |
| <b>Group header</b>    | <p><b>sec.name</b>: An identifier referring to a cross-section of type <a href="#">cslb</a> declared in the sections module.</p> <p><b>type</b>: one of the following: <code>left.edge.rib</code>, <code>cover</code>, <code>central.rib</code>, and <code>right.edge.rib</code>.</p> <p><b>gauss.points</b>: 3 entries representing number of gauss points in the local x, y and z directions, respectively.</p> <p><b>[options]</b>: optional parameter indicating the element order <b>[bilinear quadratic]</b>; defaults to <b>bilinear</b>.</p>   |

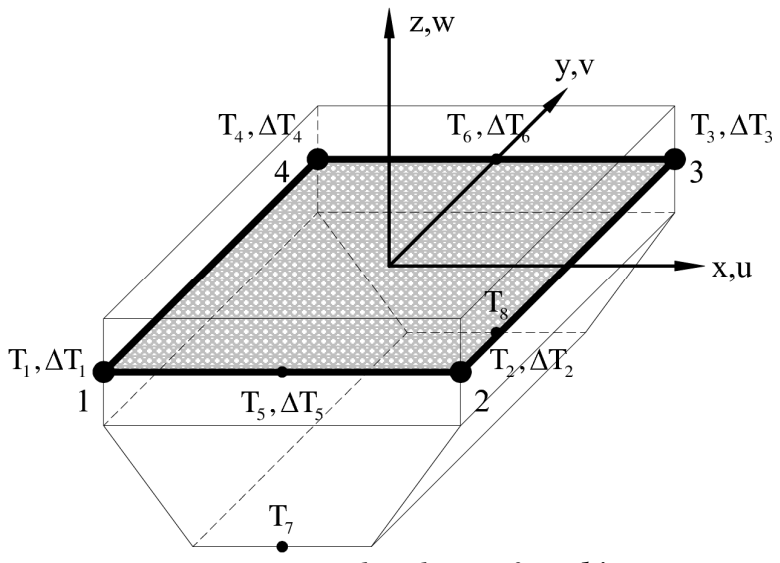
---



Element types for *cs14*: (I) left.edge.rib; (II) cover; (III) central.rib; (IV) right.edge.rib



Additional freedoms for element *cs14*



Temperature distribution for *cs14*

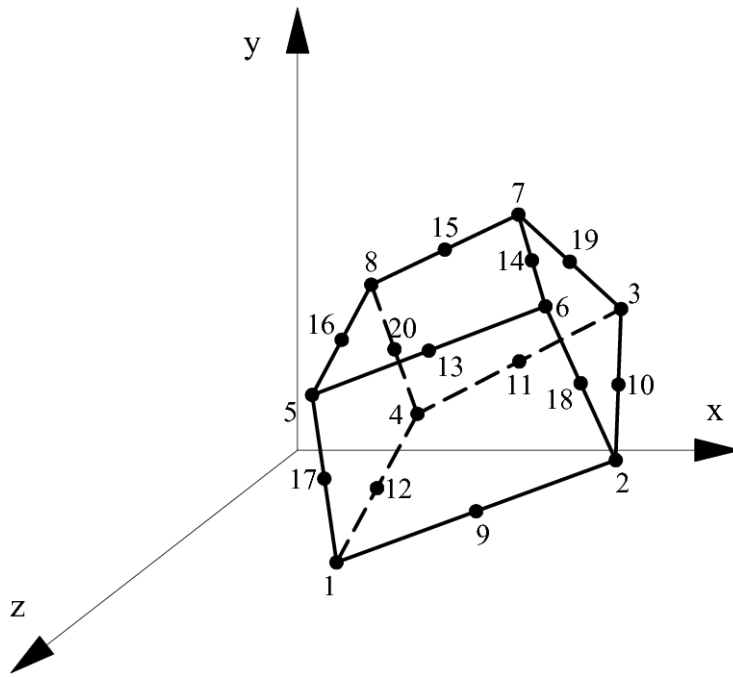
## bk20

---

|                        |   |
|------------------------|---|
| <b>Description</b>     | 20 noded 3D brick element.  |
| <b>Nodes</b>           | 20  |
| <b>Characteristics</b> | Models 3D continuum large displacement problems using Green's strain.<br>Applies to static, dynamic and elevated temperature analysis.<br>Allows direct specification of material density and Rayleigh damping parameters for dynamic analysis.   |
| <b>Application</b>     | Static/dynamic analysis of 3D continuum problems.   |
| <b>Restrictions</b>    | Works with material models <a href="#">beth</a> , <a href="#">bnsi</a> , <a href="#">bnsk</a> and <a href="#">tpth</a> .  |
| <b>Group header</b>    | <b>mat.name</b> :An identifier referring to one of the <a href="#">materials</a> declared in the <b>materials</b> module.<br><b>[gauss.points]</b> : optional total number of gauss points; defaults to 27 (ie. 3×3×3).<br><b>[density]</b> : optional material density used for dynamic analysis; defaults to zero.<br><b>[damping.parameter]</b> : two optional parameters for mass- and stiffness-proportional Rayleigh damping, respectively; default to the values of <b>mass.damping.parameter</b> and <b>stiffness.damping.parameter</b> specified in the <a href="#">default.parameters</a> module. |

---





*Nodal ordering for **bk20***

# Chapter 7. DATA SYNTAX

## 7.1 Introduction

A header-oriented syntax is utilized in ADAPTIC data files. Data modules are identified by means of unique headers, and only the first four characters in the header key words are necessary. However, if more than four characters of a key word are employed, the ADAPTIC data input module checks for the consistency of all characters.

Names or numbers employed, for example, as identifiers for elements or nodes can be up to 8 character long. However, if this number is exceeded only the first 8 characters are considered.

The following symbols are used for describing the ADAPTIC data syntax. Note that these symbols are used in the rest of this manual only for delivering information, and they must not be used within an ADAPTIC data file.

| <u>Symbol</u> | <u>Description</u>  |
|---------------|---|
| ( ..... )     | Parantheses used to include a list of items.  |
|               | Exclusive OR. For example ( <b>2d</b>   <b>3d</b> ) is equivalent to a single entry which can be either 2d or 3d.                     |
| [ ..... ]     | Brackets used to include optional item(s). For example [z] means that entry z is optional.  |
| < entry >     | Specifies the entry type. For example < integer > indicates an integer data entry.  |
| ^             | Indicates that the entries for the previous key word in the header can be defined by assignment outside the header line. For example, |

```
mat.name    model^    properties
indicates that the following two data modules,
mat.name    model    properties
m1          stl1    210e9 300e6 0.01
and,
model = stl1
mat.name    properties
m1          210e9 300e6 0.01
are equivalent.
```

## **7.2 General Facilities**

This sections describes general facilities which are available with all data modules, unless indicated otherwise.

## 7.2.1 Continuation

The ampersand ( **&** ) symbol can be used to continue data entry on the next line.

## 7.2.2 Comments

Comments can be added anywhere in the data file using the hash ( # ) symbol. All entries following a ( # ) on the current line are ignored.

### 7.2.3 Incrementation

The automatic incrementation facility can be used with some data modules. This is indicated where applicable. The general syntax is given below:

|                                      |                |       |                             |
|--------------------------------------|----------------|-------|-----------------------------|
| <b>f</b>                             | < entry {1} >  | ..... | < entry {n} >               |
| <b>r</b>                             | < inc. {1,1} > | ..... | < inc. {n,1} > < rep. {1} > |
| <b>r</b> [ <b>&lt;range{2}&gt;</b> ] | < inc. {1,2} > | ..... | < inc. {n,2} > < rep. {2} > |
| <b>r</b> [ <b>&lt;range{m}&gt;</b> ] | < inc. {1,m} > | ..... | < inc. {n,m} > < rep. {m} > |

- <entry {i}> ith entry on the first data line used for generation.
- <range {j}> Range of previously generated lines to be used for further incrementation.  
Syntax of <range {j}> is ( [<first {j}>] : [<last {j}>] ), for example 4:8.
- <inc. {i,j}> The increment to be used in the generation of the ith entries.  
If <entry {i}> is a character string then <inc{i,j}> must be a dash ( - ).
- <rep. {j}> The number of times each line in the range <range {j}> is incremented.

**Notes** The defaults for optional arguments are:

- <range {j}> = **1**:(total number of lines generated so far)
- <first {j}> = **1**
- <last{j}> = total number of lines generated so far

# 7.3 Input Modules

This sections describes the input modules available within ADAPTIC.

### 7.3.1 Analysis

This module specifies the analysis type.

---

---

```
analysis ( 2d | 3d ) ( eigenvalue | dynamic | static )
```

---

---

|                   |                             |
|-------------------|-----------------------------|
| <b>2d</b>         | Two dimensional analysis.   |
| <b>3d</b>         | Three dimensional analysis. |
| <b>eigenvalue</b> | Eigenvalue analysis.        |
| <b>dynamic</b>    | Dynamic analysis.           |
| <b>static</b>     | Static analysis.            |

#### Notes



### 7.3.2 Default.parameters

This module specifies some default parameters.

---

---

**default.parameters**

**mass.damping.parameter** = < real >

**stiffness.damping.parameter** = < real >

---

---

|                                    |   |
|------------------------------------|---|
| <b>mass.damping.parameter</b>      | Parameter used to specify mass-proportional damping, without the need for damping elements. Applies to mass elements <a href="#">cmm2</a> , <a href="#">lmm2</a> , <a href="#">cbm2</a> , <a href="#">cmm3</a> , <a href="#">lmm3</a> , <a href="#">cbm3</a> and <a href="#">bk20</a> . |
| <b>stiffness.damping.parameter</b> | Parameter used to specify stiffness-proportional damping, without the need for damping elements. Applies to elements <a href="#">bk20</a> .   |

#### Notes

### 7.3.3 Materials

This module specifies material identifiers referring to a particular model and model properties.

---

---

| <code>materials</code> |                     |                         |
|------------------------|---------------------|-------------------------|
| <code>mat.name</code>  | <code>model^</code> | <code>properties</code> |

---

---

|                         |  |
|-------------------------|--|
| <code>mat.name</code>   | A material identifier referring to the specified model and properties. The material name can be any alphanumeric string.               |
| <code>model</code>      | The material model used. The model should be one of those specified in <a href="#">Chapter 3</a> .                                     |
| <code>properties</code> | The material model properties. The number of properties must be as indicated in <a href="#">Chapter 3</a> for the corresponding model. |

#### Notes

### 7.3.4 Sections

This module specifies [cross-section](#) identifiers referring to a section type, constituent materials and section dimensions.

---

---

| <code>sections</code> |                                |                                    |                         |
|-----------------------|--------------------------------|------------------------------------|-------------------------|
| <code>sec.name</code> | <code>type</code> <sup>^</sup> | <code>mat.name</code> <sup>^</sup> | <code>dimensions</code> |

---

---

|                         |   |
|-------------------------|---|
| <code>sec.name</code>   | The name of the section which has the given properties. The name can be any alphanumeric string.  |
| <code>type</code>       | The section type. This must be one of the available types given in <a href="#">Chapter 5</a> .  |
| <code>mat.name</code>   | Specifies the material(s) used. The specified entry(s) should be one of the material identifiers declared in the <code>materials</code> module. |
| <code>dimensions</code> | Dimensions of the section. The number of dimension must be as defined in <a href="#">Chapter 5</a> for the corresponding section type.          |

#### Notes

### 7.3.5 Patterns

This module defines subdivision patterns utilised in automatic mesh refinement. The specified ratios indicate the number of potential subelements and their relative lengths.

---

---

| <code>patterns</code> |                     |
|-----------------------|---------------------|
| <code>pat.name</code> | <code>ratios</code> |

---

---

`pat.name`

A pattern identifier.

`ratios`

Integer values denoting relative lengths of zones where inelasticity is checked. The number of integers implicitly defines the number of zones.

#### Notes

### 7.3.6 Groups

This module defines properties for [element](#) groups. The number and nature of group properties depend on the type of elements for which the group is being established.

---

---

**groups**

**type.of.element** = < element type > \_ **grp.name** = <group header>

---

---

### 7.3.7 Structural.nodal.coordinates

This module defines coordinates of structural nodes.

---

---

|   |                 |                 |                   |
|---|-----------------|-----------------|-------------------|
| <code>structural.nodal.coordinates</code> |                 |                 |                   |
| <code>nod.name</code>                     | <code>x^</code> | <code>y^</code> | <code>[z^]</code> |

---

---

`nod.name`                    A node identifier which can be any alphanumeric string.

`x, y, z`                      Global nodal coordinates.

**Notes**                      `z` is only required for 3D analysis.

                                Incrementation can be used with this module.

### 7.3.8 Non.structural.nodal.coordinates

This module defines coordinates of structural nodes.

---

---

|   |                 |                 |                   |
|---|-----------------|-----------------|-------------------|
| <code>non.structural.nodal.coordinates</code> |                 |                 |                   |
| <code>nod.name</code>                         | <code>x^</code> | <code>y^</code> | <code>[z^]</code> |

---

---

`nod.name`                    A node identifier which can be any alphanumeric string.

`x, y, z`                    Global nodal coordinates.

**Notes**                    `z` is only required for 3D analysis.

Incrementation can be used with this module.

### 7.3.9 Element.connectivity

This module defines the connectivity of elements in a mesh configuration.

---

---

| <code>element.connectivity</code> |                        |                          |
|-----------------------------------|------------------------|--------------------------|
| <code>elm.name</code>             | <code>grp.name^</code> | <code>nod.name(s)</code> |

---

---

|                          |   |
|--------------------------|---|
| <code>elm.name</code>    | An element identifier which can be any alphanumeric string.   |
| <code>grp.name</code>    | An identifier referring to one of the groups declared in the <code>groups</code> module.  |
| <code>nod.name(s)</code> | The element end nodes defined in the<br><code>structural.nodal.coordinates</code> or<br><code>non.structural.nodal.coordinates</code><br>modules. |

**Notes** Incrementation can be used with this module.



### 7.3.10 Imperfections

This module specifies imperfection levels within elements of specific types.

---

---

|   |
|---|
| <b>imperfections</b>                      |
| <b>elm.name</b> <b>values<sup>^</sup></b> |

---

---

**elm.name**      The element which has the specified imperfection values.

**values**      The imperfection values for the element.

#### Notes

### 7.3.11 Restraints

This module defines nodal restraints.

---

---

|                   |                                 |
|-------------------|---------------------------------|
| <b>restraints</b> |                                 |
| [ <b>nod.name</b> | <b>direction</b> <sup>^</sup> ] |
| [ <b>elm.name</b> | <b>freedom</b> <sup>^</sup> ]   |

---

---

|                  |   |
|------------------|---|
| <b>nod.name</b>  | The node to be restrained.  |
| <b>direction</b> | Specifies the direction in which the defined node is restrained.<br>= <b>x</b> displacement along global X-axis.<br>= <b>y</b> displacement along global Y-axis.<br>= <b>z</b> displacement along global Z-axis.<br>= <b>rx</b> rotation about global X-axis.<br>= <b>ry</b> rotation about global Y-axis.<br>= <b>rz</b> rotation about global Z-axis. |
| <b>elm.name</b>  | The element to be restrained.   |
| <b>freedom</b>   | The element additional freedom to be restrained.<br>= <b>fa##</b> (e.g. fa5 and fa12 for freedoms 5 and 12).  |

**Notes** In two dimensional analysis, only **x**, **y** and **rz** directions can be specified.  
Multiple freedoms can be specified by one entry (e.g. x+y+ry indicates restraints in the three directions x, y and ry).  
Incrementation can be used with this module.

### 7.3.12 Conditions

This module specifies the conditions which govern the termination of the automatic control phase under a proportional static loading regime. These conditions are expressed in terms of limits on the load factor or displacements at specific freedoms.

---

---

```
conditions
( ( lf.cnd.name limits ) |
  ( disp.cnd.name nod.name direction limits ) )
```

---

---

|                            |  |
|----------------------------|--|
| <code>lf.cnd.name</code>   | Used for the load factor condition option, with the entry representing the condition identifier.   |
| <code>limits</code>        | Specifies the minimum and maximum limits.  |
| <code>disp.cnd.name</code> | Used for the displacement condition option, with the entry representing the condition identifier.  |
| <code>nod.name</code>      | The node name for which the displacement condition applies.  |
| <code>direction</code>     | The direction for which the displacement condition applies.<br>= <b>x</b> displacement along global X-axis.<br>= <b>y</b> displacement along global Y-axis.<br>= <b>z</b> displacement along global Z-axis.<br>= <b>rx</b> rotation about global X-axis.<br>= <b>ry</b> rotation about global Y-axis.<br>= <b>rz</b> rotation about global Z-axis. |

**Notes** Multiple direction specification is not allowed in this module.

This module is only applicable when using `proportional.loads` in the `applied.loading` module.

### 7.3.13 Linear.curves

This module specifies piecewise linear load curves for dynamic or time history loading.

---

```
linear.curves
start.time = <real>
crv.name = <name>
  ( (time load.factor) |
    (file = <file name> ]
      [delay = <real> ]
      [first.line = <integer> ]
      [last.line = <integer> ]
      [format = <format specification> ] )
```

---

|                    |  |
|--------------------|--|
| <b>start.time</b>  | Specifies the start time at which all load curves have a zero value. This entry must be less than the first <b>TIME</b> entry of all load curves |
| <b>crv.name</b>    | A curve identifier.  |
| <b>time</b>        | Time or pseudo-time column of entries.   |
| <b>load.factor</b> | Load factor column entries corresponding to the <b>time</b> entries.   |
| <b>file</b>        | The name of the file in which the load curve is stored. This option can be used if the load curve is stored in a file.                           |
| <b>delay</b>       | The time delay from the start time before the load curve is applied.<br>Default = 0  |
| <b>first.line</b>  | The line number in <b>file</b> corresponding to the first entry of the load curve.<br>Default = 1  |
| <b>last.line</b>   | The line number in <b>file</b> corresponding to the last entry of the load curve.<br>Default = <end of file>                                     |
| <b>format</b>      | A FORTRAN format specification by which the load curve entries are read from <b>file</b> .<br>Default = <free format>                            |

**Notes** Load factors of all load curves are taken as zero at the start time.

The time entries of a load curve recalled from a **file** are shifted by the value of **delay** which must always be positive. The load factor for such curves is zero between **start.time** and (**start.time** + **delay**).

This module is only applicable when using **time.history.loads** or **dynamic.loads** defined in the **applied.loading** module.

### 7.3.14 Integration.scheme

This module specifies the time integration scheme for dynamic analysis and its parameters.

---

```
integration.scheme
( scheme = newmark
  [ beta = < real > ]
  [ gamma = < real > ] ) |
( scheme = hilber.hughes.taylor
  [ alpha = < real > ]
  [ beta = < real > ]
  [ gamma = < real > ] )
```

---

|               |  |
|---------------|--|
| <b>scheme</b> | The time integration scheme.   |
| <b>alpha</b>  | HHT $\alpha$ parameter ( $>-1/3$ ).<br>Default = <b>0.0</b> (Newmark)                      |
| <b>beta</b>   | Newmark/HHT $\beta$ parameter.<br>Default = <b>0.25(1-<math>\alpha</math>)<sup>2</sup></b> |
| <b>gamma</b>  | Newmark/HTT $\gamma$ parameter.<br>Default = <b>0.5-<math>\alpha</math></b>                |

**Notes** This module is only applicable for dynamic analysis defined by the existence of `dynamic.loads` in the `applied.loading` module.

### 7.3.15 Applied.loading

This module specifies the type and the value of the applied loads.

---

```
applied.loading
[ initial.loads
  ( nod.name direction^ type^ value^ ) |
  ( elm.name type^ value^ ) ]
( ( proportional.loads
  nod.name direction^ type^ value^ ) |
  ( time.history.loads
  ( nod.name direction^ type^ crv.name^ value^ ) |
  ( elm.name type^ crv.name^ value^ ) ) |
  ( dynamic.loads
  ( nod.name direction^ type^ crv.name^ value^ ) |
  ( elm.name type^ crv.name^ value^ ) ) )
```

---

|                                 |  |
|---------------------------------|--|
| <code>initial.loads</code>      | These are static loads that are applied prior to any variable load. They can be forces or prescribed displacements applied at nodes in the global directions.  |
| <code>proportional.loads</code> | These are static loads having proportional variation. The magnitude of a load at any step is given by the product of its nominal value and the current load factor. Proportional loads may be forces or prescribed displacements applied at nodes in the global directions.  |
| <code>time.history.loads</code> | These are static loads varying according to different load curves in the pseudo-time domain. The magnitude of a load at any given pseudo-time is given by the product of its nominal value and the load factor obtained from its load curve at that pseudo-time. Time history loads may be forces or prescribed displacements applied at nodes in the global directions. |
| <code>dynamic.loads</code>      | These are dynamic loads varying according to different load curves in the real time domain. The magnitude of a load at any given time is given by the product of its nominal value and the load factor obtained from its load curve at that time. Dynamic loads can be forces or   |

|                        |   |
|------------------------|---|
|                        | accelerations applied at the nodes in the global directions.  |
| <code>nod.name</code>  | The node at which the load is applied.  |
| <code>nod.name</code>  | The node at which the load is applied.  |
| <code>direction</code> | The direction of the applied load:<br>= <b>x</b> displacement along global X-axis.<br>= <b>y</b> displacement along global Y-axis.<br>= <b>z</b> displacement along global Z-axis.<br>= <b>rx</b> rotation about global X-axis.<br>= <b>ry</b> rotation about global Y-axis.<br>= <b>rz</b> rotation about global Z-axis. |
| <code>type</code>      | Defines the type of the applied load<br>= ( <b>force</b>   <b>f</b> ) applied force.<br>= ( <b>displacement</b>   <b>d</b> ) applied displacement.<br>= ( <b>velocity</b>   <b>v</b> ) applied velocity.<br>= ( <b>acceleration</b>   <b>a</b> ) applied acceleration.<br>= element specific keyword for element loads.   |
| <code>elm.name</code>  | The element subjected to loading.   |
| <code>value</code>     | Nominal value of the applied load.  |
| <code>crv.name</code>  | The load curve defining the variation of dynamic or time history loads. The load curve must be declared in the <code>linear.curves</code> module.   |

## Notes

`proportional.loads`, `time.history.loads` and `dynamic.loads` cannot be used in the same analysis.

`initial.loads` can be used in static or dynamic analysis, but the module is optional. The load `type` can either be `force` or `displacement` for both static and dynamic analysis. In dynamic analysis only, `velocity` and `acceleration` can be used to indicate initial conditions, but these are only applicable to dynamic freedoms (i.e. those associated with mass/damping elements or support excitation).

`proportional.loads` or `time.history.loads` must be used in static analysis, for which the load `type` can either be `force` or `displacement`.

`dynamic.loads` must be used in dynamic analysis, for which the load `type` can either be `force` or `acceleration`.

Element loads cannot be applied as `proportional.loads`.



### 7.3.16 Equilibrium.stages

This module defines stages of time intervals at which structural equilibrium is established.

---

---

|                                 |                    |
|---------------------------------|--------------------|
| <code>equilibrium.stages</code> |                    |
| <code>end.of.stage</code>       | <code>steps</code> |

---

---

`end.of.stage` Defines the end time of a stage.

`steps` The number of steps within a stage.

**Notes** The time-step size for a stage is equal to the difference between the end time of the current stage and that of the previous stage divided by the number of steps of the current stage. For the first stage, the time step size is equal to the difference between the end of the first stage and the `start.time` defined in `linear.curves`.

This module is only applicable when using `time.history.loads` or `dynamic.loads` defined in the `applied.loading` module.

### 7.3.17 Phases

This module defines the control phases used to trace the load deflection curve for proportional loading. Three types of control are available: load, displacement and automatic control.

---

```

phases
( ( load.control
    increment      path      steps ) |
  ( displacement.control
    [( nod.name | elm.name )] direction increment path steps ) |
  ( automatic.control
    type      path      cnd.name ) )

```

---

|                                       |   |
|---------------------------------------|---|
| <b>load.control</b>                   | Represents the load-control option.   |
| <b>displacement.control</b>           | Represents the displacement-control option.   |
| <b>automatic.control</b>              | Represents the automatic displacement-control option.   |
| <b>increment</b>                      | Specifies the increment in the load factor for <b>load.control</b> , the increment of displacement for <b>displacement.control</b> , or the increment of arc length.  |
| <b>path</b>                           | Specifies the sign of the increment <ul style="list-style-type: none"> <li>( <b>continue</b>   <b>c</b> ) = follow the previous loading path.</li> <li>( <b>reverse</b>   <b>r</b> ) = unload relative to the previous loading path</li> <li>( <b>keep</b>   <b>k</b> ) = keep the sign of the increment as specified. This cannot be used for arc-length control.</li> </ul> |
| <b>steps</b>                          | The number of steps used to apply the increment.  |
| ( <b>nod.name</b>   <b>elm.name</b> ) | The name of the node or element used for displacement control. Omission of this implies arc-length control. Note that arc-length control cannot be used for the first phase.  |
| <b>direction</b>                      | The global direction in which the displacement control will be applied.   |
| <b>type</b>                           | The <b>automatic.control</b> type:  |

(**nod.control** | **elm.control** | **arc.length.control**)

(**translation** | **rotation** | x+y+z).

The direction specification x+y+z is used only for **arc.length.control**, and can represent any combination of the available translational freedoms (x, y and/or z).

**cond.name**

The name of the stopping condition used in the automatic-control option. The specified condition should be declared in the **conditions** module.

## Notes

The [path](#) entry, always be **keep** for the first phase.

**automatic.control** can not be the first phase.

### 7.3.18 Iterative.strategy

This module specifies the iterative strategy applied during a load or a time step.

---

|                               |   |               |
|-------------------------------|---|---------------|
| <b>iterative.strategy</b>     |   |               |
| [ <b>number.of.iterations</b> | = | < integer > ] |
| [ <b>initial.reformations</b> | = | < integer > ] |
| [ <b>step.reduction</b>       | = | < integer > ] |
| [ <b>divergence.iteration</b> | = | < integer > ] |
| [ <b>scaled.iterations</b>    | = | < integer > ] |
| [ <b>tol.relax.level</b>      | = | < integer > ] |
| [ <b>maximum.convergence</b>  | = | < real > ]    |
| [ <b>arc.flow.iteration</b>   | = | < integer > ] |

---

|                             |  |
|-----------------------------|--|
| <b>number.of.iterations</b> | The maximum number of iterations performed for each increment.<br>Default = 10   |
| <b>initial.reformations</b> | The number of initial reformations of the tangent stiffness matrix within an increment.<br>Default = 10  |
| <b>step.reduction</b>       | The step reduction factor used when convergence is not achieved.<br>Default = 5  |
| <b>divergence.iteration</b> | The iteration after which divergence checks are performed.<br>Default = 6  |
| <b>scaled.iterations</b>    | Number of iterations (> 2) after divergence over which the iterative displacement corrections are gradually scaled from zero to their full value.<br>Default = 1 (scaling off) |
| <b>tol.relax.level</b>      | Step-reduction level (0 to 3) from and above which tolerance relaxation (between <b>tolerance</b> and <b>maximum.tolerance</b> ) is allowed.<br>Default = 0                    |
| <b>maximum.convergence</b>  | The maximum convergence value allowed for any iteration<br>Default = 1000  |

`arc.flow.iteration`            Iteration number after which the normal flow method is applied with arc-length control.

Default = `number.of.iterations`

## Notes

Using a number of `initial.reformations` equal to the `number.of.iterations` is equivalent to the Newton- Raphson strategy.

Using a number of `initial.reformations` equal to 0 is equivalent to the modified Newton- Raphson strategy.

The solution is considered to be diverging if after the `divergence.iteration` the convergence of the current iteration is greater than that of the previous iteration. This check is not applied during the `scaled.iterations` stage and for a number of subsequent iterations equal to `divergence.iteration`, or if a relaxed solution within `maximum.tolerance` has been found. Scaling of iterative displacement corrections is applied after divergence if the remaining number of iterations exceeds `scaled.iterations`; this technique can be used to overcome convergence oscillations.

The increment is reduced by the `step.reduction` factor if convergence (full or relaxed) is not achieved, divergence occurs or `maximum.convergence` is exceeded. The original increment can be reduced for up to three levels.

The normal flow option for arc-length control can improve convergence characteristics, but does not guarantee that the displacement increments correspond exactly to the specified arc length.

### 7.3.19 Convergence.criteria

This module defines convergence criteria for the iterative procedures. The convergence criteria is based either on the out-of-balance norm or the maximum iterative displacement increment.

---

---

|                             |   |            |
|-----------------------------|---|------------|
| <b>convergence.criteria</b> |   |            |
| <b>tolerance</b>            | = | < real >   |
| ( <b>force.ref</b>          | = | < real >   |
| <b>moment.ref</b>           | = | < real > ) |
| ( <b>displacement.ref</b>   | = | < real >   |
| <b>rotation.ref</b>         | = | < real > ) |
| ( <b>work.ref</b>           | = | < real >   |
| [ <b>maximum.tolerance</b>  | = | < real > ] |

---

---

|                          |  |
|--------------------------|--|
| <b>tolerance</b>         | The required convergence tolerance for each load or time step.   |
| <b>force.ref</b>         | The force reference value used in calculating the convergence. Applicable to convergence criteria based on the out-of-balance norm.  |
| <b>moment.ref</b>        | The moment reference value used in calculating the convergence. Applicable to convergence criteria based on the out-of-balance norm.   |
| <b>displacement.ref</b>  | The displacement reference value used in calculating the convergence. Applicable to convergence criteria based on the maximum iterative displacement increment.  |
| <b>rotation.ref</b>      | The rotation reference value used in calculating the convergence. Applicable to convergence criteria based on the maximum iterative displacement increment.  |
| <b>work.ref</b>          | The work reference value used in calculating the convergence. Applicable to convergence criteria based on the energy norm.   |
| <b>maximum.tolerance</b> | The maximum tolerance to which a solution may be relaxed to if the specified <b>tolerance</b> could not be satisfied with the <a href="#">iterative.strategy</a> . This is used in conjunction with <b>tol.relax.level</b> . |

Default = 0

**Notes**

A `tolerance` and `maximum.tolerance` equal to zero is equivalent to an iterative procedure in which a fixed `number.of.iterations` is performed for each load or time step without consideration of convergence.

### 7.3.20 Output

This module specifies the frequency of numerical output.

---

---

**output**

**frequency** < integer > [**stress**] [**local.displacements** |  
**no.local.displacements**] **eigenvalue.interval** < integer >

---

---

**frequency**

Provides the frequency of the numerical output.

= 0 all equilibrium steps including step reduction levels.

= 1 all equilibrium steps without step reduction levels.

= n output every "n" equilibrium steps.

**stress**

Specified if element stresses are required. Applicable only to specific [element types](#).

[**no.**] **local.displacements**

Indicates whether the local displacements of elements are output, which is true by default.

**eigenvalue.interval**

Indicates the output interval for eigenvalue analysis during dynamic analysis.



### 7.3.21 Lanczos.eigenvalue

This module specifies the number of required eigenvalues and the range of natural frequencies of interest. The Lanczos eigenvalue algorithm is utilized.

---

---

```
lanczos.eigenvalue  
number.of eigenvalues = < integer >  
steps = < integer >  
w.min = < real >  
w.max = < real >  
shift = < real >  
  
[ starting.vector  
  nod.name      direction^      value^ ]
```

---

---

|                              |   |
|------------------------------|---|
| <b>number.of eigenvalues</b> | The number of required eigenvalues.   |
| <b>steps</b>                 | The number of <a href="#">Lanczos</a> steps to converge to the eigenvectors.  |
| <b>w.min</b>                 | Minimum natural frequency of interest.  |
| <b>w.max</b>                 | Maximum natural frequency of interest.  |
| <b>shift</b>                 | The frequency shift during the solution of the eigenvalue problem.  |
| <b>starting.vector</b>       | Initial vector used by the <a href="#">Lanczos</a> algorithm to derive eigenvectors.                                |
| <b>nod.name</b>              | Node name considered in the starting vector.  |
| <b>direction</b>             | The global direction which is given the specified values.   |
| <b>value</b>                 | The value of the entry in the starting vector corresponding to the <b>nod.name</b> in the global <b>direction</b> . |

**Notes**

The number of steps must be less or equal to the total number of freedoms for the structure.

**w.min**, **w.max** and **shift** are in rd/sec.

**shift** must be between **w.min** and **w.max**.

A random starting vector is generated if the starting vector module is not specified.

# Chapter 8. POST-PROCESSING

## 8.1 Start-Up

After the analysis has been *completed*, a post-processing application may be started to study the structural response graphically. Two graphics post-processing applications are available:

- 1) **ADAPTIC\_graphs** for plotting X-Y graphs. This is activated as follows

```
{prompt} adaptic -g [filename[.dat|.svg]]
```

- 2) **ADAPTIC\_shapes** for plotting deflected shapes. This is activated as follows

```
{prompt} adaptic -s [filename[.dat|.svs]]
```

The above applications are discussed separately in the following sections.

## 8.2 ADAPTIC\_graphs

### 8.2.1 General Facilities

The main items of the graphics region in the ADAPTIC\_graphs application are shown in Figure 8.2.1. The mouse buttons can be used to manipulate the appearance, size and position of each of the components, as discussed below.

#### Moving

Each of the items may be moved using the left mouse button with a single click to activate moving followed by a click and drag to move to the desired position.

#### Resizing

This facility only applies to the "Graph Area" item. It can be performed using the right mouse button with a single click to activate resizing followed by a click and drag of the bottom right corner to the desired position.

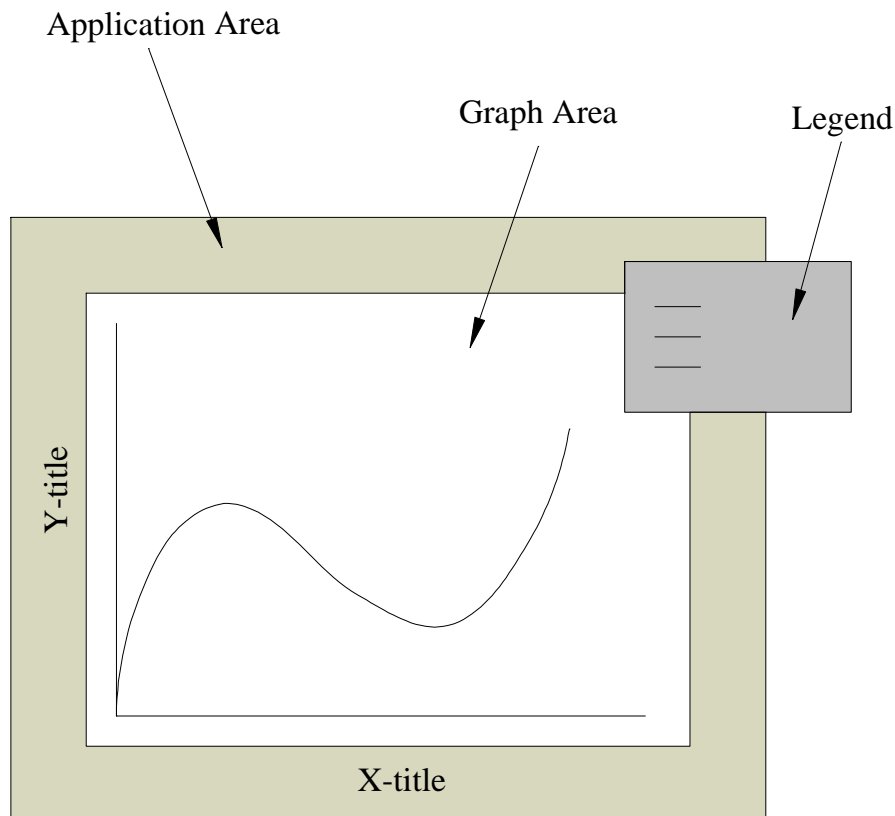


Figure 8.2.1. Graphics region of ADAPTIC\_graphs application

## 8.2.2 File

This menu option offers the following facilities discussed with reference to the initiating buttons.

### Data File

This invokes a form which allows the selection of the data file corresponding to the analysis that has been performed. Select the file *filename.dat* from the list of files in the directory where the analysis has been performed, where *filename* stands for the file identifier (e.g. *one\_storey*).

### Save

This button provides the means for storing plot information in a plot file for later retrieval. This is quite important for storing a permanent description of the plot, so that future modification can be performed with relative ease. Save files for the ADAPTIC\_graphs application are automatically given a ".svg" extension.

### Retrieve

This button retrieves ".svg" plot files that have been previously saved.

### Print/Export

This button allows i) the output of the plot description to an Encapsulated PostScript (EPS) file, which can be imported into word processing applications, or ii) the export of numerical data as X-Y columns within a text file, which can be used for further processing and plotting in spreadsheet applications.

### Exit

This allows the ADAPTIC\_graphs application to be terminated. Before exiting, make sure you have saved your plot file, if necessary.

### 8.2.3 Graphs

Three facilities can be accessed using this menu option, as discussed below.

#### New Curve

This allows the selection of X and Y entities for a new line graph. After selecting the entities, described hereafter, the Done button must be pressed followed by the Plot button for displaying the new line graph.

TIME/LOAD FACTORS: Allows the selection of time or load factor, depending on the type of analysis, as well as CPU time and output number for plotting. The output numbers are explicitly indicated for the various steps of the nonlinear analysis in the output file *filename.out*.

FORCES AT PRESCRIBED FREEDOMS: Allows the selection of forces at restrained or prescribed freedoms. The latter are defined as any freedom subject to a displacement or time-history acceleration load.

NODAL ENTITIES: This covers nodal displacements, velocities and accelerations. The last two should only be requested for dynamic analysis.

ELEMENT ENTITIES: This covers i) local element entities (e.g. element forces and local displacements which depend on the element type), and ii) stresses and strains, the availability of which depend on the element type.

ENERGY GROUPS: This allows the selection of energy components determined for pre-defined energy groups.

ARITHMETIC EXPRESSIONS: This is a general utility which allows the combination of entities corresponding to previous line graphs in arithmetic expressions. The following definitions are valid combinations, referring to the Y coordinate of line graph 1, the X coordinate of line graph 3 and the Y coordinate of line graph 2:

Y1-2-X3/6

Y2\*\*2-Y1\*X3

Y2-Y1

Such expressions should be typed in the dialogue box.

One application of this utility is for generating entities representing relative displacements rather than absolute nodal displacements.

#### Delete Curves

This allows previous line graphs to be deleted. This may be desirable if a curve is no longer required, especially if it was originally intended for providing X and Y coordinates to be manipulated by the ARITHMETIC EXPRESSIONS utility described above.

#### Clear All

This facility clears the contents of the current plot. This allows the construction of a new plot.

## 8.2.4 Customize

This option facilitates the customisation of the graph characteristics.

### Fonts

This allows the modification of the font name, size and style for the axes titles, axes labels and legend text.

### Axes

This facility can be used to modify the axes attributes, including thickness, colour, etc. It also allows individual axes to be modified in terms of minimum and maximum values, step size, scaling factor, etc.

### Lines

Each line graph can be customised using this facility with regard to thickness, style, colour, the use of points, activation/de-activation, the output range of interest, the corresponding legend text, etc.

### Legend

The legend can be customised with regard to visibility as well as the number of legend columns.

## 8.3 ADAPTIC\_shapes

### 8.3.1 General Facilities

The main components of the ADAPTIC\_shapes application are shown in Figure 8.3.1. The functionality of each component is described hereafter.

#### Graphics Display Area

This is the main graphics area where the structure is displayed. Each of the three mouse buttons has a *click-and-drag* functionality, which is modified by the Shift key, and which depend on whether normal or perspective [view](#) is selected.

*For normal view:*

- Lef button: rotate about planar axes, origin centred in structure.
- Lef button + Shift: rotate about out-of-plane axis.
- Right button: zoom in.
- Right button + Shift: zoom out.
- Middle button: move.
- Middle button + Shift: pan.

*For perspective view:*

- Lef button: rotate camera about planar axes, origin centred at focal point.
- Lef button + Shift: rotate camera about out-of-plane axis.
- Right button: move camera forwards/backwards.
- Right button + Shift: zoom camera in/out.
- Middle button: pan camera in plane.
- Middle button + Shift: move scene in plane.

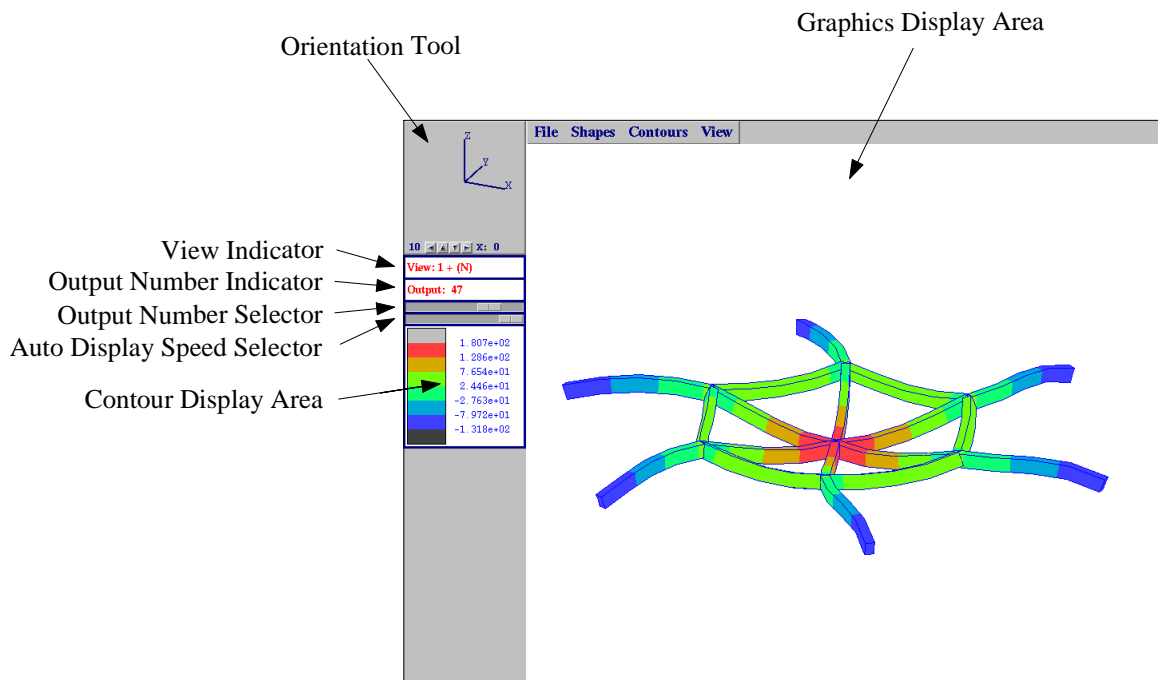


Figure 8.3.1. Components of ADAPTIC\_shapes application



### Orientation Tool

This tool displays the orientation of the global structural reference axes in the current view. The four arrow buttons can be used to change this orientation by i) selecting a global axis for incremental rotation, ii) specifying the increment of rotation, iii) applying positive rotation increments, and/or iv) applying negative rotation increments.

A single click with the mouse buttons on the orientation display area has the following functionality:

- Lef button: controlled customisation of current [view](#).
- Right button: turn on/off axes orientation in the Graphics Display Area.

### View Indicator

This displays the current view number (1, 2 or 3). The presence of (+) indicates that the current view is a subsequent modification of a stored view, whereas (-) indicates that the current view is a precursor to a stored view. Furthermore, (N) indicates a normal view, whereas (P) indicates a perspective view.

### Output Number Indicator

This displays the current output number, as well as the corresponding eigenvalue mode if any, in view. For example, “Output: 3” refers to the actual deflected shape in output number 3, “Output: 5 [M2]” refers to mode 2 of output number 5 with auto display/slider control given to varying the output number, while “Output: [5] M2” refers to the same mode and output number with auto display/slider control given to varying the mode number.

A single click with the left mouse button enables specification of output number and eigenvalue mode.

### Output Number Selector

This allows output number selection using a slider, which is more convenient for a quick browse through the deflected shapes.

### Auto Display Speed Selector

This enable the speed of automatic display for deflected shapes to be controlled using a slider.

### Contour Display Area

This area displays the contour colours and scale, and is activated by the [General Settings](#) button.

A single click with the mouse buttons on the contour display area has the following functionality:

- Lef button: customisation of [contours](#).
- Right button: turn on/off contour information in the Graphics Display Area.

### 8.3.2 File

This menu option offers the following facilities discussed with reference to the initiating buttons.

#### Data File

This allows the selection of the data filename, provided the application is started on the command line without a filename specification, i.e.:

```
{prompt} adaptic -s
```

#### Save

This button provides the means for storing plot information in a plot file for later retrieval. This is quite important for storing a permanent description of the plot, so that future modification can be performed with relative ease. Save files for the ADAPTIC\_shapes application are automatically given a ".svs" extension.

#### Retrieve

This button retrieves ".svs" plot files that have been previously saved.

#### Print

This button allows the output of the plot description to an Encapsulated PostScript (EPS) file, which can be imported into word processing applications.

#### General Settings

This button enables/disables the display of i) the initial shape alongside the deflected shape, ii) node and element labels, iii) contours, and iv) customisation of auto display/slider control.

The initial shape and labels are enabled by default for the undeflected configuration.

Control can be given to [Auto Display](#) and the [Output Number Selector \(Slider\)](#) to vary either the output number for a specific mode or the mode number for a specific output number. Also, a increment of output/mode numbers can be specified for Auto Display.

#### Exit

This allows the ADAPTIC\_shapes application to be terminated. Before exiting, make sure you have saved your plot file, if necessary.

### 8.3.3 Shapes

This menu option offers the following facilities discussed with reference to the initiating buttons.

#### Output Number

This specifies the output and mode numbers to be displayed.

Output number 0 refers to the initial undeflected configuration, with other numbers referring to various equilibrium states obtained during nonlinear analysis.

For a specific output number, mode number 0 refers to the actual deflected shape of the equilibrium state, while other mode numbers refer to eigenvalue modes if any have been obtained for this equilibrium state.

#### Auto Display

This enables an animation of the structural response or the eigenvalue modes through sequential automatic display of deflected shapes/modes.

Animation control can be given in the [General Settings](#) over varying the output numbers for a specific mode (0 for the deflected shape) or the mode numbers for a specific output number (0 for the initial configuration).

The speed of animation is controlled by the [Auto Display Speed Selector](#). The animation can be interrupted with a single mouse click with any button anywhere within the application window.

#### Customize

This allows the display of various element types to be customised, mainly in terms of i) basic or full plotting, ii) range of element to be excluded from view, iii) plotting divisions over element, iv) line colour, v) fill colour, vi) line thickness and vii) appearance of nodal and element labels. The customisation can be applied selectively for individual element types or uniformly for all element types.

### 8.3.4 Contours

This menu option offers the following facilities discussed with reference to the initiating buttons.

#### Select Entities

This allows the selection of entities associated with specific element types for contour plotting. Note that this facility may not be available for some element types. Furthermore, the plotting of contours in the Graphics Display Area is controlled by the specification under [General Settings](#).

#### Customize

This enables the specification of the number of contours, the associated colours and the corresponding numerical range, whether manual or automatic. An automatic contour range is established from the maximum and minimum values of the entities to be plotted.

### 8.3.5 View

This menu option offers the following facilities discussed with reference to the initiating buttons.

#### Scale

This specifies the displacement/mode scale to be used.

Two independent scale values can be specified for plotting the deflected shape (i.e. mode = 0) and the eigenvalue modes (i.e. mode > 0).

For large displacement analysis, the scale for the deflected shape (mode = 0) is normally specified as (1).

For eigenvalue analysis, a large scale ( $\gg 1$ ) may need to be specified to distinguish the mode shape from the initial undeflected shape.

#### Select

This allows the selection of any of the three stored views in addition to the previous view. By default, the three views correspond to normal views of the i) X-Y, ii) X-Z and iii) Y-Z planes.

#### Store

This allows the storage of the current view into one of the three available views.

#### Customize

This enables customisation of the current view, including i) axes orientation, ii) zoom centre, iii) zoom scale, and iv) normal/perspective specification.

# Chapter 9. EXAMPLES

## 9.1 Space dome subject to vertical apex load

The dome space structure shown in the figure has been widely considered in the verification of nonlinear analysis methods for 3D frames. The aim here is to be able to predict the lowest buckling mode of the dome.

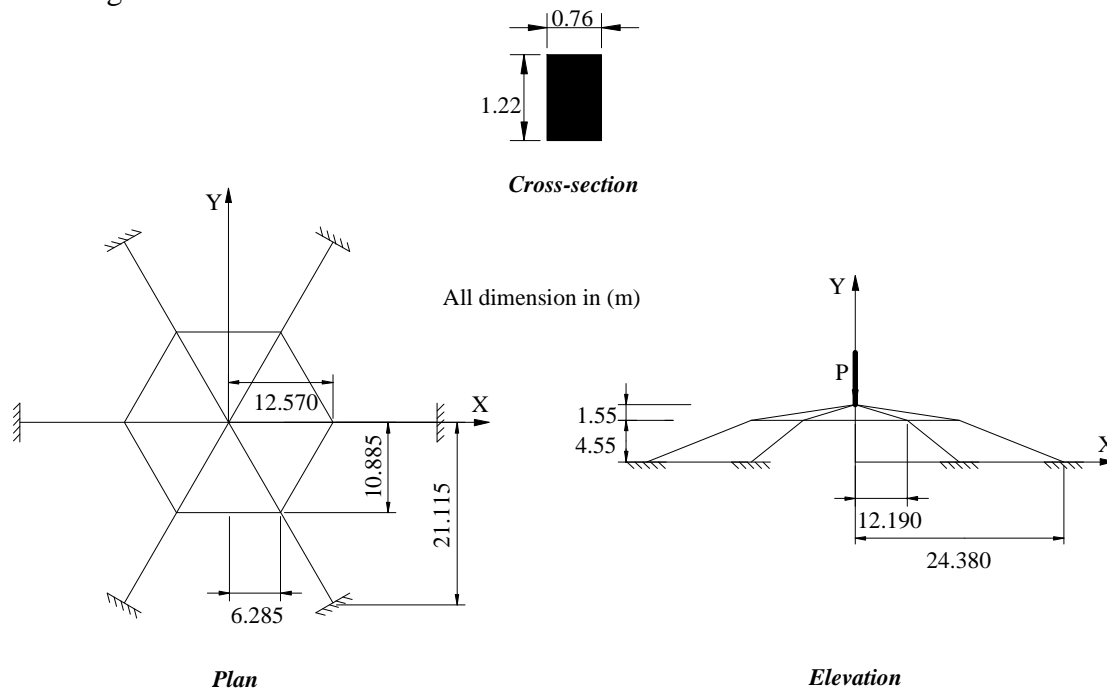


figure 9.1. Configuration of space dome subject to vertical apex load.

In order to illustrate the behaviour of the structure under an increasing load, here is going to be use ADAPTIC, which has the capability of predicting the large displacements static and dynamic behaviour of elastic and inelastic plane and space frames.

## 9.1.1 Data file

```

#
analysis 3d static (a)
#
materials (b)
  mat.name  model  properties
  mat1      beth  20690 0.172 0.0
sections (c)
  type = rss
  sec.name  mat.name  dimensions
  sect1     mat1     0.76 1.22
#
groups (d)
type = gel3
  grp.name  sec.name
  gp1       sect1
#
structural (e)
  nod.n  x  y  z
  1      0  0  0
  11     6.286 -10.886 -1.551
  12     12.572 0.002 -1.552
  13     6.288 10.888 -1.553
  14     -6.287 10.887 -1.552
  15     -12.573 0.003 -1.553
  16     -6.286 -10.886 -1.551
  21     12.190 -21.115 -6.10
  22     24.380 0 -6.10
  23     12.190 21.115 -6.10
  24     -12.190 21.115 -6.10
  25     -24.380 0 -6.10
  26     -12.190 -21.115 -6.10
#
non.structural (f)
  nod.name  x  y  z
  1011     6.286 -10.886 10
  1012     12.572 0.002 10
  1013     6.288 10.888 10
  1014     -6.287 10.887 10
  1015     -12.573 0.003 10
  1016     -6.286 -10.886 10
#
restraints (g)
  direction = x+y+z+rx+ry+rz
  nod.name
f  21
r  1 5
#
element.connectivity (h)
  grp.name = gp1
  elm.name  nod.name
f  1 21 11 1011
r  1 1 1 1 5
#
f  11 11 1 1011
r  1 1 0 1 5
#
f  21 11 12 1011
r  1 1 1 1 4

```

```

    26      16   11  1016
#
applied.loading \(i\)
  proportional
    type = force
      nod.name      direction  value
      1              z         -1
#
phases \(j\)
load.control
  increment  path  steps
  70         k    14
displacement.control
  nod.name  dire  increment  path  steps
  1         rz   -0.24     k    30
  1         z    -3         k    20
#
iterative.strategy \(k\)
number = 10
initial.reformations = 10
step.reduction = 10
divergence.iteration = 8
maximum.convergence = 1e+8
#
convergence.criteria \(l\)
  tolerance = 0.1e-5
  force.ref = 1
  moment.ref = 1
#
output \(m\)
frequency 1 local
#
end

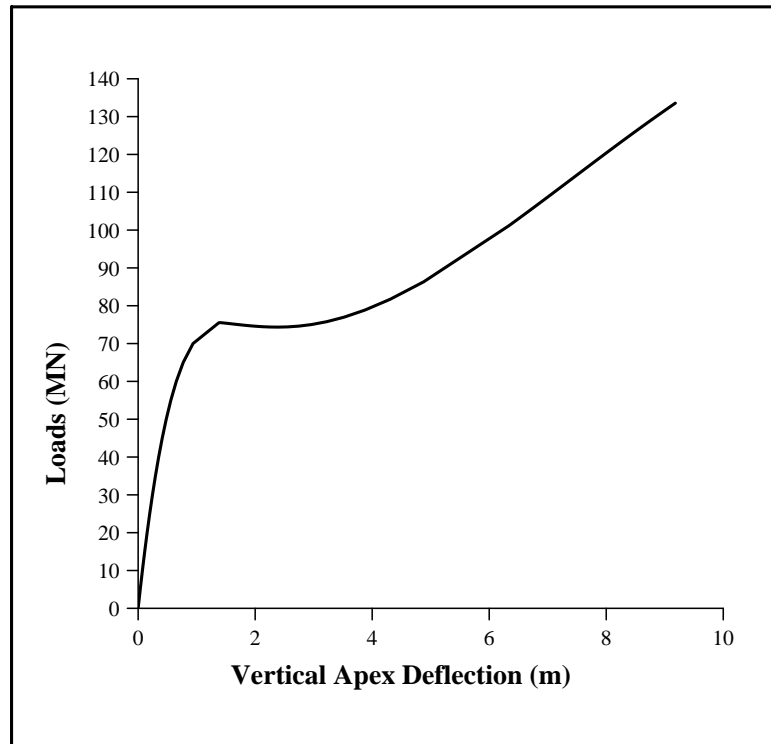
```



### 9.1.2 Structural behaviour

The nonlinear analysis is undertaken using one element per member, the response shown in the figure illustrate the ability of this method to predict the lowest buckling mode and to trace the associated post buckling path when an imperfect dome is considered.

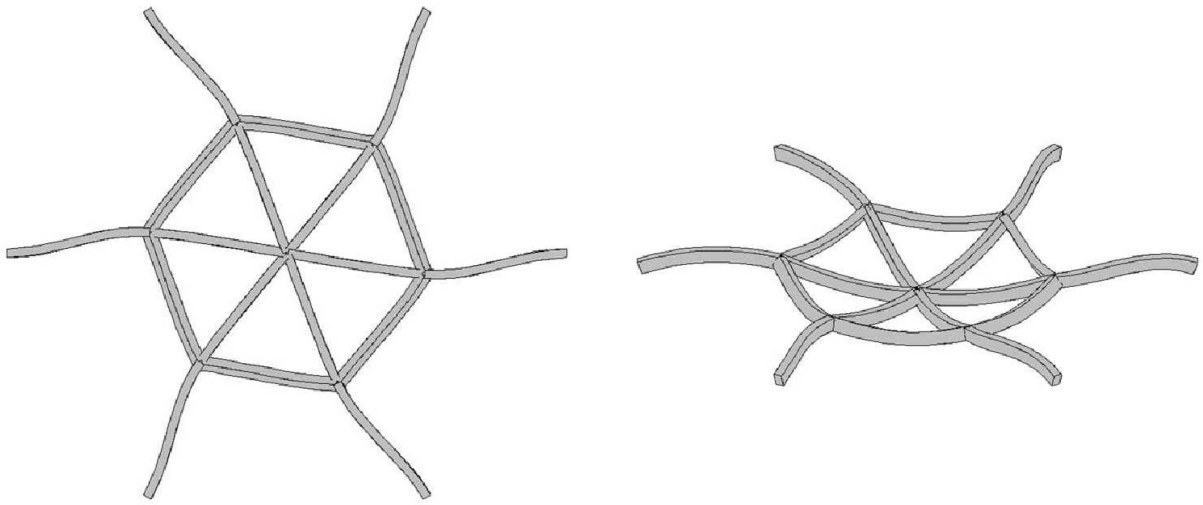
Here is been obtained how the vertical apex deflection varies while the load increases.



*figure 9.1.2.a. Response of space dome structure.*

As is shown in the figure there is a first path where the displacements of the structure are almost proportional to the load, but when is arrived to a certain value of load, the displacement are nonlinear, and they increase more than the load.

It is evident that the introduction of small imperfections activates the lowest buckling mode, which involves a planar rotational mode, like is shown in the *figure*. In the absence of these imperfections the dome deflects fully symmetric about the dome apex (*papers*).



*figure 9.1.2.b.Final deflected shape of space imperfect dome.*

### 9.1.3 Output file

ADAPTIC also give an output file, where can be found the way that the program calculates the structure.

```

          ELEMENT ASSEMBLY ORDER
----->>>> ----->>>> ----->>>> ----->>>> ----->>>> ----->>>> ----->>>> ----->>>>
1         11         21         26         2         12         22         13
14        15        16         6         25         3         23         4
24         5

```

```

MAXIMUM FRONT: (NODAL = 5) - (ADDITIONAL FREEDOMS = 0)
+++++

```

```

          V A R I A B L E      L O A D I N G
          +++++

```

```

PHASE NUMBER = 1
TYPE = LOAD CONTROL
INCREMENT FACTOR =0.700000E+02
NUMBER OF STEPS = 14

```

| OUTPUT | VARIABLE<br>LOAD<br>FACTOR | LEVEL | CONV.-NORM | ITERATIONS |
|--------|----------------------------|-------|------------|------------|
| 1      | 0.50000000E+01             | 0     | 0.546E-10  | 2          |
| 2      | 0.10000000E+02             | 0     | 0.883E-10  | 2          |
| 3      | 0.15000000E+02             | 0     | 0.162E-09  | 2          |
| 4      | 0.20000000E+02             | 0     | 0.293E-09  | 2          |
| 5      | 0.25000000E+02             | 0     | 0.568E-09  | 2          |
| 6      | 0.30000000E+02             | 0     | 0.118E-08  | 2          |
| 7      | 0.35000000E+02             | 0     | 0.266E-08  | 2          |
| 8      | 0.40000000E+02             | 0     | 0.659E-08  | 2          |
| 9      | 0.45000000E+02             | 0     | 0.185E-07  | 2          |
| 10     | 0.50000000E+02             | 0     | 0.613E-07  | 2          |
| 11     | 0.55000000E+02             | 0     | 0.255E-06  | 2          |
| 12     | 0.60000000E+02             | 0     | 0.860E-11  | 3          |
| 13     | 0.65000000E+02             | 0     | 0.918E-11  | 3          |
| 14     | 0.70000000E+02             | 0     | 0.325E-08  | 3          |

```

PHASE NUMBER = 2
NODAL DISPLACEMENT CONTROL
GLOBAL DIRECTION = RZ
CONTROLLED NODE = 1

```

```

DISPLACEMENT INCREMENT =-.240000E+00
NUMBER OF STEPS = 30

```

| OUTPUT<br>ITERATIONS | DISPLACEMENT<br>INCREMENT | VARIABLE<br>LOAD<br>FACTOR | LEVEL | CONV.-NORM |   |
|----------------------|---------------------------|----------------------------|-------|------------|---|
| 0                    | -.80000000E-03            | 0.74819797E+02             | 1     | 0.188E-07  | 8 |
| 0                    | -.80000000E-03            | 0.75170596E+02             | 1     | 0.871E-11  | 3 |
| 0                    | -.80000000E-03            | 0.75299433E+02             | 1     | 0.604E-06  | 2 |
| 0                    | -.80000000E-03            | 0.75366635E+02             | 1     | 0.150E-07  | 2 |
| 0                    | -.80000000E-03            | 0.75407861E+02             | 1     | 0.891E-09  | 2 |
| 0                    | -.80000000E-03            | 0.75435665E+02             | 1     | 0.921E-10  | 2 |

|    |                |                |   |           |   |
|----|----------------|----------------|---|-----------|---|
| 0  | -.80000000E-03 | 0.75455610E+02 | 1 | 0.155E-10 | 2 |
| 0  | -.80000000E-03 | 0.75470539E+02 | 1 | 0.650E-11 | 2 |
| 0  | -.80000000E-03 | 0.75482060E+02 | 1 | 0.838E-11 | 2 |
| 15 | -.80000000E-03 | 0.75491151E+02 | 1 | 0.800E-11 | 2 |
| 16 | -.80000000E-02 | 0.75524591E+02 | 0 | 0.594E-07 | 2 |
| 17 | -.80000000E-02 | 0.75521580E+02 | 0 | 0.938E-07 | 2 |
| 18 | -.80000000E-02 | 0.75503625E+02 | 0 | 0.108E-06 | 2 |
| 19 | -.80000000E-02 | 0.75474865E+02 | 0 | 0.130E-06 | 2 |
| 20 | -.80000000E-02 | 0.75436480E+02 | 0 | 0.161E-06 | 2 |
| 21 | -.80000000E-02 | 0.75388739E+02 | 0 | 0.203E-06 | 2 |
| 22 | -.80000000E-02 | 0.75331551E+02 | 0 | 0.260E-06 | 2 |
| 23 | -.80000000E-02 | 0.75264686E+02 | 0 | 0.338E-06 | 2 |
| 24 | -.80000000E-02 | 0.75187920E+02 | 0 | 0.446E-06 | 2 |
| 25 | -.80000000E-02 | 0.75101171E+02 | 0 | 0.599E-06 | 2 |
| 26 | -.80000000E-02 | 0.75004682E+02 | 0 | 0.820E-06 | 2 |
| 27 | -.80000000E-02 | 0.74899266E+02 | 0 | 0.694E-11 | 3 |
| 28 | -.80000000E-02 | 0.74786682E+02 | 0 | 0.629E-11 | 3 |
| 29 | -.80000000E-02 | 0.74670196E+02 | 0 | 0.106E-10 | 3 |
| 30 | -.80000000E-02 | 0.74555445E+02 | 0 | 0.885E-11 | 3 |
| 31 | -.80000000E-02 | 0.74451780E+02 | 0 | 0.843E-11 | 3 |
| 32 | -.80000000E-02 | 0.74374309E+02 | 0 | 0.462E-11 | 3 |
| 33 | -.80000000E-02 | 0.74346913E+02 | 0 | 0.996E-11 | 3 |
| 34 | -.80000000E-02 | 0.74406363E+02 | 0 | 0.492E-11 | 3 |
| 35 | -.80000000E-02 | 0.74607289E+02 | 0 | 0.875E-11 | 3 |
| 36 | -.80000000E-02 | 0.75027175E+02 | 0 | 0.149E-10 | 3 |
| 37 | -.80000000E-02 | 0.75770907E+02 | 0 | 0.351E-10 | 3 |
| 38 | -.80000000E-02 | 0.76977822E+02 | 0 | 0.792E-10 | 3 |
| 39 | -.80000000E-02 | 0.78843610E+02 | 0 | 0.182E-09 | 3 |
| 40 | -.80000000E-02 | 0.81695491E+02 | 0 | 0.723E-09 | 3 |
| 41 | -.80000000E-02 | 0.86304315E+02 | 0 | 0.138E-07 | 3 |
| 0  | -.80000000E-03 | 0.86954218E+02 | 1 | 0.269E-09 | 2 |
| 0  | -.80000000E-03 | 0.87640899E+02 | 1 | 0.566E-09 | 2 |
| 0  | -.80000000E-03 | 0.88387322E+02 | 1 | 0.911E-09 | 2 |
| 0  | -.80000000E-03 | 0.89206621E+02 | 1 | 0.155E-08 | 2 |
| 0  | -.80000000E-03 | 0.90117991E+02 | 1 | 0.273E-08 | 2 |
| 0  | -.80000000E-03 | 0.91151485E+02 | 1 | 0.496E-08 | 2 |
| 0  | -.80000000E-03 | 0.92359318E+02 | 1 | 0.273E-07 | 2 |
| 0  | -.80000000E-03 | 0.93849297E+02 | 1 | 0.670E-06 | 2 |
| 0  | -.80000000E-03 | 0.95940853E+02 | 1 | 0.391E-10 | 3 |
| 0  | -.80000000E-04 | 0.96260563E+02 | 2 | 0.129E-09 | 2 |
| 0  | -.80000000E-04 | 0.96572169E+02 | 2 | 0.103E-08 | 2 |
| 0  | -.80000000E-04 | 0.96917884E+02 | 2 | 0.345E-08 | 2 |
| 0  | -.80000000E-04 | 0.97312732E+02 | 2 | 0.186E-07 | 2 |
| 0  | -.80000000E-04 | 0.97785290E+02 | 2 | 0.182E-06 | 2 |
| 0  | -.80000000E-04 | 0.98411526E+02 | 2 | 0.918E-11 | 3 |
| 0  | -.80000000E-05 | 0.98520476E+02 | 3 | 0.146E-10 | 2 |
| 0  | -.80000000E-05 | 0.98609176E+02 | 3 | 0.365E-09 | 2 |
| 0  | -.80000000E-05 | 0.98703536E+02 | 3 | 0.417E-09 | 2 |
| 0  | -.80000000E-05 | 0.98806745E+02 | 3 | 0.109E-08 | 2 |
| 0  | -.80000000E-05 | 0.98921952E+02 | 3 | 0.363E-08 | 2 |
| 0  | -.80000000E-05 | 0.99054545E+02 | 3 | 0.171E-07 | 2 |
| 0  | -.80000000E-05 | 0.99215707E+02 | 3 | 0.145E-06 | 2 |
| 0  | -.80000000E-05 | 0.99438530E+02 | 3 | 0.636E-10 | 3 |

Phase (2) terminated

+++++

PHASE NUMBER = 3  
 NODAL DISPLACEMENT CONTROL  
 GLOBAL DIRECTION = Z  
 CONTROLLED NODE = 1

DISPLACEMENT INCREMENT =-.300000E+01  
NUMBER OF STEPS = 20

| OUTPUT<br>ITERATIONS | DISPLACEMENT<br>INCREMENT | VARIABLE<br>LOAD<br>FACTOR | LEVEL | CONV. -NORM |   |
|----------------------|---------------------------|----------------------------|-------|-------------|---|
| 42                   | -.15000000E+00            | 0.10110066E+03             | 0     | 0.224E-08   | 2 |
| 43                   | -.15000000E+00            | 0.10278682E+03             | 0     | 0.230E-08   | 2 |
| 44                   | -.15000000E+00            | 0.10449112E+03             | 0     | 0.233E-08   | 2 |
| 45                   | -.15000000E+00            | 0.10621060E+03             | 0     | 0.238E-08   | 2 |
| 46                   | -.15000000E+00            | 0.10794230E+03             | 0     | 0.247E-08   | 2 |
| 47                   | -.15000000E+00            | 0.10968333E+03             | 0     | 0.258E-08   | 2 |
| 48                   | -.15000000E+00            | 0.11143082E+03             | 0     | 0.273E-08   | 2 |
| 49                   | -.15000000E+00            | 0.11318196E+03             | 0     | 0.293E-08   | 2 |
| 50                   | -.15000000E+00            | 0.11493396E+03             | 0     | 0.318E-08   | 2 |
| 51                   | -.15000000E+00            | 0.11668410E+03             | 0     | 0.352E-08   | 2 |
| 52                   | -.15000000E+00            | 0.11842972E+03             | 0     | 0.395E-08   | 2 |
| 53                   | -.15000000E+00            | 0.12016827E+03             | 0     | 0.452E-08   | 2 |
| 54                   | -.15000000E+00            | 0.12189727E+03             | 0     | 0.527E-08   | 2 |
| 55                   | -.15000000E+00            | 0.12361439E+03             | 0     | 0.630E-08   | 2 |
| 56                   | -.15000000E+00            | 0.12531749E+03             | 0     | 0.772E-08   | 2 |
| 57                   | -.15000000E+00            | 0.12700463E+03             | 0     | 0.972E-08   | 2 |
| 58                   | -.15000000E+00            | 0.12867421E+03             | 0     | 0.127E-07   | 2 |
| 59                   | -.15000000E+00            | 0.13032502E+03             | 0     | 0.171E-07   | 2 |
| 60                   | -.15000000E+00            | 0.13195645E+03             | 0     | 0.240E-07   | 2 |
| 61                   | -.15000000E+00            | 0.13356868E+03             | 0     | 0.355E-07   | 2 |

## 9.2 K-frame subject to vertical load

The k-frame, shown in the figure, is subjected to an end force **P**, where load application in the middle of the upper frame. The buckling forces for this frame were also obtained with ADAPTIC, where the following values were reported using 4 elements.

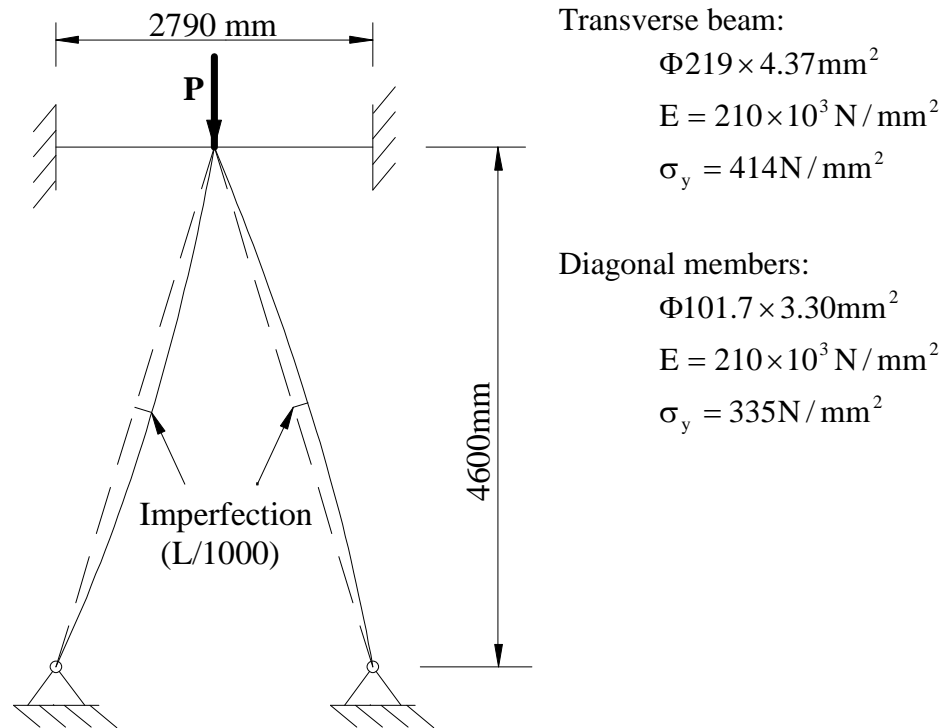


figure 9.2.a Geometric configuration of K-frame.

## 9.2.1 Data file

```

#
analysis 2d statics (a)
#
materials
  mat.name   model   properties
  mat1      stl1   0.210e6 0.335e3 0.00 (b)
  mat2      stl1   0.210e6 0.414e3 0.00
#
sections (c)
  type = chs
  sec.name   mat.name   dimensions
  sect1     mat1       101.7  3.30
  sect2     mat2       219.0  4.37
#
groups (d)
type = qph2
  grp.name   sec.name   subdivision
  grp1      sect1      t
  grp2      sect2      f
#
structural.nodal (e)
  nod.n      x          y
  f 1       0000.0     0000.0
  r 1       2790.0     0000.0 1
  f 3       0000.0     4600.0
  r 1       1395.0     0000.0 2
#
restraints (g)
  nod.name   direction
  f 1        x+y
  r 1         -      1
  f 3        x+y+rz
  r 2         -      1
#
element.connectivity (h)
  elm.name   grp.name   nod.name
  f 1        grp1      1 4
  r 1         -        3 -2 1
  f 3        grp2      3 4
  r 1         -        1 1 1
#
imperfection (n)
  elm.name   values
  1          -3.6 -4.8 -3.6
  2          3.6  4.8  3.6
#
applied.loading (i)
  proportional
  nod.name   direction   type   value
  4          y          force  -0.100e+7
#
condition (o)
  disp.cnd.name nod.name   direction   limits
  1            4          y          -300.0 0.0
#
phases (j)
load.control
  increment   path   steps

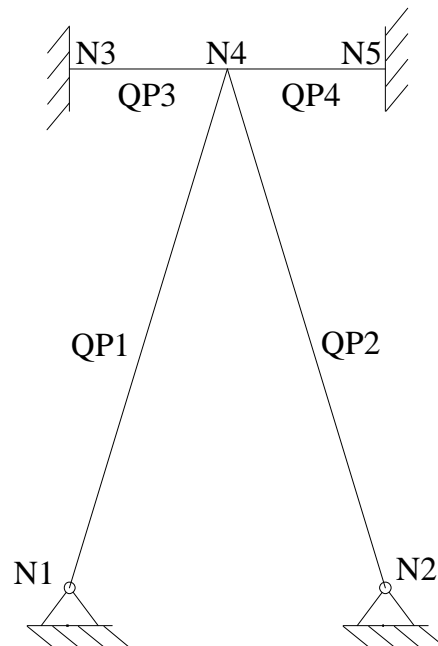
```

```

1.0      k      25
automatic.control
  type           path      cnd.name
  nodal translation      c      1
#use default iterative strategy
#iterative.strategy      (k)
#number = 10
#initial.reformations = 10
#step.reduction = 10
#divergence.iteration = 6
#maximum.convergence = 0.1e5
#
convergence.criteria      (l)
  tolerance = 0.1e-5
  force = 0.5e+6
  moment = 0.1e+8
#
output      (m)
frequency 0
#
end

```

**Note**            The following picture shows the names that have been given to the nodes and elements in the data file.

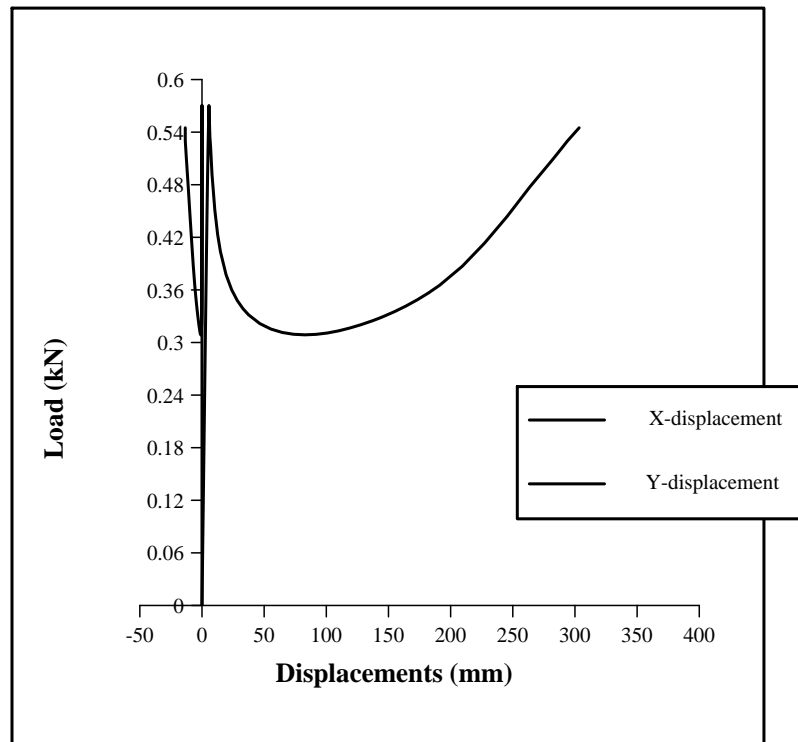


*figure 9.2.1 Nodes and elements of the K-frame.*



## 9.2.2 Structural behaviour

The nonlinear analysis is undertaken using one element per member, the response shown in the figure 9.2.2a shows the static response of K-frame.

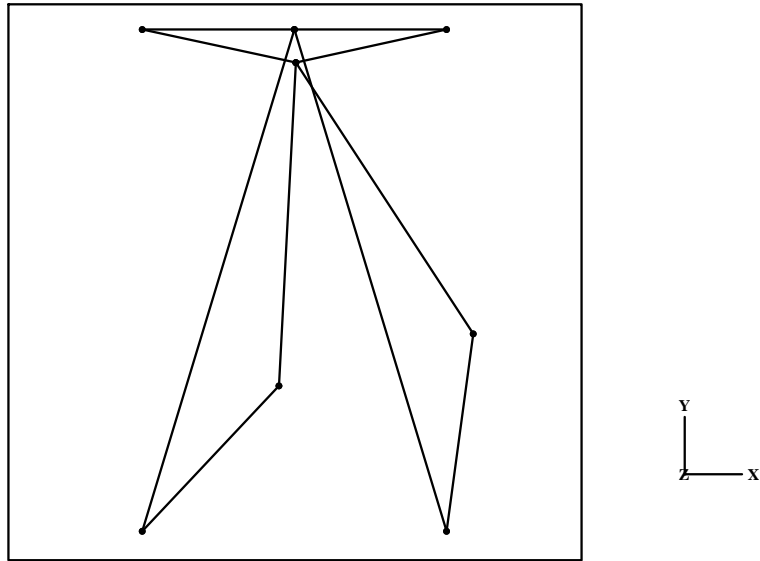


*figure 9.2.2a Static response of K-frame*

Here is shown the ability of this method to predict the lowest buckling mode and to trace the associated post-buckling path when an imperfect K-frame is considered.

The figure illustrates that the higher displacements of the structure are in the X-direction of the frame. When is arrived to a certain value of load, the displacement increase with fewer loads, and with minor load you can obtain higher displacements.

The following figure illustrates the response of modelling K-frame with the plastic-hinge approach.



*Figure 9.2.2b Deformed shape modelling with the plastic-hinge approach.*

It is evident that the introduction of small imperfections activates the lowest buckling mode, which involves a deflection shape, like is shown in the figure. In the absence of these imperfections the K-frame deflects fully symmetric about symmetry axes.

### 9.2.3 Output file

This is the output file given by ADAPTIC.

```

----->>>> ----->>>> ----->>>> ----->>>> ----->>>> ----->>>> ----->>>>
1           2           3           4

MAXIMUM FRONT: (NODAL =      3) - (ADDITIONAL FREEDOMS =      0)
+++++++

```

VARIABLE LOADING  
+++++++

```

PHASE NUMBER =      1
TYPE = LOAD CONTROL
INCREMENT FACTOR =0.100000E+01
NUMBER OF STEPS = 25

```

| OUTPUT | VARIABLE<br>LOAD<br>FACTOR | LEVEL | CONV.-NORM | ITERATIONS |
|--------|----------------------------|-------|------------|------------|
| 1      | 0.40000000E-01             | 0     | 0.155E-07  | 1          |
| 2      | 0.80000000E-01             | 0     | 0.242E-07  | 1          |
| 3      | 0.12000000E+00             | 0     | 0.390E-07  | 1          |
| 4      | 0.16000000E+00             | 0     | 0.651E-07  | 1          |
| 5      | 0.20000000E+00             | 0     | 0.114E-06  | 1          |
| 6      | 0.24000000E+00             | 0     | 0.209E-06  | 1          |
| 7      | 0.28000000E+00             | 0     | 0.407E-06  | 1          |
| 8      | 0.32000000E+00             | 0     | 0.854E-06  | 1          |
| 9      | 0.36000000E+00             | 0     | 0.135E-11  | 2          |
| 10     | 0.40000000E+00             | 0     | 0.913E-11  | 2          |
| 11     | 0.44000000E+00             | 0     | 0.725E-10  | 2          |
| 12     | 0.48000000E+00             | 0     | 0.595E-09  | 2          |
| 13     | 0.52000000E+00             | 0     | 0.414E-08  | 2          |
| 14     | 0.56000000E+00             | 0     | 0.408E-07  | 2          |
| 15     | 0.56800000E+00             | 1     | 0.460E-06  | 1          |
| 16     | 0.56960000E+00             | 2     | 0.672E-09  | 1          |
| 17     | 0.56992000E+00             | 3     | 0.965E-06  | 0          |
| 18     | 0.57024000E+00             | 3     | 0.974E-06  | 0          |

Phase (1) terminated  
+++++++

```

PHASE NUMBER =      2
NODAL DISPLACEMENT CONTROL
GLOBAL DIRECTION = Y
CONTROLLED NODE = 4

```

| OUTPUT<br>ITERATIONS                         | DISPLACEMENT<br>INCREMENT | VARIABLE<br>LOAD<br>FACTOR | LEVEL | CONV.-NORM |   |
|--|---------------------------|----------------------------|-------|------------|---|
| 19   | -.58886522E-02            | 0.57032137E+00             | 0     | 0.993E-06  | 1 |
| Plastic hinge formed for element 2 at node 4 |                           |                            |       |            |   |
| 20   | -.35331913E-01            | 0.56783100E+00             | 0     | 0.303E-07  | 2 |
| Plastic hinge formed for element 1 at node 4 |                           |                            |       |            |   |
| 21   | -.14132765E+00            | 0.56085432E+00             | 0     | 0.228E-06  | 2 |

```

***** ( SUBDIVISION OF ELEMENT 1 ) *****
*
*NUMBER OF NODES CREATED
*      1
* NOD.NAME      COORD'S (X,Y) RELATIVE TO END(1) OF SUBDIVIDED ELEMENT
* #n1           0.537226E+03      0.175588E+04
*-----*
*
*NUMBER OF ELEMENTS CREATED
*      2
* ELM.NAME      TYPE.OF.ELEMENT      NOD.NAMES
* #e1           qph2                 1      #n1
* #e2           qph2                 #n1    4
*-----*
*
*NUMBER OF IMPERFECT ELEMENTS
*      2
* ELM.NAME      TH1I      TH2I      TI
* #e1           -.152581E-02  0.152581E-02  -.700432E+00
* #e2           -.246847E-02  0.246847E-02  -.183324E+01
*****

```

```

***** ( SUBDIVISION OF ELEMENT 2 ) *****
*
*NUMBER OF NODES CREATED
*      1
* NOD.NAME      COORD'S (X,Y) RELATIVE TO END(1) OF SUBDIVIDED ELEMENT
* #n2           0.867206E+03      -.284399E+04
*-----*
*
*NUMBER OF ELEMENTS CREATED
*      2
* ELM.NAME      TYPE.OF.ELEMENT      NOD.NAMES
* #e3           qph2                 4      #n2
* #e4           qph2                 #n2    2
*-----*
*
*NUMBER OF IMPERFECT ELEMENTS
*      2
* ELM.NAME      TH1I      TH2I      TI
* #e3           0.247064E-02  -.247064E-02  0.183647E+01
* #e4           0.152364E-02  -.152364E-02  0.698438E+00
*****

```

```

22      -.56531062E+00      0.53452938E+00      0      0.354E-06      6
Plastic hinge formed for element #e3      at node 4
Plastic hinge formed for element #e2      at node #n1
Plastic hinge formed for element #e2      at node 4
Plastic hinge formed for element #e4      at node #n2
23      -.56531062E+00      0.52314632E+00      0      0.100E-06      5
Plastic hinge formed for element 3      at node 4
24      -.11306212E+01      0.49180805E+00      0      0.988E-06      5
Plastic hinge formed for element 3      at node 3
25      -.22612425E+01      0.45116331E+00      0      0.447E-06      8
Plastic hinge formed for element 4      at node 5
26      -.22612425E+01      0.42323379E+00      0      0.498E-06      6
27      -.22612425E+01      0.40365272E+00      0      0.896E-06      5
28      -.45224849E+01      0.37733661E+00      0      0.803E-06      8
29      -.45224849E+01      0.36011033E+00      0      0.356E-06      7
30      -.45224849E+01      0.34784546E+00      0      0.601E-06      6

```

|  |                |                |   |           |   |
|--|----------------|----------------|---|-----------|---|
| 31   | -.45224849E+01 | 0.33867433E+00 | 0 | 0.133E-06 | 6 |
| 32   | -.45224849E+01 | 0.33159941E+00 | 0 | 0.623E-06 | 5 |
| 33   | -.90449698E+01 | 0.32159929E+00 | 0 | 0.775E-06 | 8 |
| 34   | -.90449698E+01 | 0.31528570E+00 | 0 | 0.190E-06 | 8 |
| 35   | -.90449698E+01 | 0.31143394E+00 | 0 | 0.798E-06 | 7 |
| 36   | -.90449698E+01 | 0.30938842E+00 | 0 | 0.790E-06 | 7 |
| 37   | -.90449698E+01 | 0.30875711E+00 | 0 | 0.784E-06 | 7 |
| 38   | -.90449698E+01 | 0.30929004E+00 | 0 | 0.401E-06 | 8 |
| 39   | -.90449698E+01 | 0.31082759E+00 | 0 | 0.924E-06 | 7 |
| 40   | -.90449698E+01 | 0.31326084E+00 | 0 | 0.878E-06 | 7 |
| Plastic hinge closed for element #e2 at node 4 |                |                |   |           |   |
| 41   | -.90449698E+01 | 0.31650563E+00 | 0 | 0.473E-06 | 8 |
| 42   | -.90449698E+01 | 0.32032074E+00 | 0 | 0.269E-06 | 9 |
| 43   | -.90449698E+01 | 0.32469935E+00 | 0 | 0.664E-06 | 8 |
| 44   | -.18089940E+01 | 0.32565287E+00 | 1 | 0.121E-07 | 2 |
| 45   | -.18089940E+01 | 0.32663005E+00 | 1 | 0.141E-07 | 2 |
| 46   | -.18089940E+01 | 0.32763135E+00 | 1 | 0.119E-06 | 2 |
| Plastic hinge closed for element #e3 at node 4 |                |                |   |           |   |
| 47   | -.18089940E+01 | 0.32865710E+00 | 1 | 0.137E-07 | 2 |
| 48   | -.18089940E+01 | 0.32970771E+00 | 1 | 0.124E-07 | 2 |
| 49   | -.90449698E+01 | 0.33532282E+00 | 0 | 0.540E-06 | 7 |
| 50   | -.90449698E+01 | 0.34162424E+00 | 0 | 0.229E-06 | 7 |
| 51   | -.90449698E+01 | 0.34866739E+00 | 0 | 0.546E-06 | 6 |
| 52   | -.90449698E+01 | 0.35653812E+00 | 0 | 0.234E-06 | 6 |
| 53   | -.90449698E+01 | 0.36537081E+00 | 0 | 0.672E-06 | 5 |
| 54   | -.18089940E+02 | 0.38688104E+00 | 0 | 0.234E-06 | 6 |
| 55   | -.18089940E+02 | 0.41356265E+00 | 0 | 0.852E-06 | 8 |
| 56   | -.18089940E+02 | 0.44388832E+00 | 0 | 0.542E-06 | 8 |
| 57   | -.18089940E+02 | 0.47725230E+00 | 0 | 0.304E-06 | 6 |
| Plastic hinge formed for element 4 at node 4   |                |                |   |           |   |
| 58   | -.18089940E+02 | 0.50809231E+00 | 0 | 0.571E-06 | 9 |
| 59   | -.36179879E+01 | 0.51444736E+00 | 1 | 0.329E-07 | 2 |
| 60   | -.36179879E+01 | 0.52086955E+00 | 1 | 0.348E-07 | 2 |
| 61   | -.36179879E+01 | 0.52735930E+00 | 1 | 0.362E-07 | 2 |
| 62   | -.72359759E+00 | 0.52866515E+00 | 2 | 0.412E-06 | 1 |
| 63   | -.72359759E+00 | 0.52995151E+00 | 2 | 0.924E-08 | 2 |
| 64   | -.72359759E+00 | 0.53110568E+00 | 2 | 0.181E-07 | 1 |
| 65   | -.72359759E+00 | 0.53225959E+00 | 2 | 0.181E-07 | 1 |
| 66   | -.72359759E+00 | 0.53341324E+00 | 2 | 0.180E-07 | 1 |
| 67   | -.36179879E+01 | 0.53917749E+00 | 1 | 0.391E-09 | 2 |
| 68   | -.36179879E+01 | 0.54493498E+00 | 1 | 0.384E-09 |   |

### 9.3 Lee's frame

The Lee's frame, shown in the figure 9.3, is subjected to an end force P. The buckling forces for this frame were also obtained with ADAPTIC, where the following values were reported using 3 elements.

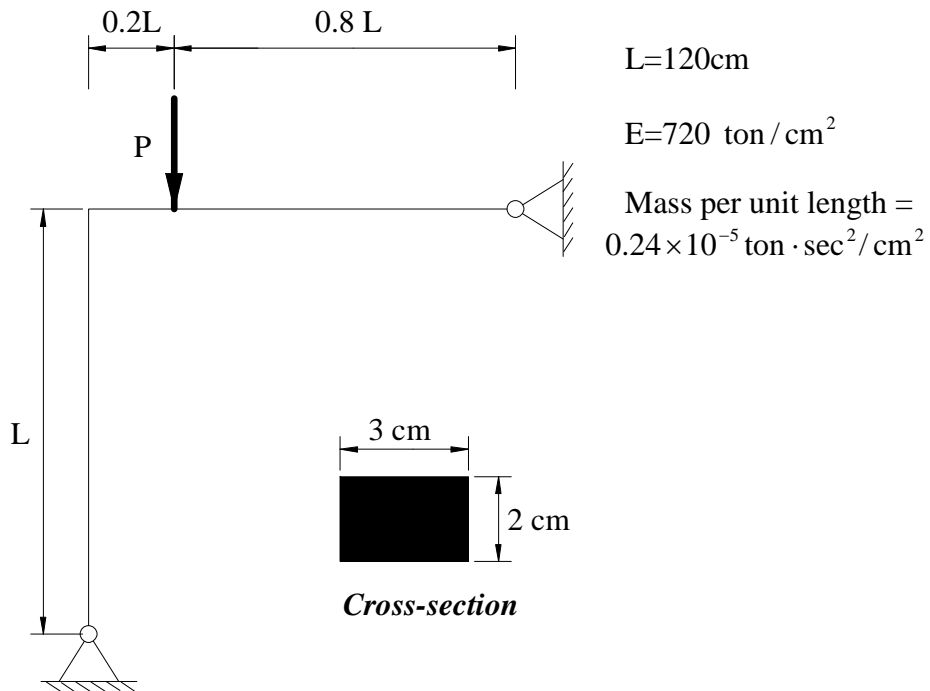


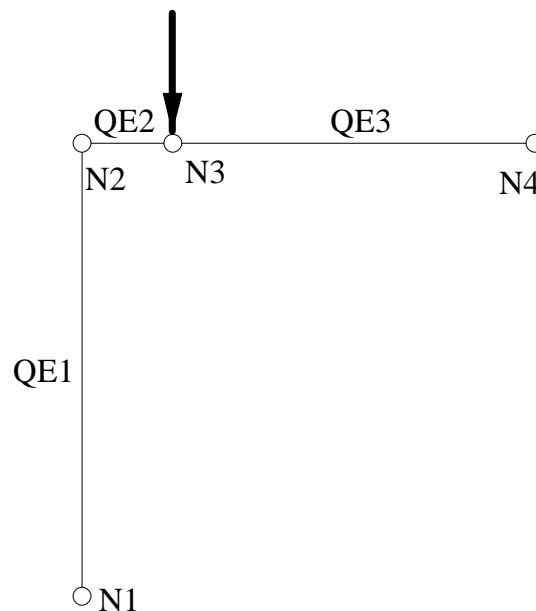
figure 9.3 Geometry and loading of Lee's frame.

### 9.3.1 Data file

```
#
analysis 2d statics (a)
# control start
#
#
materials (b)
  mat.name      model properties
  mat1          st11 0.720e3 0.100e1 0.00
#
sections (c)
  type = rss
  sec.name      mat.name  dimensions
  sect1         mat1      3.0 2.0
#
groups (d)
type.of.element = gel2
  grp.name      sec.name
  grp1          sect1
#
structural (e)
  nod.n         x         y
  1             0.00      0.00
  2             0.00      120.00
  3             24.00     120.00
  4             120.00    120.00
#
restraints (g)
  nod.name      direction
  1             x+y
  4             x+y
#
element.connectivity (h)
  elm.name      grp.name  nod.
  f 1           grp1      1 2
  r 1           -         1 1 2
#
applied.loading (i)
proportional.loads
  nod.name      direction  type  value
  3             y          force -0.10e+1
#
condition (o)
  lf.cnd.name   limits
  1             -2.0 2.0
  disp.cnd.name nod.name  direction  limits
  2             3         x            -0.12e+3 0.12e+3
  3             3         y            -0.12e+3 0.12e+3
#
phases (j)
load.control
  increment     path      steps
  0.2e+1        k         20
automatic.control
  type          path      cnd.name
  nodal translation  c         1 2 3
#
iterative.strategy (k)
number = 5
```

```
initial.reformations = 5
step.reduction = 5
divergence.iteration = 4
maximum.convergence = 0.1e3
#
convergence.criteria (1)
  tolerance = 0.1e-5
  force = 0.2e+1
  mome = 0.1e+3
#
output (m)
frequency 0
#
end
```

**Note:** The elements and the nodes that are used are shown in the figure 9.3.1.



*figure 9.3.1 Nodes and elements of Lee's frame.*

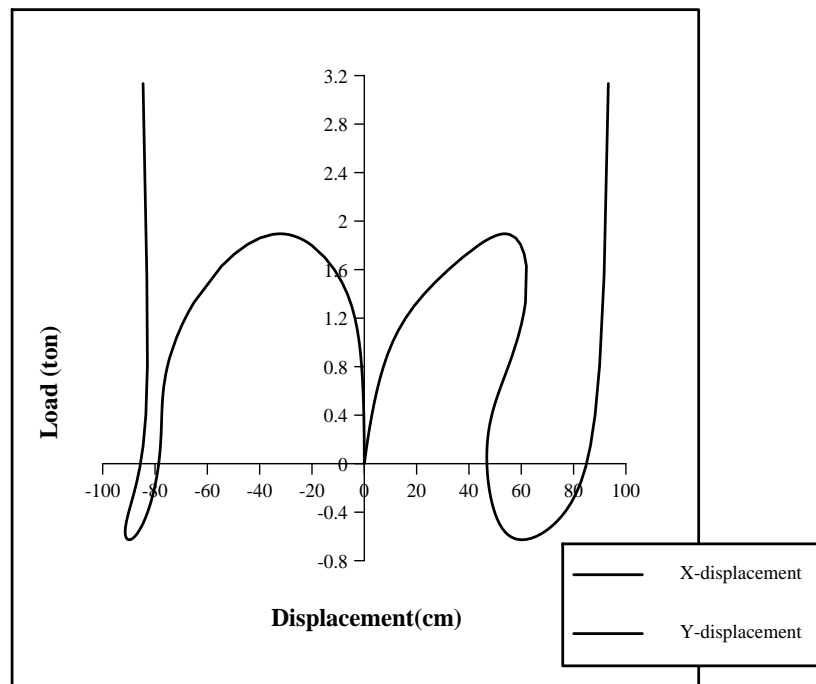


### 9.3.2 Structural behaviour

The nonlinear analysis is undertaken using one element per member. The following figures show the static response of Lee's frame.

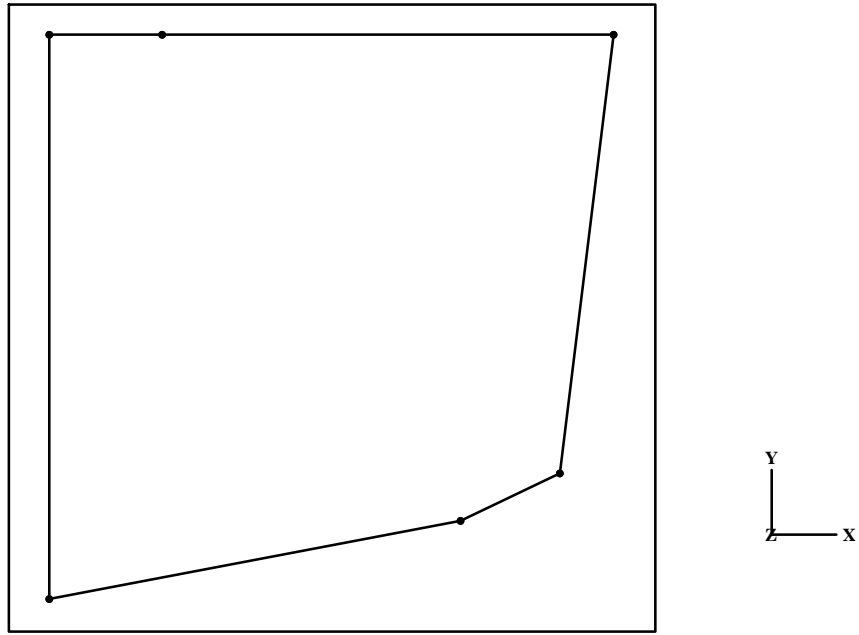
The node 1 only experiments rotation, as could be seen in the figure. It has the same behaviour as the node 4.

The nodes 2 and 3 have similar behaviour,



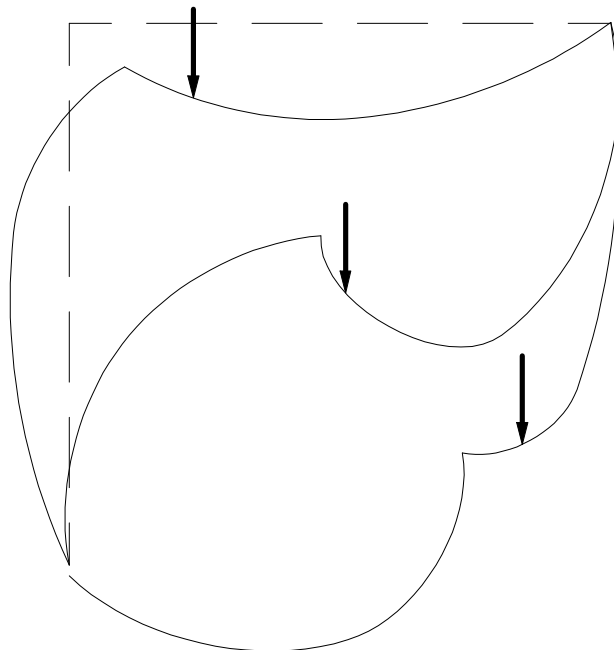
*figure 9.3.2a Static response of Lee's frame at node 3.*

This is the deformed shape of the Lee's frame. As it could be seen, nodes 1 and 4 only experiment rotation, and the displacements of node 2 are bigger than the displacements of node 3, even the develop in the time follows the same tendency.



*figure 9.3.2b Deflected shape of Lee's frame.*

The real deflected shape of Lee's frame when the load increase vary like is shown in the following figure.



*figure 9.3.2c Deflected shape of Lee's frame during static loading.*

### 9.3.3 Output file

```

ELEMENT ASSEMBLY ORDER
----->>> ----->>> ----->>> ----->>> ----->>> ----->>> ----->>>
1         2         3

```

```

MAXIMUM FRONT: (NODAL = 2) - (ADDITIONAL FREEDOMS = 0)
+++++++

```

```

VARIABLE LOADING
+++++++

```

```

PHASE NUMBER = 1
TYPE = LOAD CONTROL
INCREMENT FACTOR =0.200000E+01
NUMBER OF STEPS = 20

```

| OUTPUT | VARIABLE<br>LOAD<br>FACTOR | LEVEL | CONV.-NORM | ITERATIONS |
|--------|----------------------------|-------|------------|------------|
| 1      | 0.10000000E+00             | 0     | 0.489E-09  | 3          |
| 2      | 0.20000000E+00             | 0     | 0.926E-08  | 3          |
| 3      | 0.30000000E+00             | 0     | 0.304E-07  | 3          |
| 4      | 0.40000000E+00             | 0     | 0.392E-07  | 3          |
| 5      | 0.50000000E+00             | 0     | 0.357E-07  | 3          |
| 6      | 0.60000000E+00             | 0     | 0.314E-07  | 3          |
| 7      | 0.70000000E+00             | 0     | 0.305E-07  | 3          |
| 8      | 0.80000000E+00             | 0     | 0.343E-07  | 3          |
| 9      | 0.90000000E+00             | 0     | 0.459E-07  | 3          |
| 10     | 0.10000000E+01             | 0     | 0.711E-07  | 3          |
| 11     | 0.11000000E+01             | 0     | 0.118E-06  | 3          |
| 12     | 0.12000000E+01             | 0     | 0.187E-06  | 3          |
| 13     | 0.13000000E+01             | 0     | 0.242E-06  | 3          |
| 14     | 0.14000000E+01             | 0     | 0.244E-06  | 3          |
| 15     | 0.15000000E+01             | 0     | 0.245E-06  | 3          |
| 16     | 0.16000000E+01             | 0     | 0.434E-06  | 3          |
| 17     | 0.17000000E+01             | 0     | 0.152E-11  | 4          |
| 18     | 0.18000000E+01             | 0     | 0.100E-08  | 4          |
| 19     | 0.18200000E+01             | 1     | 0.380E-12  | 3          |
| 20     | 0.18400000E+01             | 1     | 0.529E-11  | 3          |
| 21     | 0.18600000E+01             | 1     | 0.197E-09  | 3          |
| 22     | 0.18800000E+01             | 1     | 0.803E-07  | 3          |
| 23     | 0.18840000E+01             | 2     | 0.736E-07  | 2          |
| 24     | 0.18880000E+01             | 2     | 0.499E-06  | 2          |
| 25     | 0.18920000E+01             | 2     | 0.340E-09  | 3          |
| 26     | 0.18928000E+01             | 3     | 0.144E-08  | 2          |
| 27     | 0.18936000E+01             | 3     | 0.929E-08  | 2          |
| 28     | 0.18944000E+01             | 3     | 0.145E-06  | 2          |
| 29     | 0.18952000E+01             | 3     | 0.462E-07  | 3          |

```

Phase (1) terminated
+++++++

```

```

PHASE NUMBER = 2
NODAL DISPLACEMENT CONTROL
GLOBAL DIRECTION = X
CONTROLLED NODE = 2

```

```

VARIABLE
DISPLACEMENT      LOAD

```

| OUTPUT<br>ITERATIONS | INCREMENT      | FACTOR         | LEVEL | CONV. -NORM |   |
|----------------------|----------------|----------------|-------|-------------|---|
| 30                   | 0.12676487E+01 | 0.18951791E+01 | 0     | 0.635E-09   | 2 |
| 31                   | 0.25352974E+01 | 0.18902504E+01 | 0     | 0.121E-06   | 2 |
| 32                   | 0.50705949E+01 | 0.18612923E+01 | 0     | 0.114E-10   | 3 |
| 33                   | 0.50705949E+01 | 0.18077847E+01 | 0     | 0.405E-11   | 3 |
| 34                   | 0.50705949E+01 | 0.17303899E+01 | 0     | 0.130E-11   | 3 |
| 35                   | 0.50705949E+01 | 0.16283372E+01 | 0     | 0.269E-06   | 2 |
| 36                   | 0.10141190E+02 | 0.13300448E+01 | 0     | 0.612E-07   | 3 |
| 37                   | 0.20282379E+01 | 0.12478470E+01 | 1     | 0.614E-07   | 2 |
| 38                   | 0.20282379E+01 | 0.11529115E+01 | 1     | 0.443E-06   | 2 |
| 39                   | 0.20282379E+01 | 0.10386773E+01 | 1     | 0.630E-11   | 3 |
| 40                   | 0.20282379E+01 | 0.88635252E+00 | 1     | 0.357E-07   | 3 |
| 41                   | 0.40564759E+00 | 0.84608354E+00 | 2     | 0.138E-06   | 2 |
| 42                   | 0.40564759E+00 | 0.79871870E+00 | 2     | 0.702E-12   | 3 |
| 43                   | 0.40564759E+00 | 0.73803157E+00 | 2     | 0.924E-09   | 3 |
| 44                   | 0.40564759E+00 | 0.63150114E+00 | 2     | 0.342E-11   | 5 |

Current control type terminated  
\*\*\*\*\*

PHASE NUMBER = 2  
NODAL DISPLACEMENT CONTROL  
GLOBAL DIRECTION = Y  
CONTROLLED NODE = 3

| OUTPUT<br>ITERATIONS | DISPLACEMENT<br>INCREMENT | VARIABLE<br>LOAD<br>FACTOR | LEVEL | CONV. -NORM |   |
|----------------------|---------------------------|----------------------------|-------|-------------|---|
| 45                   | 0.67338419E+00            | 0.59122201E+00             | 0     | 0.842E-12   | 3 |
| 46                   | 0.67338419E+00            | 0.54930670E+00             | 0     | 0.341E-10   | 3 |
| 47                   | 0.67338419E+00            | 0.50485740E+00             | 0     | 0.297E-08   | 3 |
| 48                   | 0.67338419E+00            | 0.45652421E+00             | 0     | 0.761E-11   | 4 |
| 49                   | 0.13467684E+00            | 0.44621774E+00             | 1     | 0.752E-08   | 2 |
| 50                   | 0.13467684E+00            | 0.43564685E+00             | 1     | 0.145E-07   | 2 |
| 51                   | 0.13467684E+00            | 0.42478342E+00             | 1     | 0.295E-07   | 2 |
| 52                   | 0.13467684E+00            | 0.41359499E+00             | 1     | 0.628E-07   | 2 |
| 53                   | 0.13467684E+00            | 0.40204378E+00             | 1     | 0.141E-06   | 2 |
| 54                   | 0.67338419E+00            | 0.33693690E+00             | 0     | 0.905E-10   | 4 |
| 55                   | 0.13467684E+00            | 0.32186952E+00             | 1     | 0.877E-12   | 3 |
| 56                   | 0.13467684E+00            | 0.30581535E+00             | 1     | 0.382E-08   | 3 |
| 57                   | 0.13467684E+00            | 0.28855344E+00             | 1     | 0.605E-07   | 3 |
| 58                   | 0.13467684E+00            | 0.26977110E+00             | 1     | 0.122E-06   | 3 |
| 59                   | 0.13467684E+00            | 0.24899930E+00             | 1     | 0.141E-06   | 3 |
| 60                   | 0.13467684E+00            | 0.22547457E+00             | 1     | 0.236E-06   | 3 |
| 61                   | 0.13467684E+00            | 0.19778790E+00             | 1     | 0.448E-11   | 4 |
| 62                   | 0.13467684E+00            | 0.16268829E+00             | 1     | 0.454E-07   | 4 |
| 63                   | 0.26935367E-01            | 0.15410827E+00             | 2     | 0.504E-07   | 2 |
| 64                   | 0.26935367E-01            | 0.14468054E+00             | 2     | 0.123E-06   | 2 |
| 65                   | 0.26935367E-01            | 0.13410380E+00             | 2     | 0.381E-06   | 2 |
| 66                   | 0.26935367E-01            | 0.12184021E+00             | 2     | 0.594E-11   | 3 |
| 67                   | 0.26935367E-01            | 0.10672673E+00             | 2     | 0.851E-09   | 3 |
| 68                   | 0.26935367E-01            | 0.84875270E-01             | 2     | 0.245E-09   | 4 |
| 69                   | 0.53870735E-02            | 0.78273464E-01             | 3     | 0.225E-06   | 2 |
| 70                   | 0.53870735E-02            | 0.69112846E-01             | 3     | 0.146E-08   | 3 |

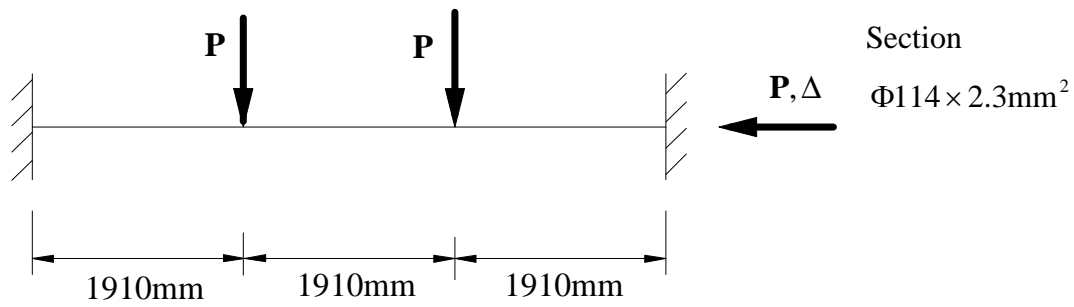
Current control type terminated  
\*\*\*\*\*

PHASE NUMBER = 2  
 NODAL DISPLACEMENT CONTROL  
 GLOBAL DIRECTION = Y  
 CONTROLLED NODE = 2

| OUTPUT<br>ITERATIONS | DISPLACEMENT<br>INCREMENT | VARIABLE<br>LOAD<br>FACTOR | LEVEL | CONV. -NORM |   |
|----------------------|---------------------------|----------------------------|-------|-------------|---|
| 71                   | -.80789915E-01            | 0.57646662E-01             | 0     | 0.884E-08   | 2 |
| 72                   | -.16157983E+00            | 0.36441746E-01             | 0     | 0.848E-06   | 2 |
| 73                   | -.32315966E+00            | -.97531927E-03             | 0     | 0.948E-10   | 3 |
| 74                   | -.32315966E+00            | -.33812188E-01             | 0     | 0.341E-11   | 3 |
| 75                   | -.32315966E+00            | -.63438327E-01             | 0     | 0.972E-12   | 3 |
| 76                   | -.32315966E+00            | -.90632858E-01             | 0     | 0.581E-12   | 3 |
| 77                   | -.32315966E+00            | -.11588821E+00             | 0     | 0.602E-06   | 2 |
| 78                   | -.64631932E+00            | -.16182271E+00             | 0     | 0.508E-10   | 3 |
| 79                   | -.64631932E+00            | -.20296138E+00             | 0     | 0.685E-11   | 3 |
| 80                   | -.64631932E+00            | -.24029833E+00             | 0     | 0.100E-11   | 3 |
| 81                   | -.64631932E+00            | -.27447033E+00             | 0     | 0.390E-12   | 3 |
| 82                   | -.64631932E+00            | -.30591620E+00             | 0     | 0.523E-12   | 3 |
| 83                   | -.64631932E+00            | -.33495588E+00             | 0     | 0.367E-12   | 3 |
| 84                   | -.64631932E+00            | -.36183352E+00             | 0     | 0.935E-06   | 2 |
| 85                   | -.12926386E+01            | -.40984154E+00             | 0     | 0.134E-09   | 3 |
| 86                   | -.12926386E+01            | -.45112304E+00             | 0     | 0.383E-10   | 3 |
| 87                   | -.12926386E+01            | -.48654527E+00             | 0     | 0.124E-10   | 3 |
| 88                   | -.12926386E+01            | -.51679131E+00             | 0     | 0.451E-11   | 3 |
| 89                   | -.12926386E+01            | -.54242477E+00             | 0     | 0.223E-11   | 3 |
| 90                   | -.12926386E+01            | -.56392427E+00             | 0     | 0.639E-12   | 3 |
| 91                   | -.12926386E+01            | -.58170326E+00             | 0     | 0.672E-12   | 3 |
| 92                   | -.12926386E+01            | -.59612224E+00             | 0     | 0.356E-12   | 3 |
| 93                   | -.12926386E+01            | -.60749699E+00             | 0     | 0.447E-12   | 3 |
| 94                   | -.12926386E+01            | -.61610455E+00             | 0     | 0.157E-12   | 3 |
| 95                   | -.12926386E+01            | -.62218784E+00             | 0     | 0.862E-06   | 2 |
| 96                   | -.25852773E+01            | -.62760442E+00             | 0     | 0.252E-09   | 3 |
| 97                   | -.25852773E+01            | -.62513542E+00             | 0     | 0.778E-10   | 3 |
| 98                   | -.25852773E+01            | -.61580883E+00             | 0     | 0.253E-10   | 3 |
| 99                   | -.25852773E+01            | -.60034713E+00             | 0     | 0.873E-11   | 3 |
| 100                  | -.25852773E+01            | -.57920181E+00             | 0     | 0.269E-11   | 3 |
| 101                  | -.25852773E+01            | -.55256728E+00             | 0     | 0.146E-11   | 3 |
| 102                  | -.25852773E+01            | -.52037179E+00             | 0     | 0.457E-12   | 3 |
| 103                  | -.25852773E+01            | -.48223868E+00             | 0     | 0.428E-12   | 3 |
| 104                  | -.25852773E+01            | -.43740453E+00             | 0     | 0.246E-12   | 3 |
| 105                  | -.25852773E+01            | -.38456730E+00             | 0     | 0.637E-12   | 3 |
| 106                  | -.25852773E+01            | -.32161248E+00             | 0     | 0.132E-11   | 3 |
| 107                  | -.25852773E+01            | -.24511144E+00             | 0     | 0.206E-11   | 3 |
| 108                  | -.25852773E+01            | -.14937073E+00             | 0     | 0.499E-11   | 3 |
| 109                  | -.25852773E+01            | -.24547529E-01             | 0     | 0.116E-10   | 3 |
| 110                  | -.25852773E+01            | 0.14728750E+00             | 0     | 0.242E-10   | 3 |
| 111                  | -.25852773E+01            | 0.40093190E+00             | 0     | 0.581E-10   | 3 |
| 112                  | -.25852773E+01            | 0.80974686E+00             | 0     | 0.339E-09   | 3 |
| 113                  | -.25852773E+01            | 0.15494444E+01             | 0     | 0.417E-08   | 3 |
| 114                  | -.25852773E+01            | 0.31338199E+01             | 0     | 0.310E-06   | 3 |

## 9.4 Fixed ended beam-column

The fixed ended beam-column, shown in the figure 9.4, is subjected to two vertical symmetric forces  $P$ , and to an horizontal force. The buckling forces for this frame where obtained using 3 elements.



*figure 9.4 Geometry of fixed ended beam-column.*

## 9.4.1 Data file

```
#
analysis 2d statics \(a\)

#
materials \(b\)

  mat.name      model      properties
  mat1          st12 & # 42 properties for multisurface steel model follow
0.210000e+06  0.100000e-02  0.200000e-02 &
0.600000e-02  0.210000e-01  0.306000e-01 &
0.187850e+03  0.101150e+06  0.260100e+03 &
0.433500e+05  0.289000e+03  0.867000e+04 &
0.306340e+03  0.115600e+04  0.323680e+03 &
0.120417e+04  0.335240e+03  0.104278e+04 &
0.187850e+03  0.101150e+06  0.260100e+03 &
0.433500e+05  0.289000e+03  0.867000e+04 &
0.306340e+03  0.115600e+04  0.323680e+03 &
0.120417e+04  0.335240e+03  0.104278e+04 &
0.000000e+00  0.000000e+00  0.000000e+00 &
0.000000e+00  0.000000e+00  0.000000e+00 &
0.000000e+00  0.000000e+00  0.000000e+00 &
0.000000e+00  0.000000e+00  0.000000e+00 &
sections \(c\)
  type = chs
# circular hollow section
  sec.name      mat.name      dimensions
  sect1        mat1          114.0  2.3
#
patterns \(p\)
# subdivision patterns for elements "qdp2"
  pat.name      ratios
  pat1          1 2 3 4 5      # 5 subelements; smallest near 1st node
  pat2          3 2 1 2 3      # 5 subelements; smallest in the middle
#
groups \(d\)
type = cbp2
  grp.name      sec.name      monitoring.points
  grp1          sect1         40
#
type = qdp2
  grp.name      cbp2.grp.name  pat.name
  grp2          grp1          pat1
  grp3          grp1          pat2
#
structural.nodal \(e\)
  nod.name      x          y
  1              0.0       0.0
  2              1910.0    0.0
  3              3810.0    0.0
  4              5720.0    0.0
#
restraints \(g\)
  nod.name      direction
  1              x+y+rz
  4              y+rz
#
```

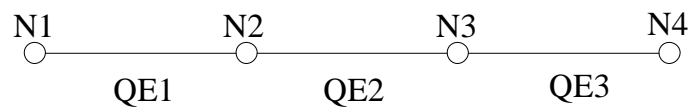
```

element.connectivity (h)

  elm.name   grp.name  nod.name
    1         grp2     1  2
    2         grp3     2  3
    3         grp2     4  3
#
linear.curves # curves for time history loads
start.time = 0.0
crv.name = c1
  time   load.factor
    1     -1.0
    3      1.0
    5     -1.0
#
applied.loading (i)
initial
  nod.name   direction   type   value
  f 2        y           force  -0.1005e+4
  r 1        -           -       0.0      1
time.history
  nod.name   direction   type   crv.name  value
    4         x           disp   c1        40.0
#
equilibrium.stages
  end.of.stage  steps
    5.0         200
# use default iterative strategy
convergence.criteria (l)
  tolerance = 0.1e-5
  force.ref = 0.1e+6
  moment.ref = 0.1e+8
#
output (m)
frequency 0 stress # all equilibrium steps including step reduction
levels
#
end

```

**Note** The following picture shows the names that have been given to the nodes and elements in the data file.



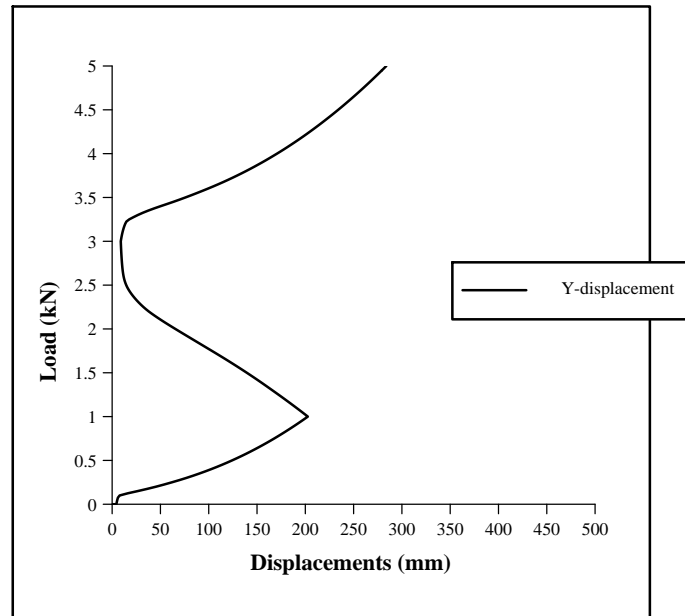
*figure 9.4.1 Nodes and elements of fixed ended beam-column.*



## 9.4.2 Structural behaviour

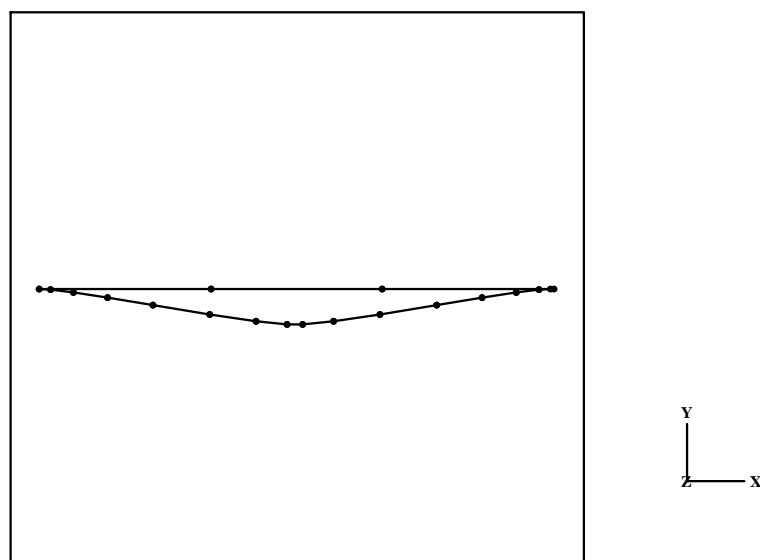
The nonlinear analysis is undertaken using one element per member. The following figures show the static response of fixed ended beam-column.

The nodes 1 and 4, only experiments rotation. The nodes 2 experiments a small displacement in X-axes and a bigger one in the Y-axes, and does not exist any rotation.



*figure 9.4.2b Displacements of fixed ended beam-column.*

The deformed shape that experiments the beam subject at those loads is the following one:



*figure 9.4.2b Deflected Shape of fixed ended beam-column.*

### 9.4.3 Output file

ELEMENT ASSEMBLY ORDER

```
----->>> ----->>> ----->>> ----->>> ----->>> ----->>> ----->>>
1           2           3
```

MAXIMUM FRONT: (NODAL = 3) - (ADDITIONAL FREEDOMS = 0)  
 ++++++

INITIAL LOADING  
 ++++++

| OUTPUT ITERATIONS | INITIAL LOADING FACTOR | CURRENT TIME   | LEVEL | CONV.-NORM |   |
|-------------------|------------------------|----------------|-------|------------|---|
| 1                 | 0.10000000E+01         | 0.00000000E+00 | 0     | 0.303E-07  | 1 |

VARIABLE LOADING  
 ++++++

| OUTPUT | CURRENT TIME   | LEVEL | CONV.-NORM | ITERATIONS |
|--------|----------------|-------|------------|------------|
| 2      | 0.25000000E-01 | 0     | 0.326E-06  | 1          |
| 3      | 0.50000000E-01 | 0     | 0.584E-06  | 1          |
| 4      | 0.75000000E-01 | 0     | 0.155E-12  | 2          |

```
***** ( SUBDIVISION OF ELEMENT 1 )*****
*
*NUMBER OF NODES CREATED
*           3
* NOD.NAME      COORD'S (X,Y) RELATIVE TO END(1) OF SUBDIVIDED ELEMENT
* #n1           0.127333E+03      0.000000E+00
* #n2           0.382000E+03      0.000000E+00
* #n3           0.764000E+03      0.000000E+00
*-----*
*
*NUMBER OF ELEMENTS CREATED
*           4
* ELM.NAME      TYPE.OF.ELEMENT      NOD.NAMES
* #e1           cbp2                 1      #n1
* #e2           cbp2                 #n1    #n2
* #e3           cbp2                 #n2    #n3
* #e4           qdp2                 #n3    2
*-----*
*
*NUMBER OF IMPERFECT ELEMENTS
*           0
*****
```

```
***** ( SUBDIVISION OF ELEMENT 2 )*****
*
*NUMBER OF NODES CREATED
*           4
* NOD.NAME      COORD'S (X,Y) RELATIVE TO END(1) OF SUBDIVIDED ELEMENT
* #n4           0.518182E+03      0.000000E+00
* #n5           0.863636E+03      0.000000E+00
* #n6           0.103636E+04      0.000000E+00
```

```

* #n7                0.138182E+04                0.000000E+00                *
*-----*
*
*NUMBER OF ELEMENTS CREATED                *
*          5                *
* ELM.NAME      TYPE.OF.ELEMENT      NOD.NAMES                *
* #e5            cbp2                2          #n4                *
* #e6            cbp2                #n4          #n5                *
* #e7            cbp2                #n5          #n6                *
* #e8            cbp2                #n6          #n7                *
* #e9            cbp2                #n7          3                *
*-----*
*
*NUMBER OF IMPERFECT ELEMENTS                *
*          0                *
*****

***** ( SUBDIVISION OF ELEMENT 3 )*****
*
*NUMBER OF NODES CREATED                *
*          3                *
* NOD.NAME      COORD'S (X,Y) RELATIVE TO END(1) OF SUBDIVIDED ELEMENT *
* #n8            -.127333E+03          0.000000E+00                *
* #n9            -.382000E+03          0.000000E+00                *
* #n10           -.764000E+03          0.000000E+00                *
*-----*
*
*NUMBER OF ELEMENTS CREATED                *
*          4                *
* ELM.NAME      TYPE.OF.ELEMENT      NOD.NAMES                *
* #e10           cbp2                4          #n8                *
* #e11           cbp2                #n8          #n9                *
* #e12           cbp2                #n9          #n10               *
* #e13           qdp2                #n10         3                *
*-----*
*
*NUMBER OF IMPERFECT ELEMENTS                *
*          0                *
*****

          5          0.10000000E+00          0          0.888E-07          3

***** ( SUBDIVISION OF ELEMENT #e4 )*****
*
*NUMBER OF NODES CREATED                *
*          1                *
* NOD.NAME      COORD'S (X,Y) RELATIVE TO END(1) OF SUBDIVIDED ELEMENT *
* #n11           0.509333E+03          0.000000E+00                *
*-----*
*
*NUMBER OF ELEMENTS CREATED                *
*          2                *
* ELM.NAME      TYPE.OF.ELEMENT      NOD.NAMES                *
* #e14           cbp2                #n3          #n11               *
* #e15           cbp2                #n11         2                *
*-----*
*
*NUMBER OF IMPERFECT ELEMENTS                *
*          0                *
*****

```

```

***** ( SUBDIVISION OF ELEMENT #e13 )*****
*
*NUMBER OF NODES CREATED
* 1
* NOD.NAME          COORD'S (X,Y) RELATIVE TO END(1) OF SUBDIVIDED ELEMENT
* #n12              -.509333E+03          0.000000E+00
*-----*
*
*NUMBER OF ELEMENTS CREATED
* 2
* ELM.NAME          TYPE.OF.ELEMENT          NOD.NAMES
* #e16              cbp2                    #n10      #n12
* #e17              cbp2                    #n12      3
*-----*
*
*NUMBER OF IMPERFECT ELEMENTS
* 0
*****

```

|    |                |   |           |   |
|----|----------------|---|-----------|---|
| 6  | 0.12500000E+00 | 0 | 0.665E-07 | 3 |
| 7  | 0.15000000E+00 | 0 | 0.219E-06 | 2 |
| 8  | 0.17500000E+00 | 0 | 0.437E-06 | 2 |
| 9  | 0.20000000E+00 | 0 | 0.195E-06 | 2 |
| 10 | 0.22500000E+00 | 0 | 0.177E-06 | 2 |
| 11 | 0.25000000E+00 | 0 | 0.161E-06 | 2 |
| 12 | 0.27500000E+00 | 0 | 0.116E-06 | 2 |
| 13 | 0.30000000E+00 | 0 | 0.349E-07 | 2 |
| 14 | 0.32500000E+00 | 0 | 0.208E-08 | 3 |
| 15 | 0.35000000E+00 | 0 | 0.206E-09 | 3 |
| 16 | 0.37500000E+00 | 0 | 0.233E-08 | 3 |
| 17 | 0.40000000E+00 | 0 | 0.508E-07 | 2 |
| 18 | 0.42500000E+00 | 0 | 0.411E-07 | 2 |
| 19 | 0.45000000E+00 | 0 | 0.731E-07 | 2 |
| 20 | 0.47500000E+00 | 0 | 0.574E-07 | 2 |
| 21 | 0.50000000E+00 | 0 | 0.254E-07 | 2 |
| 22 | 0.52500000E+00 | 0 | 0.410E-07 | 2 |
| 23 | 0.55000000E+00 | 0 | 0.841E-07 | 2 |
| 24 | 0.57500000E+00 | 0 | 0.355E-09 | 3 |
| 25 | 0.60000000E+00 | 0 | 0.478E-07 | 2 |
| 26 | 0.62500000E+00 | 0 | 0.103E-06 | 2 |
| 27 | 0.65000000E+00 | 0 | 0.138E-08 | 3 |
| 28 | 0.67500000E+00 | 0 | 0.157E-09 | 3 |
| 29 | 0.70000000E+00 | 0 | 0.481E-07 | 2 |
| 30 | 0.72500000E+00 | 0 | 0.342E-07 | 2 |
| 31 | 0.75000000E+00 | 0 | 0.191E-07 | 2 |
| 32 | 0.77500000E+00 | 0 | 0.186E-07 | 2 |
| 33 | 0.80000000E+00 | 0 | 0.183E-07 | 2 |
| 34 | 0.82500000E+00 | 0 | 0.575E-09 | 3 |
| 35 | 0.85000000E+00 | 0 | 0.173E-07 | 2 |
| 36 | 0.87500000E+00 | 0 | 0.128E-07 | 2 |
| 37 | 0.90000000E+00 | 0 | 0.133E-07 | 2 |
| 38 | 0.92500000E+00 | 0 | 0.242E-07 | 2 |
| 39 | 0.95000000E+00 | 0 | 0.425E-09 | 3 |
| 40 | 0.97500000E+00 | 0 | 0.186E-09 | 3 |
| 41 | 0.10000000E+01 | 0 | 0.263E-09 | 3 |
| 42 | 0.10250000E+01 | 0 | 0.312E-08 | 2 |
| 43 | 0.10500000E+01 | 0 | 0.829E-07 | 1 |
| 44 | 0.10750000E+01 | 0 | 0.828E-07 | 1 |
| 45 | 0.11000000E+01 | 0 | 0.822E-07 | 1 |

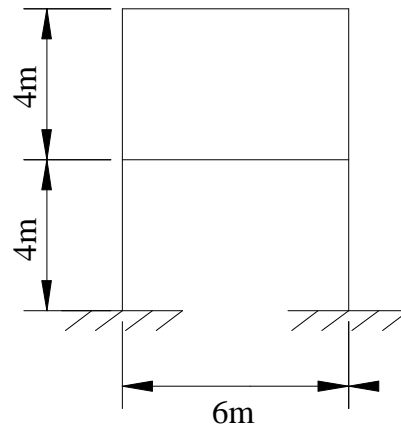
|     |                |   |           |   |
|-----|----------------|---|-----------|---|
| 46  | 0.11250000E+01 | 0 | 0.811E-07 | 1 |
| 47  | 0.11500000E+01 | 0 | 0.795E-07 | 1 |
| 48  | 0.11750000E+01 | 0 | 0.772E-07 | 1 |
| 49  | 0.12000000E+01 | 0 | 0.743E-07 | 1 |
| 50  | 0.12250000E+01 | 0 | 0.706E-07 | 1 |
| 51  | 0.12500000E+01 | 0 | 0.692E-07 | 1 |
| 52  | 0.12750000E+01 | 0 | 0.277E-06 | 2 |
| 53  | 0.13000000E+01 | 0 | 0.250E-08 | 2 |
| 54  | 0.13250000E+01 | 0 | 0.394E-07 | 2 |
| 55  | 0.13500000E+01 | 0 | 0.102E-08 | 2 |
| 56  | 0.13750000E+01 | 0 | 0.829E-08 | 2 |
| 57  | 0.14000000E+01 | 0 | 0.215E-07 | 2 |
| 58  | 0.14250000E+01 | 0 | 0.139E-07 | 2 |
| 59  | 0.14500000E+01 | 0 | 0.226E-07 | 2 |
| 60  | 0.14750000E+01 | 0 | 0.398E-07 | 2 |
| 61  | 0.15000000E+01 | 0 | 0.120E-06 | 2 |
| 62  | 0.15250000E+01 | 0 | 0.179E-06 | 2 |
| 63  | 0.15500000E+01 | 0 | 0.105E-06 | 2 |
| 64  | 0.15750000E+01 | 0 | 0.634E-07 | 2 |
| 65  | 0.16000000E+01 | 0 | 0.234E-07 | 2 |
| 66  | 0.16250000E+01 | 0 | 0.314E-07 | 2 |
| 67  | 0.16500000E+01 | 0 | 0.202E-07 | 2 |
| 68  | 0.16750000E+01 | 0 | 0.932E-07 | 2 |
| 69  | 0.17000000E+01 | 0 | 0.182E-07 | 2 |
| 70  | 0.17250000E+01 | 0 | 0.343E-07 | 2 |
| 71  | 0.17500000E+01 | 0 | 0.450E-07 | 2 |
| 72  | 0.17750000E+01 | 0 | 0.322E-06 | 2 |
| 73  | 0.18000000E+01 | 0 | 0.359E-06 | 2 |
| 74  | 0.18250000E+01 | 0 | 0.231E-07 | 2 |
| 75  | 0.18500000E+01 | 0 | 0.204E-06 | 2 |
| 76  | 0.18750000E+01 | 0 | 0.411E-06 | 2 |
| 77  | 0.19000000E+01 | 0 | 0.124E-08 | 3 |
| 78  | 0.19250000E+01 | 0 | 0.160E-07 | 2 |
| 79  | 0.19500000E+01 | 0 | 0.516E-06 | 2 |
| 80  | 0.19750000E+01 | 0 | 0.515E-06 | 2 |
| 81  | 0.20000000E+01 | 0 | 0.174E-07 | 2 |
| 82  | 0.20250000E+01 | 0 | 0.357E-07 | 2 |
| 83  | 0.20500000E+01 | 0 | 0.145E-06 | 2 |
| 84  | 0.20750000E+01 | 0 | 0.232E-07 | 2 |
| 85  | 0.21000000E+01 | 0 | 0.532E-08 | 2 |
| 86  | 0.21250000E+01 | 0 | 0.615E-08 | 2 |
| 87  | 0.21500000E+01 | 0 | 0.134E-07 | 2 |
| 88  | 0.21750000E+01 | 0 | 0.358E-08 | 2 |
| 89  | 0.22000000E+01 | 0 | 0.134E-06 | 2 |
| 90  | 0.22250000E+01 | 0 | 0.179E-07 | 2 |
| 91  | 0.22500000E+01 | 0 | 0.372E-07 | 2 |
| 92  | 0.22750000E+01 | 0 | 0.591E-06 | 2 |
| 93  | 0.23000000E+01 | 0 | 0.411E-08 | 2 |
| 94  | 0.23250000E+01 | 0 | 0.491E-07 | 2 |
| 95  | 0.23500000E+01 | 0 | 0.557E-08 | 2 |
| 96  | 0.23750000E+01 | 0 | 0.616E-08 | 2 |
| 97  | 0.24000000E+01 | 0 | 0.508E-08 | 2 |
| 98  | 0.24250000E+01 | 0 | 0.721E-08 | 2 |
| 99  | 0.24500000E+01 | 0 | 0.134E-07 | 2 |
| 100 | 0.24750000E+01 | 0 | 0.487E-06 | 2 |
| 101 | 0.25000000E+01 | 0 | 0.224E-06 | 2 |
| 102 | 0.25250000E+01 | 0 | 0.788E-07 | 2 |
| 103 | 0.25500000E+01 | 0 | 0.223E-07 | 2 |
| 104 | 0.25750000E+01 | 0 | 0.320E-07 | 2 |
| 105 | 0.26000000E+01 | 0 | 0.467E-07 | 2 |
| 106 | 0.26250000E+01 | 0 | 0.382E-07 | 2 |

|     |                |   |           |   |
|-----|----------------|---|-----------|---|
| 107 | 0.26500000E+01 | 0 | 0.483E-08 | 2 |
| 108 | 0.26750000E+01 | 0 | 0.480E-08 | 2 |
| 109 | 0.27000000E+01 | 0 | 0.457E-08 | 2 |
| 110 | 0.27250000E+01 | 0 | 0.349E-08 | 2 |
| 111 | 0.27500000E+01 | 0 | 0.184E-08 | 2 |
| 112 | 0.27750000E+01 | 0 | 0.934E-06 | 1 |
| 113 | 0.28000000E+01 | 0 | 0.542E-06 | 1 |
| 114 | 0.28250000E+01 | 0 | 0.380E-06 | 1 |
| 115 | 0.28500000E+01 | 0 | 0.542E-06 | 1 |
| 116 | 0.28750000E+01 | 0 | 0.900E-06 | 1 |
| 117 | 0.29000000E+01 | 0 | 0.261E-08 | 2 |
| 118 | 0.29250000E+01 | 0 | 0.299E-08 | 2 |
| 119 | 0.29500000E+01 | 0 | 0.249E-08 | 2 |
| 120 | 0.29750000E+01 | 0 | 0.872E-06 | 1 |
| 121 | 0.30000000E+01 | 0 | 0.512E-06 | 1 |
| 122 | 0.30250000E+01 | 0 | 0.629E-09 | 2 |
| 123 | 0.30500000E+01 | 0 | 0.215E-06 | 1 |
| 124 | 0.30750000E+01 | 0 | 0.303E-06 | 1 |
| 125 | 0.31000000E+01 | 0 | 0.437E-06 | 1 |
| 126 | 0.31250000E+01 | 0 | 0.642E-06 | 1 |
| 127 | 0.31500000E+01 | 0 | 0.967E-06 | 1 |
| 128 | 0.31750000E+01 | 0 | 0.126E-11 | 2 |
| 129 | 0.32000000E+01 | 0 | 0.114E-11 | 2 |
| 130 | 0.32250000E+01 | 0 | 0.173E-08 | 3 |
| 131 | 0.32500000E+01 | 0 | 0.813E-08 | 3 |
| 132 | 0.32750000E+01 | 0 | 0.129E-06 | 3 |
| 133 | 0.33000000E+01 | 0 | 0.670E-07 | 2 |
| 134 | 0.33250000E+01 | 0 | 0.438E-07 | 2 |
| 135 | 0.33500000E+01 | 0 | 0.108E-06 | 2 |
| 136 | 0.33750000E+01 | 0 | 0.344E-06 | 2 |
| 137 | 0.34000000E+01 | 0 | 0.216E-06 | 2 |
| 138 | 0.34250000E+01 | 0 | 0.289E-06 | 2 |
| 139 | 0.34500000E+01 | 0 | 0.232E-06 | 2 |
| 140 | 0.34750000E+01 | 0 | 0.135E-08 | 3 |
| 141 | 0.35000000E+01 | 0 | 0.126E-07 | 3 |
| 142 | 0.35250000E+01 | 0 | 0.888E-07 | 2 |
| 143 | 0.35500000E+01 | 0 | 0.649E-07 | 2 |
| 144 | 0.35750000E+01 | 0 | 0.300E-06 | 2 |
| 145 | 0.36000000E+01 | 0 | 0.357E-06 | 2 |
| 146 | 0.36250000E+01 | 0 | 0.264E-08 | 3 |
| 147 | 0.36500000E+01 | 0 | 0.194E-08 | 3 |
| 148 | 0.36750000E+01 | 0 | 0.214E-09 | 3 |
| 149 | 0.37000000E+01 | 0 | 0.420E-06 | 2 |
| 150 | 0.37250000E+01 | 0 | 0.760E-07 | 2 |
| 151 | 0.37500000E+01 | 0 | 0.408E-07 | 2 |
| 152 | 0.37750000E+01 | 0 | 0.200E-06 | 2 |
| 153 | 0.38000000E+01 | 0 | 0.268E-08 | 3 |
| 154 | 0.38250000E+01 | 0 | 0.162E-09 | 3 |
| 155 | 0.38500000E+01 | 0 | 0.202E-09 | 3 |
| 156 | 0.38750000E+01 | 0 | 0.139E-09 | 3 |
| 157 | 0.39000000E+01 | 0 | 0.126E-10 | 3 |
| 158 | 0.39250000E+01 | 0 | 0.110E-10 | 3 |
| 159 | 0.39500000E+01 | 0 | 0.614E-09 | 2 |
| 160 | 0.39750000E+01 | 0 | 0.307E-09 | 2 |
| 161 | 0.40000000E+01 | 0 | 0.225E-06 | 2 |
| 162 | 0.40250000E+01 | 0 | 0.973E-08 | 2 |
| 163 | 0.40500000E+01 | 0 | 0.653E-06 | 2 |
| 164 | 0.40750000E+01 | 0 | 0.920E-06 | 2 |
| 165 | 0.41000000E+01 | 0 | 0.256E-09 | 2 |
| 166 | 0.41250000E+01 | 0 | 0.154E-09 | 2 |
| 167 | 0.41500000E+01 | 0 | 0.113E-08 | 2 |

|     |                |   |           |   |
|-----|----------------|---|-----------|---|
| 168 | 0.41750000E+01 | 0 | 0.343E-08 | 2 |
| 169 | 0.42000000E+01 | 0 | 0.348E-09 | 2 |
| 170 | 0.42250000E+01 | 0 | 0.410E-08 | 2 |
| 171 | 0.42500000E+01 | 0 | 0.139E-08 | 2 |
| 172 | 0.42750000E+01 | 0 | 0.102E-07 | 2 |
| 173 | 0.43000000E+01 | 0 | 0.602E-10 | 3 |
| 174 | 0.43250000E+01 | 0 | 0.174E-08 | 2 |
| 175 | 0.43500000E+01 | 0 | 0.148E-06 | 2 |
| 176 | 0.43750000E+01 | 0 | 0.331E-08 | 2 |
| 177 | 0.44000000E+01 | 0 | 0.256E-08 | 2 |
| 178 | 0.44250000E+01 | 0 | 0.971E-10 | 3 |
| 179 | 0.44500000E+01 | 0 | 0.592E-09 | 2 |
| 180 | 0.44750000E+01 | 0 | 0.194E-09 | 2 |
| 181 | 0.45000000E+01 | 0 | 0.930E-09 | 2 |
| 182 | 0.45250000E+01 | 0 | 0.924E-09 | 2 |
| 183 | 0.45500000E+01 | 0 | 0.946E-09 | 2 |
| 184 | 0.45750000E+01 | 0 | 0.320E-10 | 3 |
| 185 | 0.46000000E+01 | 0 | 0.104E-08 | 2 |
| 186 | 0.46250000E+01 | 0 | 0.999E-09 | 2 |
| 187 | 0.46500000E+01 | 0 | 0.332E-08 | 2 |
| 188 | 0.46750000E+01 | 0 | 0.582E-09 | 2 |
| 189 | 0.47000000E+01 | 0 | 0.398E-10 | 2 |
| 190 | 0.47250000E+01 | 0 | 0.430E-10 | 2 |
| 191 | 0.47500000E+01 | 0 | 0.175E-09 | 2 |
| 192 | 0.47750000E+01 | 0 | 0.142E-09 | 2 |
| 193 | 0.48000000E+01 | 0 | 0.729E-10 | 2 |
| 194 | 0.48250000E+01 | 0 | 0.107E-09 | 2 |
| 195 | 0.48500000E+01 | 0 | 0.164E-09 | 2 |
| 196 | 0.48750000E+01 | 0 | 0.208E-09 | 2 |
| 197 | 0.49000000E+01 | 0 | 0.130E-08 | 2 |
| 198 | 0.49250000E+01 | 0 | 0.676E-10 | 3 |
| 199 | 0.49500000E+01 | 0 | 0.486E-09 | 2 |
| 200 | 0.49750000E+01 | 0 | 0.543E-09 | 2 |
| 201 | 0.50000000E+01 | 0 | 0.137E-09 | 2 |

## 9.5 Two-storey

This example illustrates the influence of an earthquake on the resistance of steel frames.



*figure 9.5 Steel frames subject to earthquake.*



## 9.5.1 Data file

```
#
analysis 2d dynamics \(a\)
#
materials \(b\)
  mat.name      model      properties
  mat1          st11        0.210e12 0.300e9 0.100e-1
#
sections \(c\)
  type = rss
  sec.name      mat.name      dimensions
  sect1         mat1          0.10 0.10
#
patterns \(p\)
  pat.name      ratios
  pat1          1 2 3 3 2 1
#
groups \(d\)
type = cbp2
  grp.name      sec.name      monitoring.points
  grp1          sect1         30

type = qdp2
  grp.name      cbp2.grp.name  pat.name
  grp2          grp1          pat1

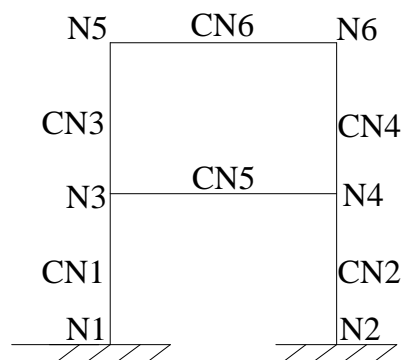
type = cnm2
  grp.name      mass
  grp3          20000
#
structural \(e\)
  nod.n      x      y
  f 1        0.0    0.0
  r 1        6.0    0.0 1
  r 2        0.0    4.0 2
#
restraints \(f\)
  direction = y+rz
  nod.name
  1
  2
#
element.connectivity \(g\)
  grp.name = grp2
  elm.name      nod.name
  f 1           1 3
  r 1           1 1 1
  r 2           2 2 1
  5            3 4
  6            5 6
  grp.name = grp3
  elm.name      nod.name
  f 10          3
  r 1           1 3
#
integration \(r\)
scheme = newmark
beta = 0.25
gamma = 0.5
```

```

#
linear.curves \(q\)
start.time = 0.0
crv.name = crv1
file      = earthquake1
first.line = 1
last.line  = 1200
format    = (23x,2(e15.8,2x))
#
equilibrium.stages \(s\)
    end.of.stage      steps
    5                  500
#
applied.loading \(i\)
dynamic
    nod.name      direction      type      crv.name      value
    f 1           x              acceleration crv1          9.81
    r 1           -              -         -           0 1
#
iterative.strategy \(k\)
number = 10
initial.reformations = 7
step.reduction = 10
divergence.iteration = 7
maximum.convergence = 1.0
#
convergence.criteria \(l\)
    tolerance = 0.1e-3
    displacement.ref = 1.0
    rotation.ref = 1.0
#
output \(m\)
frequency 2
#
end

```

**Note** The following picture shows the names that have been given to the nodes and elements in the data file.

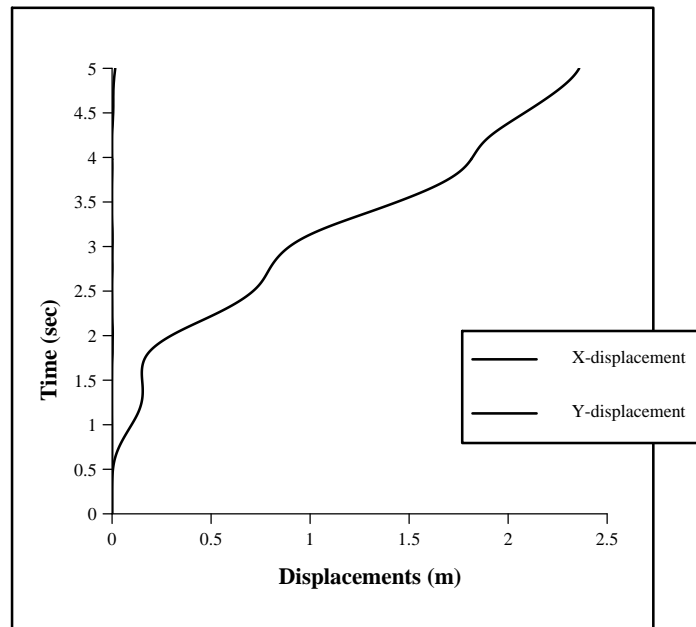


*figure 9.5.1 Nodes and elements of the two-storey.*

## 9.5.2 Structural behaviour

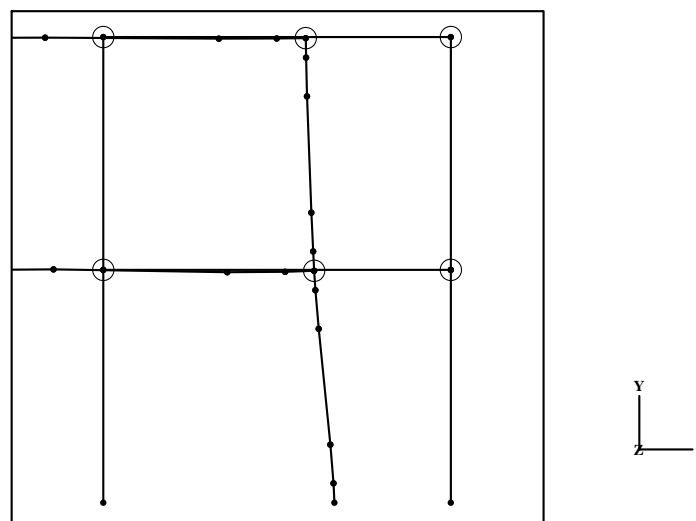
The nonlinear analysis is undertaken using one element per member. The following figures show the dynamic response of the structure.

The displacements of the node 121 at the Y-axes are almost nonexistent compare into the ones at the X-axes, which vary with the time.



*figure 9.5.2b Displacements of two-storey.*

The deformed shape given by ADAPTIC is the one shown in the figure, where could be seen that the main effect of the earthquake is a translation of the structure.



*figure 9.5.2b Deflected Shape of two-storey.*

### 9.5.3 Output file

```

ELEMENT ASSEMBLY ORDER
----->>> ----->>> ----->>> ----->>> ----->>> ----->>> ----->>>
1         3         5         10        6         12         4         13
2         11

```

```

MAXIMUM FRONT: (NODAL = 4) - (ADDITIONAL FREEDOMS = 0)
+++++

```

```

VARIABLE LOADING
+++++

```

| OUTPUT | CURRENT TIME   | LEVEL | CONV.-NORM | ITERATIONS |
|--------|----------------|-------|------------|------------|
| 0      | 0.10000000E-01 | 0     | 0.147E-06  | 0          |
| 1      | 0.20000000E-01 | 0     | 0.736E-06  | 0          |
| 0      | 0.30000000E-01 | 0     | 0.190E-05  | 0          |
| 2      | 0.40000000E-01 | 0     | 0.362E-05  | 0          |
| 0      | 0.50000000E-01 | 0     | 0.516E-05  | 0          |
| 3      | 0.60000000E-01 | 0     | 0.511E-05  | 0          |
| 0      | 0.70000000E-01 | 0     | 0.128E-05  | 0          |
| 4      | 0.80000000E-01 | 0     | 0.932E-05  | 0          |
| 0      | 0.90000000E-01 | 0     | 0.261E-04  | 0          |
| 5      | 0.10000000E+00 | 0     | 0.449E-04  | 0          |
| 0      | 0.11000000E+00 | 0     | 0.622E-04  | 0          |
| 6      | 0.12000000E+00 | 0     | 0.750E-04  | 0          |
| 0      | 0.13000000E+00 | 0     | 0.795E-04  | 0          |
| 7      | 0.14000000E+00 | 0     | 0.716E-04  | 0          |
| 0      | 0.15000000E+00 | 0     | 0.485E-04  | 0          |
| 8      | 0.16000000E+00 | 0     | 0.884E-05  | 0          |
| 0      | 0.17000000E+00 | 0     | 0.509E-04  | 0          |
| 9      | 0.18000000E+00 | 0     | 0.860E-09  | 1          |
| 0      | 0.19000000E+00 | 0     | 0.266E-08  | 1          |
| 10     | 0.20000000E+00 | 0     | 0.556E-08  | 1          |
| 0      | 0.21000000E+00 | 0     | 0.895E-08  | 1          |
| 11     | 0.22000000E+00 | 0     | 0.116E-07  | 1          |
| 0      | 0.23000000E+00 | 0     | 0.132E-07  | 1          |
| 12     | 0.24000000E+00 | 0     | 0.149E-07  | 1          |
| 0      | 0.25000000E+00 | 0     | 0.168E-07  | 1          |
| 13     | 0.26000000E+00 | 0     | 0.178E-07  | 1          |
| 0      | 0.27000000E+00 | 0     | 0.177E-07  | 1          |
| 14     | 0.28000000E+00 | 0     | 0.173E-07  | 1          |
| 0      | 0.29000000E+00 | 0     | 0.171E-07  | 1          |
| 15     | 0.30000000E+00 | 0     | 0.166E-07  | 1          |
| 0      | 0.31000000E+00 | 0     | 0.160E-07  | 1          |
| 16     | 0.32000000E+00 | 0     | 0.159E-07  | 1          |
| 0      | 0.33000000E+00 | 0     | 0.170E-07  | 1          |
| 17     | 0.34000000E+00 | 0     | 0.199E-07  | 1          |
| 0      | 0.35000000E+00 | 0     | 0.248E-07  | 1          |
| 18     | 0.36000000E+00 | 0     | 0.312E-07  | 1          |
| 0      | 0.37000000E+00 | 0     | 0.383E-07  | 1          |
| 19     | 0.38000000E+00 | 0     | 0.450E-07  | 1          |
| 0      | 0.39000000E+00 | 0     | 0.508E-07  | 1          |
| 20     | 0.40000000E+00 | 0     | 0.565E-07  | 1          |
| 0      | 0.41000000E+00 | 0     | 0.631E-07  | 1          |
| 21     | 0.42000000E+00 | 0     | 0.722E-07  | 1          |
| 0      | 0.43000000E+00 | 0     | 0.840E-07  | 1          |
| 22     | 0.44000000E+00 | 0     | 0.971E-07  | 1          |
| 0      | 0.45000000E+00 | 0     | 0.112E-06  | 1          |

|    |                |   |           |   |
|----|----------------|---|-----------|---|
| 23 | 0.46000000E+00 | 0 | 0.132E-06 | 1 |
| 0  | 0.47000000E+00 | 0 | 0.158E-06 | 1 |
| 24 | 0.48000000E+00 | 0 | 0.190E-06 | 1 |
| 0  | 0.49000000E+00 | 0 | 0.222E-06 | 1 |
| 25 | 0.50000000E+00 | 0 | 0.245E-06 | 1 |
| 0  | 0.51000000E+00 | 0 | 0.252E-06 | 1 |
| 26 | 0.52000000E+00 | 0 | 0.245E-06 | 1 |
| 0  | 0.53000000E+00 | 0 | 0.227E-06 | 1 |
| 27 | 0.54000000E+00 | 0 | 0.208E-06 | 1 |
| 0  | 0.55000000E+00 | 0 | 0.191E-06 | 1 |
| 28 | 0.56000000E+00 | 0 | 0.177E-06 | 1 |
| 0  | 0.57000000E+00 | 0 | 0.164E-06 | 1 |
| 29 | 0.58000000E+00 | 0 | 0.146E-06 | 1 |
| 0  | 0.59000000E+00 | 0 | 0.123E-06 | 1 |
| 30 | 0.60000000E+00 | 0 | 0.110E-06 | 1 |
| 0  | 0.61000000E+00 | 0 | 0.109E-06 | 1 |
| 31 | 0.62000000E+00 | 0 | 0.110E-06 | 1 |
| 0  | 0.63000000E+00 | 0 | 0.115E-06 | 1 |
| 32 | 0.64000000E+00 | 0 | 0.122E-06 | 1 |
| 0  | 0.65000000E+00 | 0 | 0.129E-06 | 1 |
| 33 | 0.66000000E+00 | 0 | 0.132E-06 | 1 |
| 0  | 0.67000000E+00 | 0 | 0.134E-06 | 1 |
| 34 | 0.68000000E+00 | 0 | 0.137E-06 | 1 |
| 0  | 0.69000000E+00 | 0 | 0.142E-06 | 1 |
| 35 | 0.70000000E+00 | 0 | 0.157E-06 | 1 |
| 0  | 0.71000000E+00 | 0 | 0.171E-06 | 1 |
| 36 | 0.72000000E+00 | 0 | 0.171E-06 | 1 |
| 0  | 0.73000000E+00 | 0 | 0.182E-06 | 1 |
| 37 | 0.74000000E+00 | 0 | 0.193E-06 | 1 |
| 0  | 0.75000000E+00 | 0 | 0.204E-06 | 1 |
| 38 | 0.76000000E+00 | 0 | 0.213E-06 | 1 |
| 0  | 0.77000000E+00 | 0 | 0.224E-06 | 1 |
| 39 | 0.78000000E+00 | 0 | 0.226E-06 | 1 |
| 0  | 0.79000000E+00 | 0 | 0.232E-06 | 1 |
| 40 | 0.80000000E+00 | 0 | 0.239E-06 | 1 |
| 0  | 0.81000000E+00 | 0 | 0.247E-06 | 1 |
| 41 | 0.82000000E+00 | 0 | 0.253E-06 | 1 |
| 0  | 0.83000000E+00 | 0 | 0.266E-06 | 1 |
| 42 | 0.84000000E+00 | 0 | 0.275E-06 | 1 |
| 0  | 0.85000000E+00 | 0 | 0.261E-06 | 1 |
| 43 | 0.86000000E+00 | 0 | 0.262E-06 | 1 |
| 0  | 0.87000000E+00 | 0 | 0.262E-06 | 1 |
| 44 | 0.88000000E+00 | 0 | 0.262E-06 | 1 |
| 0  | 0.89000000E+00 | 0 | 0.260E-06 | 1 |
| 45 | 0.90000000E+00 | 0 | 0.276E-06 | 1 |
| 0  | 0.91000000E+00 | 0 | 0.278E-06 | 1 |
| 46 | 0.92000000E+00 | 0 | 0.261E-06 | 1 |
| 0  | 0.93000000E+00 | 0 | 0.257E-06 | 1 |
| 47 | 0.94000000E+00 | 0 | 0.254E-06 | 1 |
| 0  | 0.95000000E+00 | 0 | 0.248E-06 | 1 |
| 48 | 0.96000000E+00 | 0 | 0.239E-06 | 1 |
| 0  | 0.97000000E+00 | 0 | 0.230E-06 | 1 |
| 49 | 0.98000000E+00 | 0 | 0.217E-06 | 1 |
| 0  | 0.99000000E+00 | 0 | 0.205E-06 | 1 |
| 50 | 0.10000000E+01 | 0 | 0.199E-06 | 1 |
| 0  | 0.10100000E+01 | 0 | 0.200E-06 | 1 |
| 51 | 0.10200000E+01 | 0 | 0.212E-06 | 1 |
| 0  | 0.10300000E+01 | 0 | 0.224E-06 | 1 |
| 52 | 0.10400000E+01 | 0 | 0.243E-06 | 1 |
| 0  | 0.10500000E+01 | 0 | 0.258E-06 | 1 |
| 53 | 0.10600000E+01 | 0 | 0.306E-06 | 1 |

|    |                |   |           |   |
|----|----------------|---|-----------|---|
| 0  | 0.10700000E+01 | 0 | 0.354E-06 | 1 |
| 54 | 0.10800000E+01 | 0 | 0.371E-06 | 1 |
| 0  | 0.10900000E+01 | 0 | 0.330E-06 | 1 |
| 55 | 0.11000000E+01 | 0 | 0.276E-06 | 1 |
| 0  | 0.11100000E+01 | 0 | 0.209E-06 | 1 |
| 56 | 0.11200000E+01 | 0 | 0.149E-06 | 1 |
| 0  | 0.11300000E+01 | 0 | 0.104E-06 | 1 |
| 57 | 0.11400000E+01 | 0 | 0.809E-07 | 1 |
| 0  | 0.11500000E+01 | 0 | 0.627E-07 | 1 |
| 58 | 0.11600000E+01 | 0 | 0.381E-07 | 1 |
| 0  | 0.11700000E+01 | 0 | 0.260E-07 | 1 |
| 59 | 0.11800000E+01 | 0 | 0.240E-07 | 1 |
| 0  | 0.11900000E+01 | 0 | 0.266E-07 | 1 |
| 60 | 0.12000000E+01 | 0 | 0.544E-07 | 1 |
| 0  | 0.12100000E+01 | 0 | 0.898E-07 | 1 |
| 61 | 0.12200000E+01 | 0 | 0.973E-07 | 1 |
| 0  | 0.12300000E+01 | 0 | 0.799E-07 | 1 |
| 62 | 0.12400000E+01 | 0 | 0.989E-07 | 1 |
| 0  | 0.12500000E+01 | 0 | 0.116E-06 | 1 |
| 63 | 0.12600000E+01 | 0 | 0.132E-06 | 1 |
| 0  | 0.12700000E+01 | 0 | 0.149E-06 | 1 |
| 64 | 0.12800000E+01 | 0 | 0.172E-06 | 1 |
| 0  | 0.12900000E+01 | 0 | 0.200E-06 | 1 |
| 65 | 0.13000000E+01 | 0 | 0.234E-06 | 1 |
| 0  | 0.13100000E+01 | 0 | 0.269E-06 | 1 |
| 66 | 0.13200000E+01 | 0 | 0.303E-06 | 1 |
| 0  | 0.13300000E+01 | 0 | 0.334E-06 | 1 |
| 67 | 0.13400000E+01 | 0 | 0.366E-06 | 1 |
| 0  | 0.13500000E+01 | 0 | 0.398E-06 | 1 |
| 68 | 0.13600000E+01 | 0 | 0.430E-06 | 1 |
| 0  | 0.13700000E+01 | 0 | 0.462E-06 | 1 |
| 69 | 0.13800000E+01 | 0 | 0.495E-06 | 1 |
| 0  | 0.13900000E+01 | 0 | 0.530E-06 | 1 |
| 70 | 0.14000000E+01 | 0 | 0.564E-06 | 1 |
| 0  | 0.14100000E+01 | 0 | 0.594E-06 | 1 |
| 71 | 0.14200000E+01 | 0 | 0.620E-06 | 1 |
| 0  | 0.14300000E+01 | 0 | 0.647E-06 | 1 |
| 72 | 0.14400000E+01 | 0 | 0.685E-06 | 1 |
| 0  | 0.14500000E+01 | 0 | 0.732E-06 | 1 |
| 73 | 0.14600000E+01 | 0 | 0.788E-06 | 1 |
| 0  | 0.14700000E+01 | 0 | 0.845E-06 | 1 |
| 74 | 0.14800000E+01 | 0 | 0.901E-06 | 1 |
| 0  | 0.14900000E+01 | 0 | 0.948E-06 | 1 |
| 75 | 0.15000000E+01 | 0 | 0.974E-06 | 1 |
| 0  | 0.15100000E+01 | 0 | 0.971E-06 | 1 |
| 76 | 0.15200000E+01 | 0 | 0.941E-06 | 1 |
| 0  | 0.15300000E+01 | 0 | 0.894E-06 | 1 |
| 77 | 0.15400000E+01 | 0 | 0.849E-06 | 1 |
| 0  | 0.15500000E+01 | 0 | 0.810E-06 | 1 |
| 78 | 0.15600000E+01 | 0 | 0.777E-06 | 1 |
| 0  | 0.15700000E+01 | 0 | 0.745E-06 | 1 |
| 79 | 0.15800000E+01 | 0 | 0.709E-06 | 1 |
| 0  | 0.15900000E+01 | 0 | 0.671E-06 | 1 |
| 80 | 0.16000000E+01 | 0 | 0.636E-06 | 1 |
| 0  | 0.16100000E+01 | 0 | 0.606E-06 | 1 |
| 81 | 0.16200000E+01 | 0 | 0.581E-06 | 1 |
| 0  | 0.16300000E+01 | 0 | 0.562E-06 | 1 |
| 82 | 0.16400000E+01 | 0 | 0.548E-06 | 1 |
| 0  | 0.16500000E+01 | 0 | 0.540E-06 | 1 |
| 83 | 0.16600000E+01 | 0 | 0.548E-06 | 1 |
| 0  | 0.16700000E+01 | 0 | 0.577E-06 | 1 |

|    |                |   |           |   |
|----|----------------|---|-----------|---|
| 84 | 0.16800000E+01 | 0 | 0.621E-06 | 1 |
| 0  | 0.16900000E+01 | 0 | 0.793E-06 | 1 |
| 85 | 0.17000000E+01 | 0 | 0.105E-05 | 1 |
| 0  | 0.17100000E+01 | 0 | 0.130E-05 | 1 |
| 86 | 0.17200000E+01 | 0 | 0.147E-05 | 1 |

```

***** ( SUBDIVISION OF ELEMENT 1 ) *****
*
*NUMBER OF NODES CREATED
*      1
* NOD.NAME      COORD'S (X,Y) RELATIVE TO END(1) OF SUBDIVIDED ELEMENT
* #n1           0.000000E+00           0.333333E+00
*-----*
*
*NUMBER OF ELEMENTS CREATED
*      2
* ELM.NAME      TYPE.OF.ELEMENT      NOD.NAMES
* #e1           cbp2                 1      #n1
* #e2           qdp2                 #n1     3
*-----*
*
*NUMBER OF IMPERFECT ELEMENTS
*      0
*****

```

```

***** ( SUBDIVISION OF ELEMENT 2 ) *****
*
*NUMBER OF NODES CREATED
*      1
* NOD.NAME      COORD'S (X,Y) RELATIVE TO END(1) OF SUBDIVIDED ELEMENT
* #n2           0.000000E+00           0.333333E+00
*-----*
*
*NUMBER OF ELEMENTS CREATED
*      2
* ELM.NAME      TYPE.OF.ELEMENT      NOD.NAMES
* #e3           cbp2                 2      #n2
* #e4           qdp2                 #n2     4
*-----*
*
*NUMBER OF IMPERFECT ELEMENTS
*      0
*****

```

|    |                |   |           |   |
|----|----------------|---|-----------|---|
| 0  | 0.17300000E+01 | 0 | 0.317E-04 | 1 |
| 87 | 0.17400000E+01 | 0 | 0.374E-04 | 1 |

```

***** ( SUBDIVISION OF ELEMENT #e2 ) *****
*
*NUMBER OF NODES CREATED
*      1
* NOD.NAME      COORD'S (X,Y) RELATIVE TO END(1) OF SUBDIVIDED ELEMENT
* #n3           0.000000E+00           0.333333E+01
*-----*
*
*NUMBER OF ELEMENTS CREATED
*      2
* ELM.NAME      TYPE.OF.ELEMENT      NOD.NAMES
* #e6           cbp2                 #n3     3
* #e5           qdp2                 #n1     #n3

```

```

*-----*
*
*NUMBER OF IMPERFECT ELEMENTS
*          0
*****

***** ( SUBDIVISION OF ELEMENT #e4 )*****
*
*NUMBER OF NODES CREATED
*          1
* NOD.NAME      COORD'S (X,Y) RELATIVE TO END(1) OF SUBDIVIDED ELEMENT
* #n4           0.000000E+00          0.333333E+01
*-----*
*
*NUMBER OF ELEMENTS CREATED
*          2
* ELM.NAME      TYPE.OF.ELEMENT      NOD.NAMES
* #e8           cbp2                 #n4          4
* #e7           qdp2                 #n2          #n4
*-----*
*
*NUMBER OF IMPERFECT ELEMENTS
*          0
*****

      0          0.17500000E+01      0          0.727E-04          1
     88          0.17600000E+01      0          0.624E-04          1
      0          0.17700000E+01      0          0.327E-04          1

***** ( SUBDIVISION OF ELEMENT #e5 )*****
*
*NUMBER OF NODES CREATED
*          1
* NOD.NAME      COORD'S (X,Y) RELATIVE TO END(1) OF SUBDIVIDED ELEMENT
* #n5           0.000000E+00          0.666667E+00
*-----*
*
*NUMBER OF ELEMENTS CREATED
*          2
* ELM.NAME      TYPE.OF.ELEMENT      NOD.NAMES
* #e9           cbp2                 #n1          #n5
* #e10          qdp2                 #n5          #n3
*-----*
*
*NUMBER OF IMPERFECT ELEMENTS
*          0
*****

***** ( SUBDIVISION OF ELEMENT #e7 )*****
*
*NUMBER OF NODES CREATED
*          1
* NOD.NAME      COORD'S (X,Y) RELATIVE TO END(1) OF SUBDIVIDED ELEMENT
* #n6           0.000000E+00          0.666667E+00
*-----*
*
*NUMBER OF ELEMENTS CREATED
*          2
* ELM.NAME      TYPE.OF.ELEMENT      NOD.NAMES

```



```

* #e11          cbp2          #n2          #n6          *
* #e12          qdp2          #n6          #n4          *
*-----*
*
*NUMBER OF IMPERFECT ELEMENTS          *
*          0          *
*****

```

|     |                |   |           |   |
|-----|----------------|---|-----------|---|
| 89  | 0.17800000E+01 | 0 | 0.204E-04 | 1 |
| 0   | 0.17900000E+01 | 0 | 0.230E-04 | 1 |
| 90  | 0.18000000E+01 | 0 | 0.299E-04 | 1 |
| 0   | 0.18100000E+01 | 0 | 0.122E-05 | 1 |
| 91  | 0.18200000E+01 | 0 | 0.201E-05 | 1 |
| 0   | 0.18300000E+01 | 0 | 0.287E-05 | 1 |
| 92  | 0.18400000E+01 | 0 | 0.659E-05 | 1 |
| 0   | 0.18500000E+01 | 0 | 0.993E-06 | 1 |
| 93  | 0.18600000E+01 | 0 | 0.423E-05 | 1 |
| 0   | 0.18700000E+01 | 0 | 0.117E-04 | 1 |
| 94  | 0.18800000E+01 | 0 | 0.658E-06 | 1 |
| 0   | 0.18900000E+01 | 0 | 0.102E-04 | 1 |
| 95  | 0.19000000E+01 | 0 | 0.212E-04 | 1 |
| 0   | 0.19100000E+01 | 0 | 0.115E-04 | 1 |
| 96  | 0.19200000E+01 | 0 | 0.541E-05 | 1 |
| 0   | 0.19300000E+01 | 0 | 0.254E-05 | 1 |
| 97  | 0.19400000E+01 | 0 | 0.322E-05 | 1 |
| 0   | 0.19500000E+01 | 0 | 0.266E-05 | 1 |
| 98  | 0.19600000E+01 | 0 | 0.317E-05 | 1 |
| 0   | 0.19700000E+01 | 0 | 0.370E-05 | 1 |
| 99  | 0.19800000E+01 | 0 | 0.405E-05 | 1 |
| 0   | 0.19900000E+01 | 0 | 0.402E-05 | 1 |
| 100 | 0.20000000E+01 | 0 | 0.373E-05 | 1 |
| 0   | 0.20100000E+01 | 0 | 0.268E-04 | 1 |
| 101 | 0.20200000E+01 | 0 | 0.151E-04 | 1 |
| 0   | 0.20300000E+01 | 0 | 0.357E-05 | 1 |
| 102 | 0.20400000E+01 | 0 | 0.398E-05 | 1 |
| 0   | 0.20500000E+01 | 0 | 0.424E-05 | 1 |
| 103 | 0.20600000E+01 | 0 | 0.435E-05 | 1 |
| 0   | 0.20700000E+01 | 0 | 0.437E-05 | 1 |
| 104 | 0.20800000E+01 | 0 | 0.442E-05 | 1 |
| 0   | 0.20900000E+01 | 0 | 0.464E-05 | 1 |
| 105 | 0.21000000E+01 | 0 | 0.496E-05 | 1 |
| 0   | 0.21100000E+01 | 0 | 0.521E-05 | 1 |
| 106 | 0.21200000E+01 | 0 | 0.532E-05 | 1 |
| 0   | 0.21300000E+01 | 0 | 0.525E-05 | 1 |
| 107 | 0.21400000E+01 | 0 | 0.505E-05 | 1 |
| 0   | 0.21500000E+01 | 0 | 0.478E-05 | 1 |
| 108 | 0.21600000E+01 | 0 | 0.447E-05 | 1 |
| 0   | 0.21700000E+01 | 0 | 0.423E-05 | 1 |
| 109 | 0.21800000E+01 | 0 | 0.410E-05 | 1 |
| 0   | 0.21900000E+01 | 0 | 0.399E-05 | 1 |
| 110 | 0.22000000E+01 | 0 | 0.377E-05 | 1 |
| 0   | 0.22100000E+01 | 0 | 0.343E-05 | 1 |
| 111 | 0.22200000E+01 | 0 | 0.308E-05 | 1 |

```

***** ( SUBDIVISION OF ELEMENT 5 ) *****
*
*NUMBER OF NODES CREATED          *
*          2          *
* NOD.NAME          COORD'S (X,Y) RELATIVE TO END(1) OF SUBDIVIDED ELEMENT *
* #n7          0.500000E+00          0.000000E+00          *
* #n8          0.550000E+01          0.000000E+00          *

```

```

*-----*
*
*NUMBER OF ELEMENTS CREATED
*      3
* ELM.NAME   TYPE.OF.ELEMENT   NOD.NAMES
* #e13       cbp2              3      #n7
* #e15       cbp2              #n8     4
* #e14       qdp2              #n7     #n8
*-----*
*
*NUMBER OF IMPERFECT ELEMENTS
*      0
*****
      0      0.22300000E+01      0      0.809E-05      1
*****
***** ( SUBDIVISION OF ELEMENT 3 ) *****
*
*NUMBER OF NODES CREATED
*      1
* NOD.NAME   COORD'S (X,Y) RELATIVE TO END(1) OF SUBDIVIDED ELEMENT
* #n9        0.000000E+00      0.366667E+01
*-----*
*
*NUMBER OF ELEMENTS CREATED
*      2
* ELM.NAME   TYPE.OF.ELEMENT   NOD.NAMES
* #e17       cbp2              #n9     5
* #e16       qdp2              3      #n9
*-----*
*
*NUMBER OF IMPERFECT ELEMENTS
*      0
*****
***** ( SUBDIVISION OF ELEMENT 4 ) *****
*
*NUMBER OF NODES CREATED
*      1
* NOD.NAME   COORD'S (X,Y) RELATIVE TO END(1) OF SUBDIVIDED ELEMENT
* #n10       0.000000E+00      0.366667E+01
*-----*
*
*NUMBER OF ELEMENTS CREATED
*      2
* ELM.NAME   TYPE.OF.ELEMENT   NOD.NAMES
* #e19       cbp2              #n10    6
* #e18       qdp2              4      #n10
*-----*
*
*NUMBER OF IMPERFECT ELEMENTS
*      0
*****
***** ( SUBDIVISION OF ELEMENT 6 ) *****
*
*NUMBER OF NODES CREATED
*      2
* NOD.NAME   COORD'S (X,Y) RELATIVE TO END(1) OF SUBDIVIDED ELEMENT

```

```

* #n11          0.500000E+00          0.000000E+00          *
* #n12          0.550000E+01          0.000000E+00          *
*-----*
*
*NUMBER OF ELEMENTS CREATED          *
*          3                          *
* ELM.NAME      TYPE.OF.ELEMENT      NOD.NAMES          *
* #e20          cbp2                  5          #n11      *
* #e22          cbp2                  #n12         6          *
* #e21          qdp2                  #n11         #n12      *
*-----*
*
*NUMBER OF IMPERFECT ELEMENTS        *
*          0                          *
*****
112          0.22400000E+01          0          0.608E-05          1

***** ( SUBDIVISION OF ELEMENT #e16 )*****
*
*NUMBER OF NODES CREATED              *
*          1                          *
* NOD.NAME      COORD'S (X,Y) RELATIVE TO END(1) OF SUBDIVIDED ELEMENT *
* #n13          0.000000E+00          0.333333E+00      *
*-----*
*
*NUMBER OF ELEMENTS CREATED           *
*          2                          *
* ELM.NAME      TYPE.OF.ELEMENT      NOD.NAMES          *
* #e23          cbp2                  3          #n13      *
* #e24          qdp2                  #n13         #n9       *
*-----*
*
*NUMBER OF IMPERFECT ELEMENTS        *
*          0                          *
*****

***** ( SUBDIVISION OF ELEMENT #e18 )*****
*
*NUMBER OF NODES CREATED              *
*          1                          *
* NOD.NAME      COORD'S (X,Y) RELATIVE TO END(1) OF SUBDIVIDED ELEMENT *
* #n14          0.000000E+00          0.333333E+00      *
*-----*
*
*NUMBER OF ELEMENTS CREATED           *
*          2                          *
* ELM.NAME      TYPE.OF.ELEMENT      NOD.NAMES          *
* #e25          cbp2                  4          #n14      *
* #e26          qdp2                  #n14         #n10     *
*-----*
*
*NUMBER OF IMPERFECT ELEMENTS        *
*          0                          *
*****
0          0.22500000E+01          0          0.183E-04          1
113         0.22600000E+01          0          0.814E-05          1
0          0.22700000E+01          0          0.951E-05          1
114         0.22800000E+01          0          0.257E-04          1

```

|     |                |   |           |   |
|-----|----------------|---|-----------|---|
| 0   | 0.22900000E+01 | 0 | 0.200E-04 | 1 |
| 115 | 0.23000000E+01 | 0 | 0.248E-04 | 1 |
| 0   | 0.23100000E+01 | 0 | 0.325E-04 | 1 |
| 116 | 0.23200000E+01 | 0 | 0.216E-04 | 1 |

```

***** ( SUBDIVISION OF ELEMENT #e24 )*****
*
*NUMBER OF NODES CREATED
*      1
* NOD.NAME      COORD'S (X,Y) RELATIVE TO END(1) OF SUBDIVIDED ELEMENT
* #n15          0.000000E+00          0.666667E+00
*-----*
*
*NUMBER OF ELEMENTS CREATED
*      2
* ELM.NAME      TYPE.OF.ELEMENT      NOD.NAMES
* #e27          cbp2                  #n13      #n15
* #e28          qdp2                  #n15      #n9
*-----*
*
*NUMBER OF IMPERFECT ELEMENTS
*      0
*****

```

```

***** ( SUBDIVISION OF ELEMENT #e26 )*****
*
*NUMBER OF NODES CREATED
*      1
* NOD.NAME      COORD'S (X,Y) RELATIVE TO END(1) OF SUBDIVIDED ELEMENT
* #n16          0.000000E+00          0.666667E+00
*-----*
*
*NUMBER OF ELEMENTS CREATED
*      2
* ELM.NAME      TYPE.OF.ELEMENT      NOD.NAMES
* #e29          cbp2                  #n14      #n16
* #e30          qdp2                  #n16      #n10
*-----*
*
*NUMBER OF IMPERFECT ELEMENTS
*      0
*****

```

|     |                |   |           |   |
|-----|----------------|---|-----------|---|
| 0   | 0.23300000E+01 | 0 | 0.115E-04 | 1 |
| 117 | 0.23400000E+01 | 0 | 0.251E-04 | 1 |
| 0   | 0.23500000E+01 | 0 | 0.191E-04 | 1 |
| 118 | 0.23600000E+01 | 0 | 0.307E-04 | 1 |
| 0   | 0.23700000E+01 | 0 | 0.562E-05 | 1 |

```

***** ( SUBDIVISION OF ELEMENT #e30 )*****
*
*NUMBER OF NODES CREATED
*      1
* NOD.NAME      COORD'S (X,Y) RELATIVE TO END(1) OF SUBDIVIDED ELEMENT
* #n17          0.000000E+00          0.200000E+01
*-----*
*
*NUMBER OF ELEMENTS CREATED
*      2
* ELM.NAME      TYPE.OF.ELEMENT      NOD.NAMES

```

```

* #e32          cbp2          #n17          #n10          *
* #e31          qdp2          #n16          #n17          *
*-----*
*
*NUMBER OF IMPERFECT ELEMENTS          *
*          0          *
*****
***** ( SUBDIVISION OF ELEMENT #e21 )*****
*
*NUMBER OF NODES CREATED          *
*          1          *
* NOD.NAME          COORD'S (X,Y) RELATIVE TO END(1) OF SUBDIVIDED ELEMENT *
* #n18          0.100000E+01          0.000000E+00          *
*-----*
*
*NUMBER OF ELEMENTS CREATED          *
*          2          *
* ELM.NAME          TYPE.OF.ELEMENT          NOD.NAMES          *
* #e33          cbp2          #n11          #n18          *
* #e34          qdp2          #n18          #n12          *
*-----*
*
*NUMBER OF IMPERFECT ELEMENTS          *
*          0          *
*****
119          0.23800000E+01          0          0.148E-04          1
***** ( SUBDIVISION OF ELEMENT #e34 )*****
*
*NUMBER OF NODES CREATED          *
*          1          *
* NOD.NAME          COORD'S (X,Y) RELATIVE TO END(1) OF SUBDIVIDED ELEMENT *
* #n19          0.300000E+01          0.000000E+00          *
*-----*
*
*NUMBER OF ELEMENTS CREATED          *
*          2          *
* ELM.NAME          TYPE.OF.ELEMENT          NOD.NAMES          *
* #e36          cbp2          #n19          #n12          *
* #e35          qdp2          #n18          #n19          *
*-----*
*
*NUMBER OF IMPERFECT ELEMENTS          *
*          0          *
*****
0          0.23900000E+01          0          0.838E-05          1
***** ( SUBDIVISION OF ELEMENT #e28 )*****
*
*NUMBER OF NODES CREATED          *
*          1          *
* NOD.NAME          COORD'S (X,Y) RELATIVE TO END(1) OF SUBDIVIDED ELEMENT *
* #n20          0.000000E+00          0.200000E+01          *
*-----*
*
*NUMBER OF ELEMENTS CREATED          *
*          2          *

```

```

* ELM.NAME      TYPE.OF.ELEMENT      NOD.NAMES
* #e38          cbp2          #n20      #n9
* #e37          qdp2          #n15      #n20
*-----*

```

```

*NUMBER OF IMPERFECT ELEMENTS

```

```

*          0
*****

```

|     |                |   |           |   |
|-----|----------------|---|-----------|---|
| 120 | 0.24000000E+01 | 0 | 0.323E-05 | 1 |
| 0   | 0.24100000E+01 | 0 | 0.379E-05 | 1 |
| 121 | 0.24200000E+01 | 0 | 0.422E-05 | 1 |
| 0   | 0.24300000E+01 | 0 | 0.319E-05 | 1 |
| 122 | 0.24400000E+01 | 0 | 0.667E-06 | 1 |
| 0   | 0.24500000E+01 | 0 | 0.412E-05 | 1 |
| 123 | 0.24600000E+01 | 0 | 0.515E-05 | 1 |
| 0   | 0.24700000E+01 | 0 | 0.527E-06 | 1 |
| 124 | 0.24800000E+01 | 0 | 0.492E-05 | 1 |
| 0   | 0.24900000E+01 | 0 | 0.217E-04 | 1 |
| 125 | 0.25000000E+01 | 0 | 0.531E-06 | 1 |
| 0   | 0.25100000E+01 | 0 | 0.515E-06 | 1 |
| 126 | 0.25200000E+01 | 0 | 0.562E-06 | 1 |
| 0   | 0.25300000E+01 | 0 | 0.546E-06 | 1 |
| 127 | 0.25400000E+01 | 0 | 0.760E-06 | 1 |
| 0   | 0.25500000E+01 | 0 | 0.917E-06 | 1 |
| 128 | 0.25600000E+01 | 0 | 0.101E-05 | 1 |
| 0   | 0.25700000E+01 | 0 | 0.136E-05 | 1 |
| 129 | 0.25800000E+01 | 0 | 0.187E-05 | 1 |
| 0   | 0.25900000E+01 | 0 | 0.186E-05 | 1 |
| 130 | 0.26000000E+01 | 0 | 0.198E-05 | 1 |
| 0   | 0.26100000E+01 | 0 | 0.225E-05 | 1 |
| 131 | 0.26200000E+01 | 0 | 0.262E-05 | 1 |
| 0   | 0.26300000E+01 | 0 | 0.306E-05 | 1 |
| 132 | 0.26400000E+01 | 0 | 0.324E-05 | 1 |
| 0   | 0.26500000E+01 | 0 | 0.332E-05 | 1 |
| 133 | 0.26600000E+01 | 0 | 0.370E-05 | 1 |
| 0   | 0.26700000E+01 | 0 | 0.410E-05 | 1 |
| 134 | 0.26800000E+01 | 0 | 0.421E-05 | 1 |
| 0   | 0.26900000E+01 | 0 | 0.435E-05 | 1 |
| 135 | 0.27000000E+01 | 0 | 0.464E-05 | 1 |
| 0   | 0.27100000E+01 | 0 | 0.477E-05 | 1 |
| 136 | 0.27200000E+01 | 0 | 0.477E-05 | 1 |
| 0   | 0.27300000E+01 | 0 | 0.491E-05 | 1 |
| 137 | 0.27400000E+01 | 0 | 0.481E-05 | 1 |
| 0   | 0.27500000E+01 | 0 | 0.446E-05 | 1 |
| 138 | 0.27600000E+01 | 0 | 0.433E-05 | 1 |
| 0   | 0.27700000E+01 | 0 | 0.451E-05 | 1 |
| 139 | 0.27800000E+01 | 0 | 0.484E-05 | 1 |
| 0   | 0.27900000E+01 | 0 | 0.503E-05 | 1 |
| 140 | 0.28000000E+01 | 0 | 0.469E-05 | 1 |
| 0   | 0.28100000E+01 | 0 | 0.393E-05 | 1 |
| 141 | 0.28200000E+01 | 0 | 0.353E-05 | 1 |
| 0   | 0.28300000E+01 | 0 | 0.356E-05 | 1 |
| 142 | 0.28400000E+01 | 0 | 0.379E-05 | 1 |
| 0   | 0.28500000E+01 | 0 | 0.387E-05 | 1 |
| 143 | 0.28600000E+01 | 0 | 0.370E-05 | 1 |
| 0   | 0.28700000E+01 | 0 | 0.344E-05 | 1 |
| 144 | 0.28800000E+01 | 0 | 0.317E-05 | 1 |
| 0   | 0.28900000E+01 | 0 | 0.292E-05 | 1 |
| 145 | 0.29000000E+01 | 0 | 0.276E-05 | 1 |
| 0   | 0.29100000E+01 | 0 | 0.271E-05 | 1 |

|     |                |   |           |   |
|-----|----------------|---|-----------|---|
| 146 | 0.29200000E+01 | 0 | 0.270E-05 | 1 |
| 0   | 0.29300000E+01 | 0 | 0.253E-05 | 1 |
| 147 | 0.29400000E+01 | 0 | 0.240E-05 | 1 |
| 0   | 0.29500000E+01 | 0 | 0.250E-05 | 1 |
| 148 | 0.29600000E+01 | 0 | 0.410E-05 | 1 |
| 0   | 0.29700000E+01 | 0 | 0.113E-04 | 1 |
| 149 | 0.29800000E+01 | 0 | 0.191E-05 | 1 |
| 0   | 0.29900000E+01 | 0 | 0.153E-05 | 1 |
| 150 | 0.30000000E+01 | 0 | 0.152E-04 | 1 |
| 0   | 0.30100000E+01 | 0 | 0.146E-05 | 1 |
| 151 | 0.30200000E+01 | 0 | 0.590E-05 | 1 |
| 0   | 0.30300000E+01 | 0 | 0.722E-05 | 1 |
| 152 | 0.30400000E+01 | 0 | 0.531E-04 | 1 |
| 0   | 0.30500000E+01 | 0 | 0.745E-05 | 1 |
| 153 | 0.30600000E+01 | 0 | 0.417E-06 | 1 |
| 0   | 0.30700000E+01 | 0 | 0.315E-06 | 1 |
| 154 | 0.30800000E+01 | 0 | 0.273E-06 | 1 |
| 0   | 0.30900000E+01 | 0 | 0.270E-05 | 1 |
| 155 | 0.31000000E+01 | 0 | 0.627E-07 | 1 |
| 0   | 0.31100000E+01 | 0 | 0.102E-04 | 1 |
| 156 | 0.31200000E+01 | 0 | 0.124E-06 | 1 |
| 0   | 0.31300000E+01 | 0 | 0.136E-06 | 1 |
| 157 | 0.31400000E+01 | 0 | 0.121E-06 | 1 |
| 0   | 0.31500000E+01 | 0 | 0.147E-06 | 1 |
| 158 | 0.31600000E+01 | 0 | 0.241E-06 | 1 |
| 0   | 0.31700000E+01 | 0 | 0.410E-06 | 1 |
| 159 | 0.31800000E+01 | 0 | 0.712E-06 | 1 |
| 0   | 0.31900000E+01 | 0 | 0.104E-05 | 1 |
| 160 | 0.32000000E+01 | 0 | 0.121E-05 | 1 |
| 0   | 0.32100000E+01 | 0 | 0.117E-05 | 1 |
| 161 | 0.32200000E+01 | 0 | 0.124E-05 | 1 |
| 0   | 0.32300000E+01 | 0 | 0.146E-05 | 1 |
| 162 | 0.32400000E+01 | 0 | 0.185E-05 | 1 |
| 0   | 0.32500000E+01 | 0 | 0.218E-05 | 1 |
| 163 | 0.32600000E+01 | 0 | 0.222E-05 | 1 |
| 0   | 0.32700000E+01 | 0 | 0.219E-05 | 1 |
| 164 | 0.32800000E+01 | 0 | 0.228E-05 | 1 |
| 0   | 0.32900000E+01 | 0 | 0.225E-05 | 1 |
| 165 | 0.33000000E+01 | 0 | 0.225E-05 | 1 |
| 0   | 0.33100000E+01 | 0 | 0.240E-05 | 1 |
| 166 | 0.33200000E+01 | 0 | 0.253E-05 | 1 |
| 0   | 0.33300000E+01 | 0 | 0.251E-05 | 1 |
| 167 | 0.33400000E+01 | 0 | 0.239E-05 | 1 |
| 0   | 0.33500000E+01 | 0 | 0.225E-05 | 1 |
| 168 | 0.33600000E+01 | 0 | 0.215E-05 | 1 |
| 0   | 0.33700000E+01 | 0 | 0.205E-05 | 1 |
| 169 | 0.33800000E+01 | 0 | 0.183E-05 | 1 |
| 0   | 0.33900000E+01 | 0 | 0.155E-05 | 1 |
| 170 | 0.34000000E+01 | 0 | 0.140E-05 | 1 |
| 0   | 0.34100000E+01 | 0 | 0.135E-05 | 1 |
| 171 | 0.34200000E+01 | 0 | 0.126E-05 | 1 |
| 0   | 0.34300000E+01 | 0 | 0.116E-05 | 1 |
| 172 | 0.34400000E+01 | 0 | 0.106E-05 | 1 |
| 0   | 0.34500000E+01 | 0 | 0.104E-05 | 1 |
| 173 | 0.34600000E+01 | 0 | 0.103E-05 | 1 |
| 0   | 0.34700000E+01 | 0 | 0.960E-06 | 1 |
| 174 | 0.34800000E+01 | 0 | 0.928E-06 | 1 |
| 0   | 0.34900000E+01 | 0 | 0.997E-06 | 1 |
| 175 | 0.35000000E+01 | 0 | 0.878E-06 | 1 |
| 0   | 0.35100000E+01 | 0 | 0.692E-06 | 1 |
| 176 | 0.35200000E+01 | 0 | 0.679E-06 | 1 |

|     |                |   |           |   |
|-----|----------------|---|-----------|---|
| 0   | 0.35300000E+01 | 0 | 0.579E-06 | 1 |
| 177 | 0.35400000E+01 | 0 | 0.585E-06 | 1 |
| 0   | 0.35500000E+01 | 0 | 0.668E-06 | 1 |
| 178 | 0.35600000E+01 | 0 | 0.768E-06 | 1 |
| 0   | 0.35700000E+01 | 0 | 0.591E-06 | 1 |
| 179 | 0.35800000E+01 | 0 | 0.468E-06 | 1 |
| 0   | 0.35900000E+01 | 0 | 0.439E-06 | 1 |
| 180 | 0.36000000E+01 | 0 | 0.404E-06 | 1 |
| 0   | 0.36100000E+01 | 0 | 0.504E-06 | 1 |
| 181 | 0.36200000E+01 | 0 | 0.607E-06 | 1 |
| 0   | 0.36300000E+01 | 0 | 0.677E-06 | 1 |
| 182 | 0.36400000E+01 | 0 | 0.757E-06 | 1 |
| 0   | 0.36500000E+01 | 0 | 0.756E-06 | 1 |
| 183 | 0.36600000E+01 | 0 | 0.776E-06 | 1 |
| 0   | 0.36700000E+01 | 0 | 0.906E-06 | 1 |
| 184 | 0.36800000E+01 | 0 | 0.250E-04 | 1 |
| 0   | 0.36900000E+01 | 0 | 0.914E-06 | 1 |
| 185 | 0.37000000E+01 | 0 | 0.124E-05 | 1 |
| 0   | 0.37100000E+01 | 0 | 0.338E-04 | 1 |
| 186 | 0.37200000E+01 | 0 | 0.140E-05 | 1 |
| 0   | 0.37300000E+01 | 0 | 0.236E-04 | 1 |
| 187 | 0.37400000E+01 | 0 | 0.424E-04 | 1 |
| 0   | 0.37500000E+01 | 0 | 0.134E-04 | 1 |
| 188 | 0.37600000E+01 | 0 | 0.344E-04 | 1 |
| 0   | 0.37700000E+01 | 0 | 0.188E-05 | 1 |
| 189 | 0.37800000E+01 | 0 | 0.141E-05 | 1 |
| 0   | 0.37900000E+01 | 0 | 0.165E-05 | 1 |
| 190 | 0.38000000E+01 | 0 | 0.250E-04 | 1 |
| 0   | 0.38100000E+01 | 0 | 0.345E-05 | 1 |
| 191 | 0.38200000E+01 | 0 | 0.140E-04 | 1 |
| 0   | 0.38300000E+01 | 0 | 0.621E-05 | 1 |
| 192 | 0.38400000E+01 | 0 | 0.375E-05 | 1 |
| 0   | 0.38500000E+01 | 0 | 0.647E-05 | 1 |
| 193 | 0.38600000E+01 | 0 | 0.464E-05 | 1 |
| 0   | 0.38700000E+01 | 0 | 0.472E-05 | 1 |
| 194 | 0.38800000E+01 | 0 | 0.523E-05 | 1 |
| 0   | 0.38900000E+01 | 0 | 0.280E-04 | 1 |
| 195 | 0.39000000E+01 | 0 | 0.197E-04 | 1 |
| 0   | 0.39100000E+01 | 0 | 0.566E-05 | 1 |
| 196 | 0.39200000E+01 | 0 | 0.627E-05 | 1 |
| 0   | 0.39300000E+01 | 0 | 0.649E-05 | 1 |
| 197 | 0.39400000E+01 | 0 | 0.625E-05 | 1 |
| 0   | 0.39500000E+01 | 0 | 0.581E-05 | 1 |
| 198 | 0.39600000E+01 | 0 | 0.616E-05 | 1 |
| 0   | 0.39700000E+01 | 0 | 0.621E-05 | 1 |
| 199 | 0.39800000E+01 | 0 | 0.626E-05 | 1 |
| 0   | 0.39900000E+01 | 0 | 0.639E-05 | 1 |
| 200 | 0.40000000E+01 | 0 | 0.644E-05 | 1 |
| 0   | 0.40100000E+01 | 0 | 0.632E-05 | 1 |
| 201 | 0.40200000E+01 | 0 | 0.607E-05 | 1 |
| 0   | 0.40300000E+01 | 0 | 0.577E-05 | 1 |
| 202 | 0.40400000E+01 | 0 | 0.552E-05 | 1 |
| 0   | 0.40500000E+01 | 0 | 0.515E-05 | 1 |
| 203 | 0.40600000E+01 | 0 | 0.463E-05 | 1 |
| 0   | 0.40700000E+01 | 0 | 0.436E-05 | 1 |
| 204 | 0.40800000E+01 | 0 | 0.439E-05 | 1 |
| 0   | 0.40900000E+01 | 0 | 0.433E-05 | 1 |
| 205 | 0.41000000E+01 | 0 | 0.381E-05 | 1 |
| 0   | 0.41100000E+01 | 0 | 0.382E-04 | 1 |
| 206 | 0.41200000E+01 | 0 | 0.334E-05 | 1 |
| 0   | 0.41300000E+01 | 0 | 0.962E-04 | 1 |



|     |                |   |           |   |
|-----|----------------|---|-----------|---|
| 207 | 0.41400000E+01 | 0 | 0.601E-04 | 1 |
| 0   | 0.41500000E+01 | 0 | 0.369E-05 | 1 |
| 208 | 0.41600000E+01 | 0 | 0.312E-04 | 1 |
| 0   | 0.41700000E+01 | 0 | 0.359E-04 | 1 |
| 209 | 0.41800000E+01 | 0 | 0.138E-04 | 1 |
| 0   | 0.41900000E+01 | 0 | 0.165E-04 | 1 |
| 210 | 0.42000000E+01 | 0 | 0.255E-04 | 1 |
| 0   | 0.42100000E+01 | 0 | 0.616E-05 | 1 |
| 211 | 0.42200000E+01 | 0 | 0.495E-05 | 1 |
| 0   | 0.42300000E+01 | 0 | 0.145E-04 | 1 |
| 212 | 0.42400000E+01 | 0 | 0.721E-05 | 1 |
| 0   | 0.42500000E+01 | 0 | 0.510E-05 | 1 |
| 213 | 0.42600000E+01 | 0 | 0.287E-04 | 1 |
| 0   | 0.42700000E+01 | 0 | 0.544E-05 | 1 |
| 214 | 0.42800000E+01 | 0 | 0.776E-05 | 1 |
| 0   | 0.42900000E+01 | 0 | 0.107E-04 | 1 |
| 215 | 0.43000000E+01 | 0 | 0.259E-04 | 1 |
| 0   | 0.43100000E+01 | 0 | 0.139E-04 | 1 |
| 216 | 0.43200000E+01 | 0 | 0.405E-04 | 1 |
| 0   | 0.43300000E+01 | 0 | 0.139E-04 | 1 |
| 217 | 0.43400000E+01 | 0 | 0.116E-04 | 1 |

\*\*\*\*\* ( SUBDIVISION OF ELEMENT #e14 )\*\*\*\*\*

\* \* \* \* \*

\*NUMBER OF NODES CREATED \* \* \* \* \*

\* 2 \* \* \* \* \*

\* NOD.NAME COORD'S (X,Y) RELATIVE TO END(1) OF SUBDIVIDED ELEMENT \* \* \* \* \*

\* #n21 0.100000E+01 0.000000E+00 \* \* \* \* \*

\* #n22 0.400000E+01 0.000000E+00 \* \* \* \* \*

\*-----\* \* \* \* \*

\* \* \* \* \*

\*NUMBER OF ELEMENTS CREATED \* \* \* \* \*

\* 3 \* \* \* \* \*

\* ELM.NAME TYPE.OF.ELEMENT NOD.NAMES \* \* \* \* \*

\* #e39 cbp2 #n7 #n21 \* \* \* \* \*

\* #e41 cbp2 #n22 #n8 \* \* \* \* \*

\* #e40 qdp2 #n21 #n22 \* \* \* \* \*

\*-----\* \* \* \* \*

\* \* \* \* \*

\*NUMBER OF IMPERFECT ELEMENTS \* \* \* \* \*

\* 0 \* \* \* \* \*

\*\*\*\*\*

|     |                |   |           |   |
|-----|----------------|---|-----------|---|
| 0   | 0.43500000E+01 | 0 | 0.253E-04 | 1 |
| 218 | 0.43600000E+01 | 0 | 0.844E-05 | 1 |
| 0   | 0.43700000E+01 | 0 | 0.258E-04 | 1 |
| 219 | 0.43800000E+01 | 0 | 0.280E-04 | 1 |
| 0   | 0.43900000E+01 | 0 | 0.492E-05 | 2 |
| 220 | 0.44000000E+01 | 0 | 0.956E-04 | 1 |
| 0   | 0.44100000E+01 | 0 | 0.657E-04 | 1 |
| 221 | 0.44200000E+01 | 0 | 0.168E-04 | 1 |
| 0   | 0.44300000E+01 | 0 | 0.231E-04 | 1 |
| 222 | 0.44400000E+01 | 0 | 0.218E-04 | 1 |
| 0   | 0.44500000E+01 | 0 | 0.181E-04 | 1 |
| 223 | 0.44600000E+01 | 0 | 0.190E-04 | 1 |
| 0   | 0.44700000E+01 | 0 | 0.463E-04 | 1 |
| 224 | 0.44800000E+01 | 0 | 0.983E-05 | 1 |
| 0   | 0.44900000E+01 | 0 | 0.137E-04 | 1 |
| 225 | 0.45000000E+01 | 0 | 0.326E-04 | 1 |
| 0   | 0.45100000E+01 | 0 | 0.339E-04 | 1 |
| 226 | 0.45200000E+01 | 0 | 0.130E-04 | 1 |

|     |                |   |           |   |
|-----|----------------|---|-----------|---|
| 0   | 0.45300000E+01 | 0 | 0.143E-04 | 1 |
| 227 | 0.45400000E+01 | 0 | 0.412E-05 | 1 |
| 0   | 0.45500000E+01 | 0 | 0.177E-05 | 1 |
| 228 | 0.45600000E+01 | 0 | 0.160E-05 | 1 |
| 0   | 0.45700000E+01 | 0 | 0.261E-05 | 1 |
| 229 | 0.45800000E+01 | 0 | 0.353E-05 | 1 |
| 0   | 0.45900000E+01 | 0 | 0.127E-04 | 1 |
| 230 | 0.46000000E+01 | 0 | 0.126E-04 | 1 |
| 0   | 0.46100000E+01 | 0 | 0.406E-06 | 1 |
| 231 | 0.46200000E+01 | 0 | 0.135E-05 | 1 |
| 0   | 0.46300000E+01 | 0 | 0.560E-04 | 1 |
| 232 | 0.46400000E+01 | 0 | 0.954E-05 | 1 |
| 0   | 0.46500000E+01 | 0 | 0.691E-06 | 1 |
| 233 | 0.46600000E+01 | 0 | 0.327E-04 | 1 |
| 0   | 0.46700000E+01 | 0 | 0.215E-04 | 1 |
| 234 | 0.46800000E+01 | 0 | 0.927E-05 | 1 |
| 0   | 0.46900000E+01 | 0 | 0.492E-05 | 1 |
| 235 | 0.47000000E+01 | 0 | 0.192E-04 | 1 |
| 0   | 0.47100000E+01 | 0 | 0.181E-04 | 1 |
| 236 | 0.47200000E+01 | 0 | 0.403E-04 | 1 |
| 0   | 0.47300000E+01 | 0 | 0.225E-04 | 1 |
| 237 | 0.47400000E+01 | 0 | 0.831E-05 | 1 |
| 0   | 0.47500000E+01 | 0 | 0.135E-04 | 1 |
| 238 | 0.47600000E+01 | 0 | 0.316E-05 | 1 |
| 0   | 0.47700000E+01 | 0 | 0.132E-04 | 1 |
| 239 | 0.47800000E+01 | 0 | 0.456E-04 | 1 |
| 0   | 0.47900000E+01 | 0 | 0.689E-05 | 1 |
| 240 | 0.48000000E+01 | 0 | 0.684E-05 | 1 |
| 0   | 0.48100000E+01 | 0 | 0.460E-04 | 1 |
| 241 | 0.48200000E+01 | 0 | 0.436E-04 | 1 |
| 0   | 0.48300000E+01 | 0 | 0.520E-05 | 1 |
| 242 | 0.48400000E+01 | 0 | 0.196E-04 | 1 |
| 0   | 0.48500000E+01 | 0 | 0.443E-04 | 1 |
| 243 | 0.48600000E+01 | 0 | 0.218E-04 | 1 |
| 0   | 0.48700000E+01 | 0 | 0.104E-04 | 1 |
| 244 | 0.48800000E+01 | 0 | 0.256E-04 | 1 |
| 0   | 0.48900000E+01 | 0 | 0.252E-04 | 1 |
| 245 | 0.49000000E+01 | 0 | 0.317E-04 | 1 |

\*\*\*\*\* ( SUBDIVISION OF ELEMENT #e12 )\*\*\*\*\*

\* \* \* \* \*

\*NUMBER OF NODES CREATED \* \* \* \* \*

\* 1 \* \* \* \* \*

\* NOD.NAME COORD'S (X,Y) RELATIVE TO END(1) OF SUBDIVIDED ELEMENT \* \* \* \* \*

\* #n23 0.000000E+00 0.200000E+01 \* \* \* \* \*

\*-----\* \* \* \* \*

\* \* \* \* \*

\*NUMBER OF ELEMENTS CREATED \* \* \* \* \*

\* 2 \* \* \* \* \*

\* ELM.NAME TYPE.OF.ELEMENT NOD.NAMES \* \* \* \* \*

\* #e43 cbp2 #n23 #n4 \* \* \* \* \*

\* #e42 qdp2 #n6 #n23 \* \* \* \* \*

\*-----\* \* \* \* \*

\* \* \* \* \*

\*NUMBER OF IMPERFECT ELEMENTS \* \* \* \* \*

\* 0 \* \* \* \* \*

\*\*\*\*\*

|   |                |   |           |   |
|---|----------------|---|-----------|---|
| 0 | 0.49100000E+01 | 0 | 0.196E-04 | 1 |
|---|----------------|---|-----------|---|

\*\*\*\*\* ( SUBDIVISION OF ELEMENT #e10 )\*\*\*\*\*

```

*
*NUMBER OF NODES CREATED
*
*          1
* NOD.NAME      COORD'S (X,Y) RELATIVE TO END(1) OF SUBDIVIDED ELEMENT
* #n24          0.000000E+00          0.200000E+01
*-----*
*
*NUMBER OF ELEMENTS CREATED
*
*          2
* ELM.NAME      TYPE.OF.ELEMENT      NOD.NAMES
* #e45          cbp2                  #n24      #n3
* #e44          qdp2                  #n5       #n24
*-----*
*
*NUMBER OF IMPERFECT ELEMENTS
*
*          0
*****

```

|     |                |   |           |   |
|-----|----------------|---|-----------|---|
| 246 | 0.49200000E+01 | 0 | 0.305E-04 | 1 |
| 0   | 0.49300000E+01 | 0 | 0.293E-04 | 1 |
| 247 | 0.49400000E+01 | 0 | 0.583E-04 | 1 |
| 0   | 0.49500000E+01 | 0 | 0.302E-04 | 1 |
| 248 | 0.49600000E+01 | 0 | 0.570E-04 | 1 |
| 0   | 0.49700000E+01 | 0 | 0.424E-04 | 1 |
| 249 | 0.49800000E+01 | 0 | 0.915E-04 | 1 |
| 0   | 0.49900000E+01 | 0 | 0.156E-04 | 1 |
| 250 | 0.50000000E+01 | 0 | 0.434E-04 | 1 |

## 9.6 Steel frame subject to explosion and fire loading

This example illustrates the considerable influence of explosion on the fire resistance of steel frames, even when the extent of structural damage due to explosion is relative small.

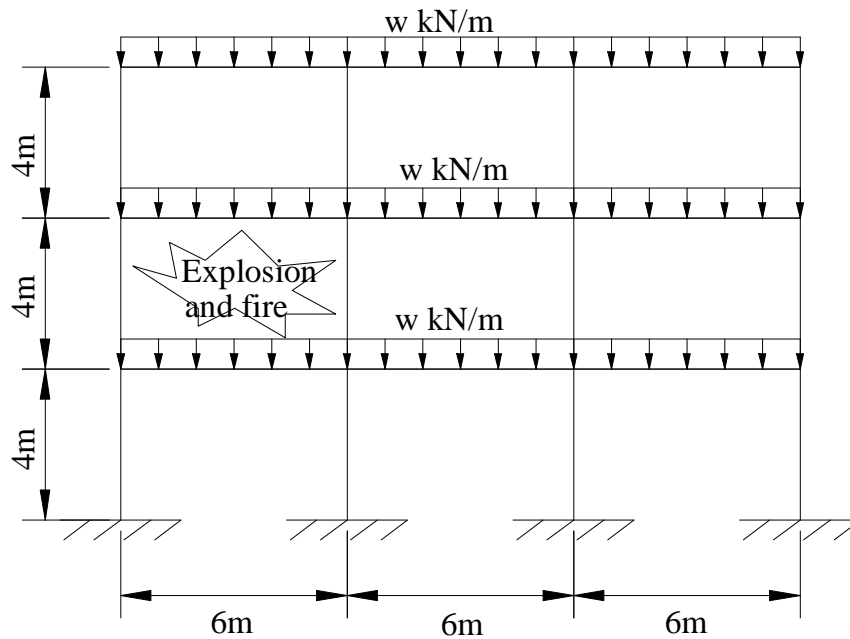


Figure 9.6 Steel frames subject to explosion and fire loading.

There are going to be used elasto-plastic cubic elements to resolve this example. The material model of steel used in this example covers the effects of the elevated temperature, creep and high strain-rate.

## 9.6.1 Data file

```
# Here temperatures are incremental over ambient temperature (20C)
#
analysis 2d dynamics (a)
#
materials (b)
mat.name      model      properties
  mat1        stl8      31.19 4.65e-3 20 &
                2.1e5 0.84e5 80. 680. 1080. &
                399. 59.9 280. 680. 980. &
                0.0 0.032 280. 380. 880. &
                0.01022 0.01652 730. 731. 1180.

#
sections (c)
  type = isec
mat.name = mat1
  sec.name      dimensions
  sec1          254.5 21.0 254.5 21.0 645.6 13.2
  sec2          152.4 6.8 152.4 6.8 138.8 6.1
  sec3          203.2 11.0 203.2 11.0 181.2 7.3

#
patterns (p)
pat.name      ratios
  pat1         1 1 1 1 1 1 1 1 1 1

#
groups (d)
type = cbp2
  grp.name      sec.name      monitoring.points
  grp1c         sec1          40
  grp2c         sec2          40
  grp3c         sec3          40
type = qdp2
  grp.name      cbp2.grp.name  pat.name
  grp1          grp1c         pat1
  grp2          grp2c         pat1
  grp3          grp3c         pat1

#
type = cnm2
  grp.name      mass
  gpm1          23.4
  gpm2          46.8

#
structural.nodal (e)
  nod.name      x      y
  f 101         0.0    0.0
  r 10          0.0    4000.0 3
  r 100         6000.0 0.0 3

#
restraints (g)
  nod.name      direction
  f 101         x+y+rz
  r 100         -      3

#
element.connectivity (h)
elm.name      grp.name      nod.name
  f 101        grp1         111 211
  r 1          -           100 100 2
  r 3          -           10 10 2

#
```

```

elm.name   grp.name   nod.name
f 201      grp2       101 111
r 1        -         10  10  2
r 3        -         300 300 1
#
elm.name   grp.name   nod.name
f 301      grp3       201 211
r 1        -         10  10  2
r 3        -         100 100 1
#
grp.name = gpm1
elm.name   nod.name
f 1101     111
r 1        10  2
r 3        300 1
#
grp.name = gpm2
elm.name   nod.name
f 1201     211
r 1        10  2
r 3        100 1
#
linear.curves # curves for time history loads
start.time = 18
crv.name = c1
      time   load.factor
      18.12   1.0
      18.15   0.0
      1220    0.0
crv.name = c2
      time   load.factor
      20     0.0
      1220   1.2
#
applied.loading
initial.load
elm.name   type   value
f 101      udl1   0   -75
r 1        -     0   0   2
r 3        -     0   0   2
#
dynamic.load
elm.name   type   crv.name   value
101        udl1   c1         0   -125
104        udl1   c1         0   125
202        udl1   c1        -125 0
302        udl1   c1         125 0
elm.name   type   crv.name   value
104        tmp2   c2        875 -0.3636   875 -0.3636   875 -0.3636
202        tmp2   c2        375 -1.6404   375 -1.6404   375 -1.6404
302        tmp2   c2       1000 0         1000 0         1000 0
equilibrium.stages
      end.of.stage   steps
      18.2           50
      20             45
      640            62
      670            30
#
integration
scheme = hilber
alpha = -0.3

```

[\(g\)](#)

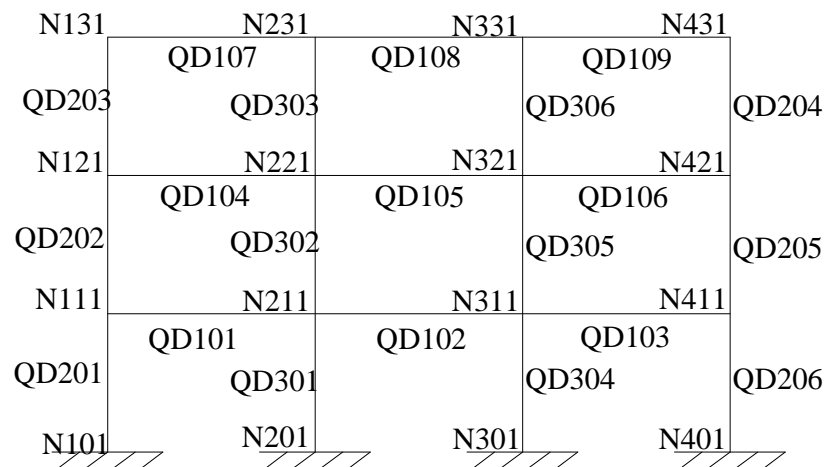
[\(i\)](#)

```

beta = 1.21
gamma = 0.8
#
iterative
number = 10
initial = 10
step = 10
dive = 10
maxi = 0.1e8
#
convergence.criteria (1)
tolerance = 0.5e-3
force.ref = 300e3
moment.ref = 300e6
#
output (m)
frequency 2
#
end

```

**Note** The following picture shows the names that have been given to the nodes and elements in the data file.

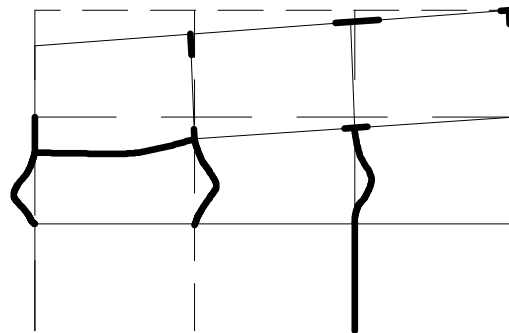


*figure 9.6.1 Nodes and elements .*

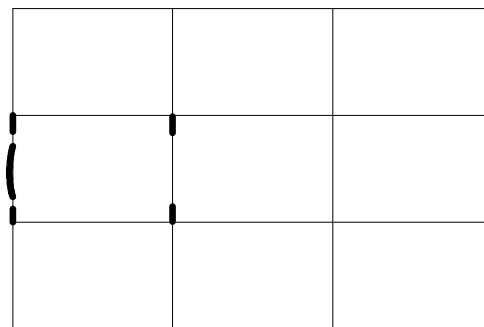
## 9.6.2 Structural behaviour

This example illustrates the considerable influence of explosion on the fire resistance of steel frames, even when the extent of structural damage due to explosion is relative small.

For both loading scenarios, elevated temperatures initiate buckling in the internal column at  $T \approx 475^\circ\text{C}$ . However, the explosion/fire scenario is associated with a much reduced overall fire resistance of ( $T \approx 642^\circ\text{C}$ ) in comparison with that of the fire only scenario ( $T \approx 894^\circ\text{C}$ ), representing a reduction of 28%. This reduction is mainly attributed to deterioration in vertical resistance of the side column due to explosion damage, leading to redistribution of vertical loading to the internal column and an earlier overall failure of the system. The deflected shapes for the two loading scenarios are shown in the following figure.



(a) fire loading



(b) explosion loading

figure 9.6.2a Final deflected shape after: (a) fire loading: (b) explosion.

The deformed shape if we consider explosion and fire loading given by ADAPTIC shows that the combination of both efforts.



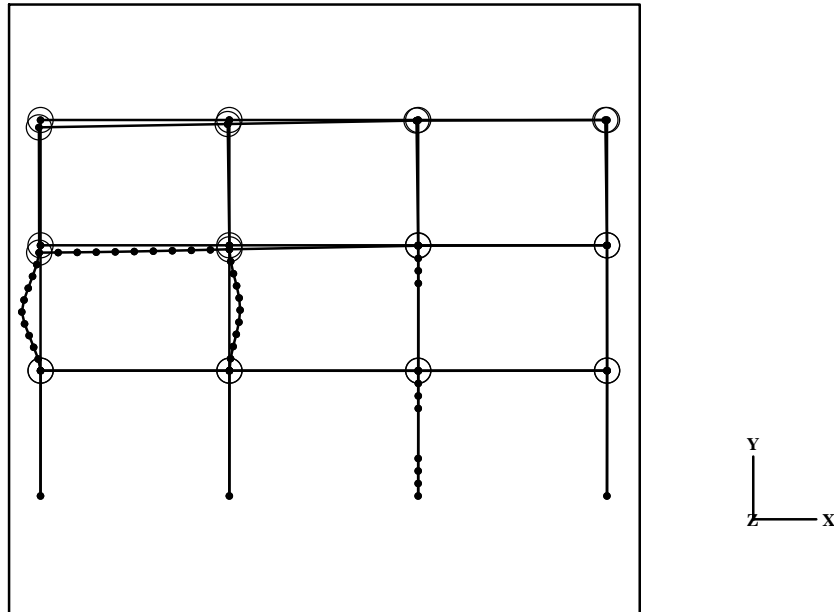


figure 9.6.2b Final deflected shape after explosion and fire loading.

In addition to the analysis of the structure it is going to be considered the CPU time demand over the displacements at the node 121, which is the one that experiments higher displacements.

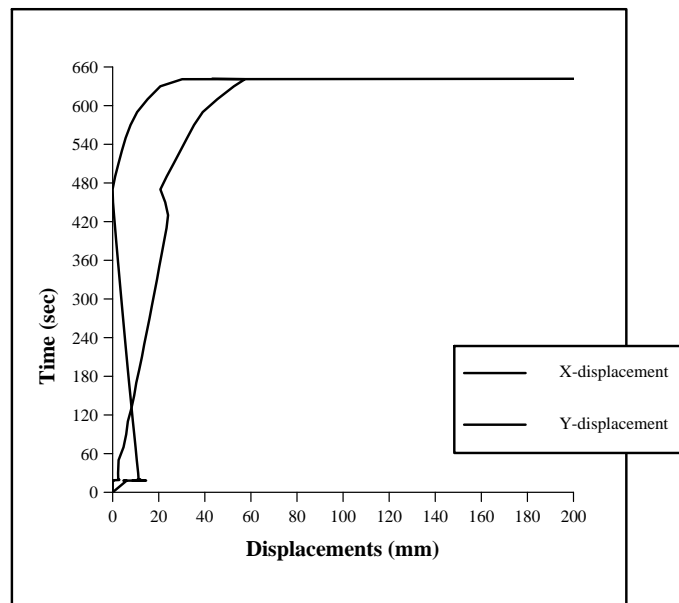


figure 9.6.2b Final deflected shape after explosion and fire loading.

### 9.6.3 Output file

```

ELEMENT ASSEMBLY ORDER
----->>>  ----->>>  ----->>>  ----->>>  ----->>>  ----->>>  ----->>>
201      101      202      1101      104      203      1102      107
1103     105     302     303     1202     108     1203     109
306      1206     206     1106     106     305     1205     102
301      1201     205     1105     103     304     1204     204
1104

```

```

MAXIMUM FRONT: (NODAL =      6) - (ADDITIONAL FREEDOMS =      0)
+++++

```

```

      I N I T I A L   L O A D I N G
      +++++

```

| OUTPUT<br>ITERATIONS | INITIAL<br>LOADING<br>FACTOR | CURRENT<br>TIME | LEVEL | CONV.-NORM |   |
|----------------------|------------------------------|-----------------|-------|------------|---|
| 1                    | 0.10000000E+01               | 0.18000000E+02  | 0     | 0.498E-07  | 1 |

```

      V A R I A B L E   L O A D I N G
      +++++

```

| OUTPUT | CURRENT<br>TIME | LEVEL | CONV.-NORM | ITERATIONS |
|--------|-----------------|-------|------------|------------|
| 0      | 0.18004000E+02  | 0     | 0.595E-05  | 0          |
| 2      | 0.18008000E+02  | 0     | 0.619E-05  | 0          |
| 0      | 0.18012000E+02  | 0     | 0.663E-05  | 0          |
| 3      | 0.18016000E+02  | 0     | 0.728E-05  | 0          |
| 0      | 0.18020000E+02  | 0     | 0.795E-05  | 0          |
| 4      | 0.18024000E+02  | 0     | 0.841E-05  | 0          |
| 0      | 0.18028000E+02  | 0     | 0.856E-05  | 0          |
| 5      | 0.18032000E+02  | 0     | 0.843E-05  | 0          |

```

***** ( SUBDIVISION OF ELEMENT 202 ) *****
*
*NUMBER OF NODES CREATED
*      1
* NOD.NAME      COORD'S (X,Y) RELATIVE TO END(1) OF SUBDIVIDED ELEMENT
* #n1           0.000000E+00           0.400000E+03
*-----*
*
*NUMBER OF ELEMENTS CREATED
*      2
* ELM.NAME      TYPE.OF.ELEMENT      NOD.NAMES
* #e1           cbp2                 111      #n1
* #e2           qdp2                 #n1      121
*-----*
*
*NUMBER OF IMPERFECT ELEMENTS
*      0
*****

```

|   |                |   |           |   |
|---|----------------|---|-----------|---|
| 0 | 0.18036000E+02 | 0 | 0.140E-03 | 0 |
| 6 | 0.18040000E+02 | 0 | 0.652E-05 | 1 |
| 0 | 0.18044000E+02 | 0 | 0.110E-05 | 1 |

```

***** ( SUBDIVISION OF ELEMENT #e2 )*****
*
*NUMBER OF NODES CREATED
*
*      1
* NOD.NAME      COORD'S (X,Y) RELATIVE TO END(1) OF SUBDIVIDED ELEMENT
* #n2           0.000000E+00           0.320000E+04
*-----*
*
*NUMBER OF ELEMENTS CREATED
*
*      2
* ELM.NAME      TYPE.OF.ELEMENT      NOD.NAMES
* #e4           cbp2                 #n2      121
* #e3           qdp2                 #n1      #n2
*-----*
*
*NUMBER OF IMPERFECT ELEMENTS
*
*      0
*****

```

|    |                |   |           |   |
|----|----------------|---|-----------|---|
| 7  | 0.18048000E+02 | 0 | 0.168E-04 | 1 |
| 0  | 0.18052000E+02 | 0 | 0.367E-04 | 1 |
| 8  | 0.18056000E+02 | 0 | 0.155E-03 | 1 |
| 0  | 0.18060000E+02 | 0 | 0.157E-03 | 1 |
| 9  | 0.18064000E+02 | 0 | 0.408E-03 | 1 |
| 0  | 0.18068000E+02 | 0 | 0.233E-05 | 2 |
| 10 | 0.18072000E+02 | 0 | 0.100E-04 | 2 |

```

***** ( SUBDIVISION OF ELEMENT #e3 )*****
*
*NUMBER OF NODES CREATED
*
*      3
* NOD.NAME      COORD'S (X,Y) RELATIVE TO END(1) OF SUBDIVIDED ELEMENT
* #n3           0.000000E+00           0.120000E+04
* #n4           0.000000E+00           0.160000E+04
* #n5           0.000000E+00           0.200000E+04
*-----*
*
*NUMBER OF ELEMENTS CREATED
*
*      4
* ELM.NAME      TYPE.OF.ELEMENT      NOD.NAMES
* #e6           cbp2                 #n3      #n4
* #e7           cbp2                 #n4      #n5
* #e5           qdp2                 #n1      #n3
* #e8           qdp2                 #n5      #n2
*-----*
*
*NUMBER OF IMPERFECT ELEMENTS
*
*      0
*****

```

|    |                |   |           |   |
|----|----------------|---|-----------|---|
| 0  | 0.18076000E+02 | 0 | 0.638E-04 | 2 |
| 11 | 0.18080000E+02 | 0 | 0.130E-03 | 2 |
| 0  | 0.18084000E+02 | 0 | 0.293E-03 | 2 |

```

***** ( SUBDIVISION OF ELEMENT #e5 )*****
*
*NUMBER OF NODES CREATED
*
*      1
* NOD.NAME      COORD'S (X,Y) RELATIVE TO END(1) OF SUBDIVIDED ELEMENT
* #n6           0.000000E+00           0.800000E+03
*-----*

```

```

*
*NUMBER OF ELEMENTS CREATED
*
*      2
* ELM.NAME      TYPE.OF.ELEMENT      NOD.NAMES
* #e10          cbp2                  #n6      #n3
* #e9           qdp2                  #n1      #n6
*-----*
*
*NUMBER OF IMPERFECT ELEMENTS
*
*      0
*****

***** ( SUBDIVISION OF ELEMENT #e8 )*****
*
*NUMBER OF NODES CREATED
*
*      1
* NOD.NAME      COORD'S (X,Y) RELATIVE TO END(1) OF SUBDIVIDED ELEMENT
* #n7           0.000000E+00          0.400000E+03
*-----*
*
*NUMBER OF ELEMENTS CREATED
*
*      2
* ELM.NAME      TYPE.OF.ELEMENT      NOD.NAMES
* #e11          cbp2                  #n5      #n7
* #e12          qdp2                  #n7      #n2
*-----*
*
*NUMBER OF IMPERFECT ELEMENTS
*
*      0
*****

12      0.18088000E+02      0      0.759E-05      3
0       0.18092000E+02      0      0.453E-03      2
13      0.18096000E+02      0      0.240E-05      3
0       0.18100000E+02      0      0.107E-04      3

***** ( SUBDIVISION OF ELEMENT 302 )*****
*
*NUMBER OF NODES CREATED
*
*      1
* NOD.NAME      COORD'S (X,Y) RELATIVE TO END(1) OF SUBDIVIDED ELEMENT
* #n8           0.000000E+00          0.400000E+03
*-----*
*
*NUMBER OF ELEMENTS CREATED
*
*      2
* ELM.NAME      TYPE.OF.ELEMENT      NOD.NAMES
* #e13          cbp2                  211      #n8
* #e14          qdp2                  #n8      221
*-----*
*
*NUMBER OF IMPERFECT ELEMENTS
*
*      0
*****

14      0.18104000E+02      0      0.322E-04      3

***** ( SUBDIVISION OF ELEMENT #e14 )*****
*
*NUMBER OF NODES CREATED

```

```

*          1
* NOD.NAME      COORD'S (X,Y) RELATIVE TO END(1) OF SUBDIVIDED ELEMENT
* #n9              0.000000E+00          0.320000E+04
*-----*
*
*NUMBER OF ELEMENTS CREATED
*          2
* ELM.NAME      TYPE.OF.ELEMENT          NOD.NAMES
* #e16          cbp2                    #n9      221
* #e15          qdp2                    #n8      #n9
*-----*
*
*NUMBER OF IMPERFECT ELEMENTS
*          0
*****
0          0.18108000E+02      0          0.335E-04      3

***** ( SUBDIVISION OF ELEMENT #e9 )*****
*
*NUMBER OF NODES CREATED
*          1
* NOD.NAME      COORD'S (X,Y) RELATIVE TO END(1) OF SUBDIVIDED ELEMENT
* #n10           0.000000E+00          0.400000E+03
*-----*
*
*NUMBER OF ELEMENTS CREATED
*          2
* ELM.NAME      TYPE.OF.ELEMENT          NOD.NAMES
* #e18          cbp2                    #n10     #n6
* #e17          qdp2                    #n1      #n10
*-----*
*
*NUMBER OF IMPERFECT ELEMENTS
*          0
*****

***** ( SUBDIVISION OF ELEMENT #e12 )*****
*
*NUMBER OF NODES CREATED
*          1
* NOD.NAME      COORD'S (X,Y) RELATIVE TO END(1) OF SUBDIVIDED ELEMENT
* #n11           0.000000E+00          0.400000E+03
*-----*
*
*NUMBER OF ELEMENTS CREATED
*          2
* ELM.NAME      TYPE.OF.ELEMENT          NOD.NAMES
* #e19          cbp2                    #n7      #n11
* #e20          qdp2                    #n11     #n2
*-----*
*
*NUMBER OF IMPERFECT ELEMENTS
*          0
*****
15         0.18112000E+02      0          0.480E-04      3
0          0.18116000E+02      0          0.267E-04      3
16         0.18120000E+02      0          0.205E-04      3
0          0.18124000E+02      0          0.583E-04      2

```

|    |                |   |           |   |
|----|----------------|---|-----------|---|
| 17 | 0.18128000E+02 | 0 | 0.485E-03 | 2 |
| 0  | 0.18132000E+02 | 0 | 0.323E-03 | 1 |
| 18 | 0.18136000E+02 | 0 | 0.595E-04 | 1 |
| 0  | 0.18140000E+02 | 0 | 0.148E-04 | 1 |
| 19 | 0.18144000E+02 | 0 | 0.385E-05 | 1 |
| 0  | 0.18148000E+02 | 0 | 0.551E-05 | 1 |
| 20 | 0.18152000E+02 | 0 | 0.290E-04 | 1 |
| 0  | 0.18156000E+02 | 0 | 0.206E-03 | 0 |
| 21 | 0.18160000E+02 | 0 | 0.119E-03 | 0 |
| 0  | 0.18164000E+02 | 0 | 0.837E-04 | 0 |
| 22 | 0.18168000E+02 | 0 | 0.171E-03 | 0 |
| 0  | 0.18172000E+02 | 0 | 0.458E-04 | 1 |
| 23 | 0.18176000E+02 | 0 | 0.268E-04 | 1 |
| 0  | 0.18180000E+02 | 0 | 0.398E-03 | 1 |
| 24 | 0.18184000E+02 | 0 | 0.270E-06 | 2 |
| 0  | 0.18188000E+02 | 0 | 0.204E-05 | 2 |
| 25 | 0.18192000E+02 | 0 | 0.165E-06 | 2 |
| 0  | 0.18196000E+02 | 0 | 0.200E-03 | 1 |
| 26 | 0.18200000E+02 | 0 | 0.560E-04 | 1 |
| 0  | 0.18240000E+02 | 0 | 0.569E-04 | 3 |
| 27 | 0.18280000E+02 | 0 | 0.263E-04 | 2 |
| 0  | 0.18320000E+02 | 0 | 0.184E-05 | 1 |
| 28 | 0.18360000E+02 | 0 | 0.186E-03 | 0 |
| 0  | 0.18400000E+02 | 0 | 0.269E-06 | 1 |
| 29 | 0.18440000E+02 | 0 | 0.133E-05 | 1 |
| 0  | 0.18480000E+02 | 0 | 0.314E-06 | 1 |
| 30 | 0.18520000E+02 | 0 | 0.474E-04 | 0 |
| 0  | 0.18560000E+02 | 0 | 0.126E-06 | 1 |
| 31 | 0.18600000E+02 | 0 | 0.352E-06 | 1 |
| 0  | 0.18640000E+02 | 0 | 0.551E-07 | 1 |
| 32 | 0.18680000E+02 | 0 | 0.353E-04 | 0 |
| 0  | 0.18720000E+02 | 0 | 0.389E-07 | 1 |
| 33 | 0.18760000E+02 | 0 | 0.106E-06 | 1 |
| 0  | 0.18800000E+02 | 0 | 0.457E-03 | 0 |
| 34 | 0.18840000E+02 | 0 | 0.379E-04 | 0 |
| 0  | 0.18880000E+02 | 0 | 0.493E-03 | 0 |
| 35 | 0.18920000E+02 | 0 | 0.438E-07 | 1 |
| 0  | 0.18960000E+02 | 0 | 0.266E-03 | 0 |
| 36 | 0.19000000E+02 | 0 | 0.312E-04 | 0 |
| 0  | 0.19040000E+02 | 0 | 0.340E-03 | 0 |
| 37 | 0.19080000E+02 | 0 | 0.487E-03 | 0 |
| 0  | 0.19120000E+02 | 0 | 0.153E-03 | 0 |
| 38 | 0.19160000E+02 | 0 | 0.215E-04 | 0 |
| 0  | 0.19200000E+02 | 0 | 0.281E-03 | 0 |
| 39 | 0.19240000E+02 | 0 | 0.314E-03 | 0 |
| 0  | 0.19280000E+02 | 0 | 0.669E-04 | 0 |
| 40 | 0.19320000E+02 | 0 | 0.366E-04 | 0 |
| 0  | 0.19360000E+02 | 0 | 0.213E-03 | 0 |
| 41 | 0.19400000E+02 | 0 | 0.202E-03 | 0 |
| 0  | 0.19440000E+02 | 0 | 0.386E-04 | 0 |
| 42 | 0.19480000E+02 | 0 | 0.513E-04 | 0 |
| 0  | 0.19520000E+02 | 0 | 0.166E-03 | 0 |
| 43 | 0.19560000E+02 | 0 | 0.121E-03 | 0 |
| 0  | 0.19600000E+02 | 0 | 0.169E-04 | 0 |
| 44 | 0.19640000E+02 | 0 | 0.403E-04 | 0 |
| 0  | 0.19680000E+02 | 0 | 0.101E-03 | 0 |
| 45 | 0.19720000E+02 | 0 | 0.577E-04 | 0 |
| 0  | 0.19760000E+02 | 0 | 0.432E-05 | 0 |
| 46 | 0.19800000E+02 | 0 | 0.375E-04 | 0 |
| 0  | 0.19840000E+02 | 0 | 0.756E-04 | 0 |
| 47 | 0.19880000E+02 | 0 | 0.458E-04 | 0 |

|    |                |   |           |   |
|----|----------------|---|-----------|---|
| 0  | 0.19920000E+02 | 0 | 0.248E-04 | 0 |
| 48 | 0.19960000E+02 | 0 | 0.497E-04 | 0 |
| 0  | 0.20000000E+02 | 0 | 0.621E-04 | 0 |
| 49 | 0.30000000E+02 | 0 | 0.216E-03 | 0 |
| 0  | 0.40000000E+02 | 0 | 0.227E-03 | 0 |
| 50 | 0.50000000E+02 | 0 | 0.184E-03 | 0 |
| 0  | 0.60000000E+02 | 0 | 0.191E-03 | 0 |
| 51 | 0.70000000E+02 | 0 | 0.197E-03 | 0 |
| 0  | 0.80000000E+02 | 0 | 0.189E-03 | 0 |
| 52 | 0.90000000E+02 | 0 | 0.187E-03 | 0 |
| 0  | 0.10000000E+03 | 0 | 0.187E-03 | 0 |
| 53 | 0.11000000E+03 | 0 | 0.180E-03 | 0 |
| 0  | 0.12000000E+03 | 0 | 0.183E-03 | 0 |
| 54 | 0.13000000E+03 | 0 | 0.183E-03 | 0 |
| 0  | 0.14000000E+03 | 0 | 0.181E-03 | 0 |
| 55 | 0.15000000E+03 | 0 | 0.178E-03 | 0 |
| 0  | 0.16000000E+03 | 0 | 0.175E-03 | 0 |
| 56 | 0.17000000E+03 | 0 | 0.173E-03 | 0 |
| 0  | 0.18000000E+03 | 0 | 0.171E-03 | 0 |
| 57 | 0.19000000E+03 | 0 | 0.170E-03 | 0 |
| 0  | 0.20000000E+03 | 0 | 0.169E-03 | 0 |
| 58 | 0.21000000E+03 | 0 | 0.166E-03 | 0 |
| 0  | 0.22000000E+03 | 0 | 0.164E-03 | 0 |
| 59 | 0.23000000E+03 | 0 | 0.162E-03 | 0 |
| 0  | 0.24000000E+03 | 0 | 0.161E-03 | 0 |
| 60 | 0.25000000E+03 | 0 | 0.160E-03 | 0 |
| 0  | 0.26000000E+03 | 0 | 0.158E-03 | 0 |
| 61 | 0.27000000E+03 | 0 | 0.156E-03 | 0 |
| 0  | 0.28000000E+03 | 0 | 0.154E-03 | 0 |
| 62 | 0.29000000E+03 | 0 | 0.152E-03 | 0 |
| 0  | 0.30000000E+03 | 0 | 0.151E-03 | 0 |
| 63 | 0.31000000E+03 | 0 | 0.149E-03 | 0 |
| 0  | 0.32000000E+03 | 0 | 0.148E-03 | 0 |
| 64 | 0.33000000E+03 | 0 | 0.146E-03 | 0 |
| 0  | 0.34000000E+03 | 0 | 0.144E-03 | 0 |

\*\*\*\*\* ( SUBDIVISION OF ELEMENT 104 )\*\*\*\*\*

```

*
*NUMBER OF NODES CREATED
*
*          9
* NOD.NAME      COORD'S (X,Y) RELATIVE TO END(1) OF SUBDIVIDED ELEMENT
* #n12          0.600000E+03      0.000000E+00
* #n13          0.120000E+04      0.000000E+00
* #n14          0.180000E+04      0.000000E+00
* #n15          0.240000E+04      0.000000E+00
* #n16          0.300000E+04      0.000000E+00
* #n17          0.360000E+04      0.000000E+00
* #n18          0.420000E+04      0.000000E+00
* #n19          0.480000E+04      0.000000E+00
* #n20          0.540000E+04      0.000000E+00
*-----*
*
*NUMBER OF ELEMENTS CREATED
*
*          10
* ELM.NAME      TYPE OF ELEMENT      NOD.NAMES
* #e21          cbp2          121      #n12
* #e22          cbp2          #n12      #n13
* #e23          cbp2          #n13      #n14
* #e24          cbp2          #n14      #n15
* #e25          cbp2          #n15      #n16
* #e26          cbp2          #n16      #n17

```

```

* #e27          cbp2          #n17          #n18          *
* #e28          cbp2          #n18          #n19          *
* #e29          cbp2          #n19          #n20          *
* #e30          cbp2          #n20          221          *

```

```

-----*
*
*NUMBER OF IMPERFECT ELEMENTS
*          0
*****

```

|    |                |   |           |   |
|----|----------------|---|-----------|---|
| 0  | 0.34100000E+03 | 1 | 0.265E-06 | 1 |
| 0  | 0.34200000E+03 | 1 | 0.310E-05 | 0 |
| 0  | 0.34300000E+03 | 1 | 0.311E-05 | 0 |
| 0  | 0.34400000E+03 | 1 | 0.308E-05 | 0 |
| 0  | 0.34500000E+03 | 1 | 0.295E-05 | 0 |
| 0  | 0.34600000E+03 | 1 | 0.290E-05 | 0 |
| 0  | 0.34700000E+03 | 1 | 0.294E-05 | 0 |
| 0  | 0.34800000E+03 | 1 | 0.302E-05 | 0 |
| 0  | 0.34900000E+03 | 1 | 0.303E-05 | 0 |
| 65 | 0.35000000E+03 | 1 | 0.299E-05 | 0 |
| 0  | 0.36000000E+03 | 0 | 0.153E-06 | 1 |
| 66 | 0.37000000E+03 | 0 | 0.289E-03 | 0 |
| 0  | 0.38000000E+03 | 0 | 0.284E-03 | 0 |
| 67 | 0.39000000E+03 | 0 | 0.281E-03 | 0 |
| 0  | 0.40000000E+03 | 0 | 0.311E-06 | 1 |

```

***** ( SUBDIVISION OF ELEMENT #e17 )*****

```

```

*
*NUMBER OF NODES CREATED
*          0

```

```

-----*
*
*NUMBER OF ELEMENTS CREATED
*          1
* ELM.NAME      TYPE.OF.ELEMENT      NOD.NAMES
* #e31          cbp2          #n1          #n10

```

```

-----*
*
*NUMBER OF IMPERFECT ELEMENTS
*          0
*****

```

```

***** ( SUBDIVISION OF ELEMENT #e20 )*****

```

```

*
*NUMBER OF NODES CREATED
*          0

```

```

-----*
*
*NUMBER OF ELEMENTS CREATED
*          1
* ELM.NAME      TYPE.OF.ELEMENT      NOD.NAMES
* #e32          cbp2          #n11         #n2

```

```

-----*
*
*NUMBER OF IMPERFECT ELEMENTS
*          0
*****

```

|   |                |   |           |   |
|---|----------------|---|-----------|---|
| 0 | 0.40100000E+03 | 1 | 0.149E-07 | 2 |
| 0 | 0.40200000E+03 | 1 | 0.317E-03 | 0 |



|    |                |   |           |   |
|----|----------------|---|-----------|---|
| 0  | 0.40300000E+03 | 1 | 0.268E-05 | 0 |
| 0  | 0.40400000E+03 | 1 | 0.269E-05 | 0 |
| 0  | 0.40500000E+03 | 1 | 0.276E-05 | 0 |
| 0  | 0.40600000E+03 | 1 | 0.286E-05 | 0 |
| 0  | 0.40700000E+03 | 1 | 0.286E-05 | 0 |
| 0  | 0.40800000E+03 | 1 | 0.276E-05 | 0 |
| 0  | 0.40900000E+03 | 1 | 0.269E-05 | 0 |
| 68 | 0.41000000E+03 | 1 | 0.268E-05 | 0 |
| 0  | 0.42000000E+03 | 0 | 0.731E-08 | 1 |

\*\*\*\*\* ( SUBDIVISION OF ELEMENT #e15 )\*\*\*\*\*

\* \* \* \* \*

\*NUMBER OF NODES CREATED \* \*

\* 1 \* \*

\* NOD.NAME COORD'S (X,Y) RELATIVE TO END(1) OF SUBDIVIDED ELEMENT \* \*

\* #n21 0.000000E+00 0.280000E+04 \* \*

\*-----\* \*

\* \* \* \* \*

\*NUMBER OF ELEMENTS CREATED \* \*

\* 2 \* \*

\* ELM.NAME TYPE.OF.ELEMENT NOD.NAMES \* \*

\* #e34 cbp2 #n21 #n9 \* \*

\* #e33 qdp2 #n8 #n21 \* \*

\*-----\* \*

\* \* \* \* \*

\*NUMBER OF IMPERFECT ELEMENTS \* \*

\* 0 \* \*

\*\*\*\*\*

|    |                |   |           |   |
|----|----------------|---|-----------|---|
| 0  | 0.42100000E+03 | 1 | 0.378E-07 | 3 |
| 0  | 0.42200000E+03 | 1 | 0.342E-04 | 1 |
| 0  | 0.42300000E+03 | 1 | 0.659E-07 | 1 |
| 0  | 0.42400000E+03 | 1 | 0.533E-08 | 1 |
| 0  | 0.42500000E+03 | 1 | 0.528E-08 | 1 |
| 0  | 0.42600000E+03 | 1 | 0.884E-09 | 1 |
| 0  | 0.42700000E+03 | 1 | 0.395E-08 | 1 |
| 0  | 0.42800000E+03 | 1 | 0.672E-08 | 1 |
| 0  | 0.42900000E+03 | 1 | 0.113E-08 | 1 |
| 69 | 0.43000000E+03 | 1 | 0.609E-07 | 1 |

\*\*\*\*\* ( SUBDIVISION OF ELEMENT #e33 )\*\*\*\*\*

\* \* \* \* \*

\*NUMBER OF NODES CREATED \* \*

\* 1 \* \*

\* NOD.NAME COORD'S (X,Y) RELATIVE TO END(1) OF SUBDIVIDED ELEMENT \* \*

\* #n22 0.000000E+00 0.400000E+03 \* \*

\*-----\* \*

\* \* \* \* \*

\*NUMBER OF ELEMENTS CREATED \* \*

\* 2 \* \*

\* ELM.NAME TYPE.OF.ELEMENT NOD.NAMES \* \*

\* #e35 cbp2 #n8 #n22 \* \*

\* #e36 qdp2 #n22 #n21 \* \*

\*-----\* \*

\* \* \* \* \*

\*NUMBER OF IMPERFECT ELEMENTS \* \*

\* 0 \* \*

\*\*\*\*\*

|   |                |   |           |   |
|---|----------------|---|-----------|---|
| 0 | 0.43100000E+03 | 1 | 0.130E-03 | 3 |
| 0 | 0.43200000E+03 | 1 | 0.383E-08 | 1 |

|   |                |   |           |   |
|---|----------------|---|-----------|---|
| 0 | 0.43300000E+03 | 1 | 0.133E-08 | 1 |
| 0 | 0.43400000E+03 | 1 | 0.281E-08 | 1 |
| 0 | 0.43500000E+03 | 1 | 0.191E-08 | 1 |
| 0 | 0.43600000E+03 | 1 | 0.203E-08 | 1 |
| 0 | 0.43700000E+03 | 1 | 0.185E-08 | 1 |
| 0 | 0.43800000E+03 | 1 | 0.283E-08 | 1 |
| 0 | 0.43900000E+03 | 1 | 0.467E-03 | 0 |
| 0 | 0.44000000E+03 | 1 | 0.152E-05 | 1 |

\*\*\*\*\* ( SUBDIVISION OF ELEMENT #e36 )\*\*\*\*\*

\* \* \* \* \*

\*NUMBER OF NODES CREATED \* \*

\* 1 \* \*

\* NOD.NAME COORD'S (X,Y) RELATIVE TO END(1) OF SUBDIVIDED ELEMENT \* \*

\* #n23 0.000000E+00 0.200000E+04 \* \*

\*-----\* \*

\* \* \* \* \*

\*NUMBER OF ELEMENTS CREATED \* \*

\* 2 \* \*

\* ELM.NAME TYPE.OF.ELEMENT NOD.NAMES \* \*

\* #e38 cbp2 #n23 #n21 \* \*

\* #e37 qdp2 #n22 #n23 \* \*

\*-----\* \*

\* \* \* \* \*

\*NUMBER OF IMPERFECT ELEMENTS \* \*

\* 0 \* \*

\*\*\*\*\*

|    |                |   |           |   |
|----|----------------|---|-----------|---|
| 0  | 0.44100000E+03 | 1 | 0.397E-04 | 2 |
| 0  | 0.44200000E+03 | 1 | 0.335E-03 | 0 |
| 0  | 0.44300000E+03 | 1 | 0.354E-03 | 0 |
| 0  | 0.44400000E+03 | 1 | 0.334E-03 | 0 |
| 0  | 0.44500000E+03 | 1 | 0.215E-05 | 2 |
| 0  | 0.44600000E+03 | 1 | 0.458E-08 | 1 |
| 0  | 0.44700000E+03 | 1 | 0.387E-03 | 0 |
| 0  | 0.44800000E+03 | 1 | 0.520E-08 | 1 |
| 0  | 0.44900000E+03 | 1 | 0.233E-05 | 1 |
| 70 | 0.45000000E+03 | 1 | 0.458E-03 | 0 |

\*\*\*\*\* ( SUBDIVISION OF ELEMENT #e37 )\*\*\*\*\*

\* \* \* \* \*

\*NUMBER OF NODES CREATED \* \*

\* 2 \* \*

\* NOD.NAME COORD'S (X,Y) RELATIVE TO END(1) OF SUBDIVIDED ELEMENT \* \*

\* #n24 0.000000E+00 0.400000E+03 \* \*

\* #n25 0.000000E+00 0.160000E+04 \* \*

\*-----\* \*

\* \* \* \* \*

\*NUMBER OF ELEMENTS CREATED \* \*

\* 3 \* \*

\* ELM.NAME TYPE.OF.ELEMENT NOD.NAMES \* \*

\* #e39 cbp2 #n22 #n24 \* \*

\* #e41 cbp2 #n25 #n23 \* \*

\* #e40 qdp2 #n24 #n25 \* \*

\*-----\* \*

\* \* \* \* \*

\*NUMBER OF IMPERFECT ELEMENTS \* \*

\* 0 \* \*

\*\*\*\*\*

|   |                |   |           |   |
|---|----------------|---|-----------|---|
| 0 | 0.45010000E+03 | 2 | 0.215E-03 | 1 |
|---|----------------|---|-----------|---|

|   |                |   |           |   |
|---|----------------|---|-----------|---|
| 0 | 0.45020000E+03 | 2 | 0.187E-04 | 0 |
| 0 | 0.45030000E+03 | 2 | 0.925E-07 | 0 |
| 0 | 0.45040000E+03 | 2 | 0.434E-05 | 0 |
| 0 | 0.45050000E+03 | 2 | 0.919E-07 | 0 |
| 0 | 0.45060000E+03 | 2 | 0.911E-07 | 0 |
| 0 | 0.45070000E+03 | 2 | 0.420E-04 | 0 |
| 0 | 0.45080000E+03 | 2 | 0.926E-07 | 0 |
| 0 | 0.45090000E+03 | 2 | 0.136E-04 | 0 |
| 0 | 0.45100000E+03 | 2 | 0.929E-07 | 0 |
| 0 | 0.45200000E+03 | 1 | 0.846E-08 | 1 |
| 0 | 0.45300000E+03 | 1 | 0.118E-04 | 1 |
| 0 | 0.45400000E+03 | 1 | 0.431E-03 | 1 |
| 0 | 0.45500000E+03 | 1 | 0.371E-04 | 1 |
| 0 | 0.45600000E+03 | 1 | 0.477E-04 | 1 |
| 0 | 0.45700000E+03 | 1 | 0.692E-04 | 1 |
| 0 | 0.45800000E+03 | 1 | 0.181E-04 | 2 |
| 0 | 0.45900000E+03 | 1 | 0.133E-03 | 2 |
| 0 | 0.46000000E+03 | 1 | 0.440E-03 | 1 |
| 0 | 0.46010000E+03 | 2 | 0.359E-04 | 3 |
| 0 | 0.46020000E+03 | 2 | 0.134E-04 | 0 |
| 0 | 0.46030000E+03 | 2 | 0.779E-05 | 0 |
| 0 | 0.46040000E+03 | 2 | 0.321E-04 | 0 |
| 0 | 0.46050000E+03 | 2 | 0.131E-04 | 0 |
| 0 | 0.46060000E+03 | 2 | 0.603E-04 | 0 |
| 0 | 0.46070000E+03 | 2 | 0.226E-04 | 0 |
| 0 | 0.46080000E+03 | 2 | 0.163E-04 | 0 |
| 0 | 0.46090000E+03 | 2 | 0.240E-04 | 0 |
| 0 | 0.46100000E+03 | 2 | 0.591E-04 | 0 |

```

***** ( SUBDIVISION OF ELEMENT #e40 )*****
*
*NUMBER OF NODES CREATED
* 1
* NOD.NAME      COORD'S (X,Y) RELATIVE TO END(1) OF SUBDIVIDED ELEMENT
* #n26          0.000000E+00      0.400000E+03
*-----*
*
*NUMBER OF ELEMENTS CREATED
* 2
* ELM.NAME      TYPE OF ELEMENT      NOD.NAMES
* #e42          cbp2                  #n24      #n26
* #e43          qdp2                  #n26      #n25
*-----*
*
*NUMBER OF IMPERFECT ELEMENTS
* 0
*****

```

|   |                |   |           |   |
|---|----------------|---|-----------|---|
| 0 | 0.46110000E+03 | 2 | 0.357E-05 | 2 |
| 0 | 0.46120000E+03 | 2 | 0.197E-03 | 0 |
| 0 | 0.46130000E+03 | 2 | 0.300E-03 | 0 |
| 0 | 0.46140000E+03 | 2 | 0.796E-04 | 1 |
| 0 | 0.46150000E+03 | 2 | 0.675E-04 | 0 |
| 0 | 0.46160000E+03 | 2 | 0.607E-04 | 0 |
| 0 | 0.46170000E+03 | 2 | 0.630E-04 | 0 |
| 0 | 0.46180000E+03 | 2 | 0.707E-04 | 0 |
| 0 | 0.46190000E+03 | 2 | 0.524E-04 | 0 |
| 0 | 0.46200000E+03 | 2 | 0.911E-04 | 0 |
| 0 | 0.46300000E+03 | 1 | 0.232E-04 | 2 |
| 0 | 0.46400000E+03 | 1 | 0.203E-05 | 1 |

```

***** ( SUBDIVISION OF ELEMENT #e43 )*****
*
*NUMBER OF NODES CREATED
*      1
* NOD.NAME      COORD'S (X,Y) RELATIVE TO END(1) OF SUBDIVIDED ELEMENT
* #n27          0.000000E+00          0.400000E+03
*-----*
*
*NUMBER OF ELEMENTS CREATED
*      2
* ELM.NAME      TYPE.OF.ELEMENT      NOD.NAMES
* #e45          cbp2                  #n27      #n25
* #e44          qdp2                  #n26      #n27
*-----*
*
*NUMBER OF IMPERFECT ELEMENTS
*      0
*****
0      0.46410000E+03      2      0.417E-05      2
0      0.46420000E+03      2      0.278E-03      0
0      0.46430000E+03      2      0.177E-03      0
0      0.46440000E+03      2      0.210E-03      0
0      0.46450000E+03      2      0.151E-03      0
0      0.46460000E+03      2      0.123E-03      0
0      0.46470000E+03      2      0.111E-03      0
0      0.46480000E+03      2      0.123E-03      0
0      0.46490000E+03      2      0.119E-03      0
0      0.46500000E+03      2      0.126E-03      0
0      0.46600000E+03      1      0.846E-04      2

***** ( SUBDIVISION OF ELEMENT #e44 )*****
*
*NUMBER OF NODES CREATED
*      0
*-----*
*
*NUMBER OF ELEMENTS CREATED
*      1
* ELM.NAME      TYPE.OF.ELEMENT      NOD.NAMES
* #e46          cbp2                  #n26      #n27
*-----*
*
*NUMBER OF IMPERFECT ELEMENTS
*      0
*****
0      0.46601000E+03      3      0.131E-03      1
0      0.46602000E+03      3      0.357E-04      0
0      0.46603000E+03      3      0.122E-04      0
0      0.46604000E+03      3      0.252E-05      0
0      0.46605000E+03      3      0.347E-05      0
0      0.46606000E+03      3      0.303E-07      0
0      0.46607000E+03      3      0.305E-07      0
0      0.46608000E+03      3      0.160E-05      0
0      0.46609000E+03      3      0.115E-06      0
0      0.46610000E+03      3      0.443E-05      0
0      0.46620000E+03      2      0.458E-03      0
0      0.46630000E+03      2      0.158E-03      0
0      0.46640000E+03      2      0.109E-03      0
0      0.46650000E+03      2      0.410E-04      0

```

|    |                |   |           |   |
|----|----------------|---|-----------|---|
| 0  | 0.46660000E+03 | 2 | 0.379E-03 | 0 |
| 0  | 0.46670000E+03 | 2 | 0.180E-04 | 0 |
| 0  | 0.46680000E+03 | 2 | 0.307E-04 | 0 |
| 0  | 0.46690000E+03 | 2 | 0.365E-04 | 0 |
| 0  | 0.46700000E+03 | 2 | 0.321E-03 | 0 |
| 0  | 0.46800000E+03 | 1 | 0.774E-04 | 4 |
| 0  | 0.46900000E+03 | 1 | 0.433E-03 | 2 |
| 71 | 0.47000000E+03 | 1 | 0.504E-04 | 3 |
| 0  | 0.48000000E+03 | 0 | 0.473E-04 | 5 |
| 72 | 0.49000000E+03 | 0 | 0.105E-03 | 2 |
| 0  | 0.50000000E+03 | 0 | 0.767E-05 | 2 |
| 73 | 0.51000000E+03 | 0 | 0.289E-05 | 2 |
| 0  | 0.52000000E+03 | 0 | 0.720E-06 | 2 |
| 74 | 0.53000000E+03 | 0 | 0.210E-06 | 2 |
| 0  | 0.54000000E+03 | 0 | 0.773E-07 | 2 |
| 75 | 0.55000000E+03 | 0 | 0.380E-03 | 1 |
| 0  | 0.56000000E+03 | 0 | 0.103E-06 | 2 |
| 76 | 0.57000000E+03 | 0 | 0.742E-04 | 2 |
| 0  | 0.58000000E+03 | 0 | 0.180E-03 | 1 |
| 77 | 0.59000000E+03 | 0 | 0.262E-03 | 1 |
| 0  | 0.60000000E+03 | 0 | 0.963E-07 | 2 |
| 78 | 0.61000000E+03 | 0 | 0.798E-06 | 2 |
| 0  | 0.62000000E+03 | 0 | 0.483E-07 | 2 |
| 79 | 0.63000000E+03 | 0 | 0.241E-07 | 2 |
| 0  | 0.64000000E+03 | 0 | 0.165E-04 | 3 |
| 0  | 0.64010000E+03 | 1 | 0.574E-04 | 1 |
| 0  | 0.64020000E+03 | 1 | 0.274E-04 | 0 |
| 0  | 0.64030000E+03 | 1 | 0.367E-04 | 0 |
| 0  | 0.64040000E+03 | 1 | 0.140E-05 | 1 |
| 0  | 0.64050000E+03 | 1 | 0.246E-03 | 0 |
| 0  | 0.64060000E+03 | 1 | 0.399E-03 | 1 |
| 0  | 0.64070000E+03 | 1 | 0.242E-04 | 1 |
| 0  | 0.64080000E+03 | 1 | 0.150E-05 | 1 |
| 0  | 0.64090000E+03 | 1 | 0.275E-05 | 1 |
| 80 | 0.64100000E+03 | 1 | 0.502E-04 | 1 |
| 0  | 0.64110000E+03 | 1 | 0.293E-03 | 1 |
| 0  | 0.64120000E+03 | 1 | 0.406E-04 | 1 |
| 0  | 0.64130000E+03 | 1 | 0.410E-03 | 1 |
| 0  | 0.64140000E+03 | 1 | 0.265E-03 | 2 |
| 0  | 0.64150000E+03 | 1 | 0.437E-05 | 3 |
| 0  | 0.64160000E+03 | 1 | 0.217E-05 | 4 |
| 0  | 0.64161000E+03 | 2 | 0.495E-03 | 3 |
| 0  | 0.64162000E+03 | 2 | 0.500E-04 | 2 |
| 0  | 0.64163000E+03 | 2 | 0.807E-04 | 2 |
| 0  | 0.64164000E+03 | 2 | 0.416E-04 | 2 |
| 0  | 0.64165000E+03 | 2 | 0.555E-04 | 2 |
| 0  | 0.64166000E+03 | 2 | 0.386E-03 | 1 |
| 0  | 0.64167000E+03 | 2 | 0.288E-04 | 2 |
| 0  | 0.64168000E+03 | 2 | 0.111E-07 | 3 |
| 0  | 0.64169000E+03 | 2 | 0.387E-04 | 1 |
| 0  | 0.64170000E+03 | 2 | 0.147E-03 | 1 |
| 0  | 0.64171000E+03 | 2 | 0.355E-04 | 3 |

\*\*\*\*\* ( SUBDIVISION OF ELEMENT 304 )\*\*\*\*\*

```

*
*NUMBER OF NODES CREATED
* 1
* NOD.NAME      COORD'S (X,Y) RELATIVE TO END(1) OF SUBDIVIDED ELEMENT
* #n28          0.000000E+00      0.400000E+03
*-----
*

```

```

*NUMBER OF ELEMENTS CREATED
*          2
* ELM.NAME   TYPE.OF.ELEMENT   NOD.NAMES
* #e47       cbp2              301      #n28
* #e48       qdp2              #n28     311
*-----*
*
*NUMBER OF IMPERFECT ELEMENTS
*          0
*****

      0          0.64172000E+03      2      0.317E-03      3

***** ( SUBDIVISION OF ELEMENT #e48 )*****
*
*NUMBER OF NODES CREATED
*          1
* NOD.NAME   COORD'S (X,Y) RELATIVE TO END(1) OF SUBDIVIDED ELEMENT
* #n29       0.000000E+00          0.320000E+04
*-----*
*
*NUMBER OF ELEMENTS CREATED
*          2
* ELM.NAME   TYPE.OF.ELEMENT   NOD.NAMES
* #e50       cbp2              #n29     311
* #e49       qdp2              #n28     #n29
*-----*
*
*NUMBER OF IMPERFECT ELEMENTS
*          0
*****

      0          0.64173000E+03      2      0.392E-07      4

***** ( SUBDIVISION OF ELEMENT #e49 )*****
*
*NUMBER OF NODES CREATED
*          1
* NOD.NAME   COORD'S (X,Y) RELATIVE TO END(1) OF SUBDIVIDED ELEMENT
* #n30       0.000000E+00          0.400000E+03
*-----*
*
*NUMBER OF ELEMENTS CREATED
*          2
* ELM.NAME   TYPE.OF.ELEMENT   NOD.NAMES
* #e51       cbp2              #n28     #n30
* #e52       qdp2              #n30     #n29
*-----*
*
*NUMBER OF IMPERFECT ELEMENTS
*          0
*****

***** ( SUBDIVISION OF ELEMENT 305 )*****
*
*NUMBER OF NODES CREATED
*          1
* NOD.NAME   COORD'S (X,Y) RELATIVE TO END(1) OF SUBDIVIDED ELEMENT
* #n31       0.000000E+00          0.360000E+04
*-----*

```

```

*
*NUMBER OF ELEMENTS CREATED
*
*      2
* ELM.NAME   TYPE.OF.ELEMENT   NOD.NAMES
* #e54       cbp2              #n31      321
* #e53       qdp2              311         #n31
*-----*
*
*NUMBER OF IMPERFECT ELEMENTS
*
*      0
*****

      0      0.64174000E+03      2      0.101E-06      4

***** ( SUBDIVISION OF ELEMENT #e53 )*****
*
*NUMBER OF NODES CREATED
*
*      1
* NOD.NAME   COORD'S (X,Y) RELATIVE TO END(1) OF SUBDIVIDED ELEMENT
* #n32       0.000000E+00      0.320000E+04
*-----*
*
*NUMBER OF ELEMENTS CREATED
*
*      2
* ELM.NAME   TYPE.OF.ELEMENT   NOD.NAMES
* #e56       cbp2              #n32      #n31
* #e55       qdp2              311         #n32
*-----*
*
*NUMBER OF IMPERFECT ELEMENTS
*
*      0
*****

      0      0.64175000E+03      2      0.172E-06      4

***** ( SUBDIVISION OF ELEMENT #e52 )*****
*
*NUMBER OF NODES CREATED
*
*      1
* NOD.NAME   COORD'S (X,Y) RELATIVE TO END(1) OF SUBDIVIDED ELEMENT
* #n33       0.000000E+00      0.240000E+04
*-----*
*
*NUMBER OF ELEMENTS CREATED
*
*      2
* ELM.NAME   TYPE.OF.ELEMENT   NOD.NAMES
* #e58       cbp2              #n33      #n29
* #e57       qdp2              #n30      #n33
*-----*
*
*NUMBER OF IMPERFECT ELEMENTS
*
*      0
*****

      0      0.64176000E+03      2      0.243E-06      4
      0      0.64177000E+03      2      0.436E-03      1
      0      0.64178000E+03      2      0.723E-05      2

***** ( SUBDIVISION OF ELEMENT #e55 )*****
*
*NUMBER OF NODES CREATED

```

```

*          1
* NOD.NAME      COORD'S (X,Y) RELATIVE TO END(1) OF SUBDIVIDED ELEMENT *
* #n34          0.000000E+00          0.280000E+04
*-----*
*
*NUMBER OF ELEMENTS CREATED
*          2
* ELM.NAME      TYPE.OF.ELEMENT      NOD.NAMES
* #e60          cbp2                  #n34      #n32
* #e59          qdp2                  311      #n34
*-----*
*
*NUMBER OF IMPERFECT ELEMENTS
*          0
*****
0          0.64179000E+03      2          0.127E-03      4
0          0.64180000E+03      2          0.319E-04      2
0          0.64181000E+03      2          0.396E-03      4

***** ( SUBDIVISION OF ELEMENT #e57 ) *****
*
*NUMBER OF NODES CREATED
*          2
* NOD.NAME      COORD'S (X,Y) RELATIVE TO END(1) OF SUBDIVIDED ELEMENT *
* #n35          0.000000E+00          0.400000E+03
* #n36          0.000000E+00          0.200000E+04
*-----*
*
*NUMBER OF ELEMENTS CREATED
*          3
* ELM.NAME      TYPE.OF.ELEMENT      NOD.NAMES
* #e61          cbp2                  #n30      #n35
* #e63          cbp2                  #n36      #n33
* #e62          qdp2                  #n35      #n36
*-----*
*
*NUMBER OF IMPERFECT ELEMENTS
*          0
*****
0          0.64182000E+03      2          0.122E-08      6
81         0.64182000E+03      4          0.191E+00      10

```



## 9.7 Apexes

- 
- 
- (a) Indicates the kind of analysis required.
  - (b) Introduces the characteristics of the materials: the name, the material model, and the properties, which are different for each material model ([Chapter 3](#)).
  - (c) Introduces the [type of section](#), the name, material and the dimensions.
  - (d) Defines the groups. There you define the [element type](#), the [group](#) name and the name give to the section.
  - (e) Defines the coordinates of the [structural nodes](#).
  - (f) Defines the global coordinates of the structural nodes ([non.structural.nodes](#)).
  - (g) Defined the nodal restraints. The f-command indicates the name of the first nodes which has [restraints](#), and the r-command is referred to the increment of this and how many times it has to increment the nod.name.
  - (h) Defines the [connectivity of elements](#) in a mesh configuration. First is indicated the group name. At the f-command is the name of the element and the extreme nodes of it and at the r-command is defined the increment of the nod.name, the extreme nodes and when it has to stop.
  - (i) Indicates the kind of [load](#) and the direction of each one.
  - (j) This module, [phases](#), is used to trace the load deflection curve for the proportional loading.
  - (k) This module specifies the [iterative strategy](#) applied during a load or time step.
  - (l) Defines the tolerance at the iterative calculating process, and the reference value in calculating the [convergence](#).
  - (m) Specifies the frequency of numerical [output](#).
  - (n) This module specifies levels within elements of specific types [\(\\*\)](#).
  - (o) This module specifies the conditions which govern the termination of the automatic control phrase under a proportional static loading regime [\(\\*\\*\)](#).
  - (p) This modules defines subdivision [patterns](#) utilised in automatic mesh refinement.
  - (q) This module specifies piecewise [linear load curves](#) for dynamic or time history loading.
  - (r) This module specifies the time scheme for dynamic analysis and its parameters [\(\\*\\*\\*\)](#).
- 
-

---

---

(s) This module defines of intervals at which structural equilibrium is established [\\*\\*\\*\\*](#).

---

---